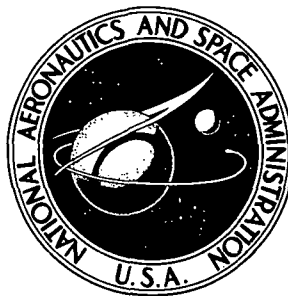


**NASA CONTRACTOR  
REPORT**



**NASA CR-2415**

**NASA CR-2415**

**SEPARATED FLOW OVER BODIES  
OF REVOLUTION USING AN UNSTEADY  
DISCRETE-VORTICITY CROSS WAKE**

**Part II - Computer Program Description**

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**NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • JUNE 1974**

1. Report No. NASA CR-2415		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle SEPARATED FLOW OVER BODIES OF REVOLUTION USING AN UNSTEADY DISCRETE-VORTICITY CROSS WAKE - PART II COMPUTER PROGRAM DESCRIPTION				5. Report Date June 1974	
				6. Performing Organization Code	
7. Author(s) F.J. Marshall and F.D. Deffenbaugh				8. Performing Organization Report No.	
9. Performing Organization Name and Address Purdue University School of Aeronautics and Astronautics W. Lafayette, Indiana				10. Work Unit No. 760-65-11-0200	
				11. Contract or Grant No. NGR 15-005-119 (181)	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, DC 20546				13. Type of Report and Period Covered Contractor Report	
				14. Sponsoring Agency Code	
15. Supplementary Notes Topical report.					
16. Abstract  A method is developed to determine the flow field of a body of revolution in separated flow. The technique employed is the use of the computer to integrate various solutions and solution properties of the sub-flow fields which made up the entire flow field without resorting to a finite difference solution to the complete Navier-Stokes equations. The technique entails the use of the unsteady cross flow analogy and a new solution to the required two-dimensional unsteady separated flow problem based upon an unsteady, discrete-vorticity wake. Data for the forces and moments on aerodynamic bodies at low speeds and high angle of attack (outside the range of linear inviscid theories) such that the flow is substantially separated are produced which compare well with experimental data. In addition, three dimensional steady separated regions and wake vortex patterns are determined.  This report describes the computer program developed to perform the numerical calculations.					
17. Key Words (Suggested by Author(s)) Bodies of Revolution Separated flow Unsteady flow Crossflow Flow field				18. Distribution Statement  Unclassified  STAR Category 12	
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages 154	
				22. Price* \$5.00	

## TABLE OF CONTENTS

INTRODUCTION . . . . .	Page 1
ABBREVIATIONS AND ADDITIONAL LIST OF SYMBOLS . . . . .	2
METHOD OF SOLUTION . . . . .	3
VCF PROGRAM DESCRIPTION . . . . .	3
VCF PROGRAM INPUT DATA . . . . .	3
VCF PROGRAM OUTPUT DATA . . . . .	6
VCF PROGRAM STRUCTURE . . . . .	7
VCF AUXILIARY FILES . . . . .	7
VCF OPERATING INSTRUCTIONS . . . . .	7
ADYNF PROGRAM DESCRIPTION . . . . .	9
ADYNF PROGRAM INPUT DATA . . . . .	9
ADYNF PROGRAM OUTPUT DATA . . . . .	11
ADYNF PROGRAM STRUCTURE . . . . .	12
ADYNF OPERATING INSTRUCTIONS . . . . .	12
APPENDIX I:       PROGRAM VCF AND SUBPROGRAM DESCRIPTIONS . . . . .	13
APPENDIX Ia:       PROGRAM ADYNF AND SUBPROGRAM DESCRIPTIONS . . . . .	47
APPENDIX Ib:       SUBROUTINE IC . . . . .	52
APPENDIX II:       CANNED SUBPROGRAMS - CADRE - SECOND - SPLINE, ARITH1 - TRID . . . . .	65
APPENDIX III:       PROGRAM LISTINGS - VCF - ADYNF - SUBPROGRAMS . . . . .	101
APPENDIX IV:       SAMPLE CASE - VCF - ADYNF . . . . .	137
REFERENCES . . . . .	152

## INTRODUCTION

In part 1 of this two part report the theory was developed to determine the forces acting on a body of revolution in a uniform stream. The body was inclined at an angle of attack sufficient for the flow to become separated and for vortices to form on the lee side. This part of the report describes the computer programs, VCF and ADYNF, which carry out the numerical calculations of part 1. VCF is the main body of the work which calculates the sectional normal force coefficient,  $c_n$ , at stations along the body axis. ADYNF using the results obtained from VCF numerically integrates  $c_n(z)$  over the body length to obtain the normal force coefficient  $C_N$ , and the moment coefficient  $C_{M,\lambda}$ . Useful vortex patterns are available, and a line of separation along the body can be determined.

## Abbreviations and Additional List of Symbols

### Abbreviations

3DS	three dimensional steady
2DUS	two dimensional unsteady
b.l.	boundary layer
r.s.l.	rear shear layer
t.b.l.	top boundary layer
b.b.l.	bottom boundary layer
t.r.s.l.	top rear shear layer
b.r.s.l.	bottom rear shear layer

### Sub- and Superscript

$( )^V$	point vortex contribution
$( )^P$	potential flow contribution

### Numerical Integration Parameters

$(\theta_i, t_k, \bar{r}_j)$	set of points in $\bar{r}, t, \theta$ plane $i = 0, 1, 2 \dots, \text{IDIM}$ $k = 0, 1, 2 \dots, \text{KFINAL}$ $j = 0, 1, 2 \dots, \text{JDIM}$
$u(\theta_i, t_k, \bar{r}_j)$	$(u)^i$ evaluated at point $(\theta_i, t_k, \bar{r}_j)$
$v(\theta_i, t_k, \bar{r}_j)$	$(v)^i$ evaluated at point $(\theta_i, t_k, \bar{r}_j)$

## METHOD OF SOLUTION

The forces acting on a body of revolution at high angle of attack are calculated by the two complementary programs VCF, and ADYNF. Program VCF calculates the normal force distribution on the body by first solving the two dimensional unsteady problem of a circular cylinder started impulsively from rest, and then by using the viscous cross flow analogy to relate the cylinder drag to the normal force sectional coefficient. ADYNF then integrates the normal force distribution supplied by VCF to obtain the normal force and moment coefficients. A detailed description of the method is given in part 1 of this report.

## VCF PROGRAM DESCRIPTION

The computer program was written in FORTRAN IV language, and was run on a CDC 6500 computer at Purdue University under the MACE operating system. VCF requires approximately 110000 octal words central memory initially, and CP time for an average run is approximately 30 minutes. The program requires three peripheral disc files in addition to the input, output, and punch files.

## VCF PROGRAM INPUT DATA

The input to VCF consists of the Reynolds number based on body length, the angle of attack, the body geometry, and program control data.

### Description of Input Decks

The user must supply the body geometry in the form of a FUNCTION subprogram named RZERO. The value of the dimensional body radius  $r_o^*$ , should be returned as a function of dimensional axial distance along the body,  $\hat{z}^*$ . In addition ENTRY DRZERO must return  $dr_o^*/d\hat{z}^*$ . FUNCTION RZERO is a subprogram deck of VCF supplied by the user.

### Deck Setup:

FUNCTION RZERO (ZSTAR)	CARD 1
RZERO = (body radius at ZSTAR)	CARD 2
RETURN	CARD 3

ENTRY DRZERO

CARD 4

RZERO = (rate of change of body radius with respect to axial distance evaluated at ZSTAR)

CARD 5

RETURN

CARD 6

END

CARD 7

### Description of Input Cards

CARD 1 - Identification. - Card 1 contains any desired identifying information in columns 1-80.

CARD 2 - Flow parameters, body length. - Card 2 contains 3 real numbers, punched in a 12-column field. Columns 37-80 may be used in any desired manner. Card 2 contains the following.

Columns	Variable	Value	Description
1-12	AATACK		Angle of attack in degrees
13-24	RE		$Re_{3DS} = V\ell/\nu$
25-36	LENGTH		Dimensional body length, $\ell$ , same units as $r_o^*$ .

CARD 3 - Remaining input data. - Card 3 contains three parameters particular to the finite difference and outer flow numerical computation schemes. They are punched in a 12-column field. Columns 37-80 may be used in any desired manner. Card 3 contains the following.

Columns	Variable	Value	Description
1-12	DELT	.125	The time increment used in the finite difference solution to the boundary layer equations, $\Delta t_k$
13-24	RC	.05	Potential vortex core cutoff radius, $r_c$
25-36	SIGMA	.05-1.0	Empirical vortex flux factor, $\sigma$

CARD 4 - Program control - The three parameters punched in Card 4, the first right justified in a three column field, and the rest in twelve column fields, determine when the program is to STOP. All data necessary for further execution of the program is written on an auxiliary disk file. Card 4 contains the following.

Columns	Variable	Value	Description
1-3	KFINAL	1-100	If KFINAL = K, where K is an integer count of the number of program time cycles completed, appropriate data is written on an auxiliary disk file and the program STOPS.
13-24	TFINAL		If TFINAL equals or exceeds the central processor time used, data is written on file and the program STOPS.
25-36	ZFINAL	0.0-1.0	If the nondimensional distance along the body axis z, equals or exceeds ZFINAL data is written on file and the program STOPS.

CARD 5 - Input/Output Control. - Card 5 contains 4 numbers each punched right justified in a 2-column field. These parameters specify which auxiliary disk files are to be used in input/output operations, the type of punched output, and the type of printed output. Card 5 contains the following.

Columns	Variable	Value	Description
1-2	LR	0,3,4	The continue data is READ from TAPE (LR). If LR = 0 no data is read from the auxiliary disk file.
3-4	LW	3-4	The continue data is WRITTEN on TAPE (LW).
5-6	LEVEL	5	Printed Output Level.
7-8	KPUN		Cards are punched every KPUN cycles.



## VCF PROGRAM OUTPUT DATA

Printed output is processed by a standard 132 characters-per-line printer, punched cards are in Hollerith (026) code, 80 characters per cards. Binary coded data is written on auxiliary files, TAPE 1, TAPE 3, and TAPE 4. The program printed output options are described below:

**LEVEL = 3** The program prints the dimensional body geometry as the radius as a function of axial distance. The maximum body diameter, the characteristic length, the fineness ratio, and frontal area, which are all functions of input body geometry are printed. Remaining card input data is printed. Point vortex locations, velocities and strengths, are printed. The pressure distribution around the two-dimensional cylinder corresponding to an axial station along the three dimensional body is printed for each program cycle, as well as values of shear and pressure drag. Data specifying the rear separation angle is printed for each cycle after the backflow velocity has exceeded .1 of the free stream velocity. Elapsed computer execution time is printed at the end of each program cycle.

**LEVEL = 5** In addition to level 3 output, the boundary layer profile for the top portion of the cylinder is printed.

The program printed output is illustrated by the sample case presented in Appendix IV.

The program punched output consists of variables punched every program cycle, and of variables punched every KPUN cycles. Values of nondimensional axial distance, coefficient of drag, nondimensional time, and the number of time cycles completed are punched every cycle. Vortex positions, velocities, and strengths are punched every KPUN cycles.

The binary coded data output consists of initial boundary layer velocities, (Reference 2), written on TAPE 1. Values of boundary layer velocities, vortex positions, vortex velocities, vortex strengths, program indices, and rear shear layer data are written on TAPE (LW) at the termination of each run.

## VCF PROGRAM STRUCTURE

VCF consists of a MAIN program, 18 SUBROUTINE subprograms, 5 FUNCTION subprograms, and 1 FUNCTION subprogram supplied by the user. Detailed descriptions of the MAIN program and of the subprograms are given in Appendix I. An example of a user supplied geometry description deck is given in Appendix IV for the case of an ogive cylinder.

## VCF AUXILIARY FILES

VCF designates TAPE 5 as the input file, TAPE 6 as the output file, and TAPE 7 as the punch file. In addition three auxiliary files are utilized for transfer of binary data. These files are designated TAPE 1, TAPE 3, and TAPE 4.

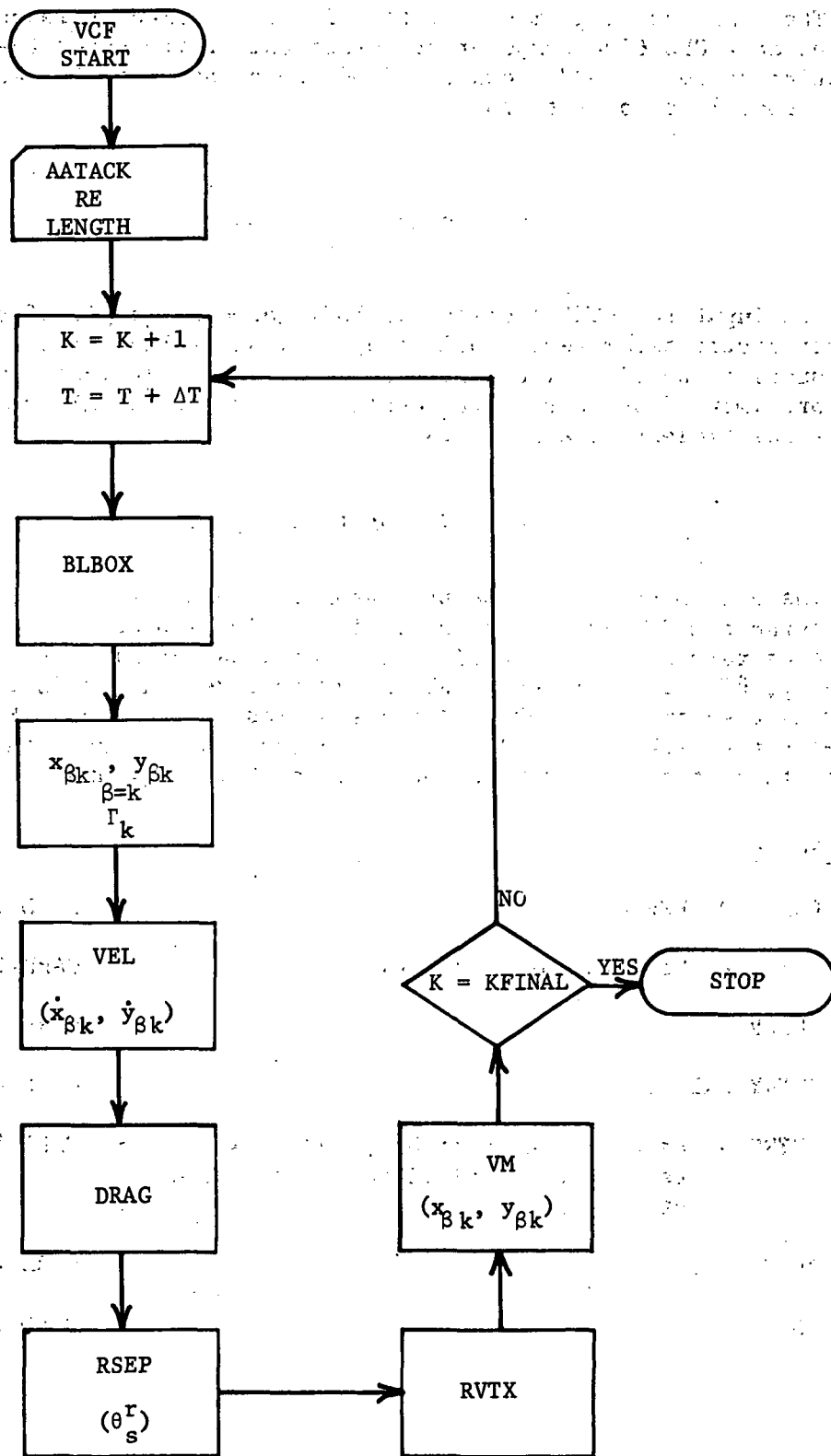
TAPE 1 is used to store the initial boundary layer profile. TAPE 3 and TAPE 4 are used to store intermediate information which is used to continue execution of the program.

These auxiliary files must be rewound and stored on magnetic tape or some other permanent storage file at the termination of each run. To continue the run the files are obtained from permanent file storage, and execution is continued, the necessary data being READ from TAPE 3 or TAPE 4.

## VCF OPERATING INSTRUCTIONS

The program deck, geometry input deck, and data deck are loaded in the following sequence: job card, system control cards, end-of-record card, program deck, geometry input deck, end-of-record card, data deck, end-of-file card. The geometry input deck and the data deck are described in the Program Input Data section.

# VCF FLOWCHART



## ADYNF PROGRAM DESCRIPTION

The computer program was written in the FORTRAN IV language, and was run on a CDC 6500 computer at Purdue University under the MACE operating system. ADYNF requires 55000 words of central memory and takes about 10 seconds to run.

## ADYNF PROGRAM INPUT DATA

The input to ADYNF consists of body geometry, angle of attack, characteristic parameters supplied by VCF, and values of  $c_n$  and  $\hat{z}$ , also supplied by VCF. The number of knots and their locations, used to approximate functions in the evaluation of the normal force and moment coefficients are also read in.

### Description of Input Decks

The user must supply the body geometry in the form of a FUNCTION subprogram named RZERO. The value of the dimensional body radius  $r_o^*$ , should be returned as a function of dimensional axial distance along the body,  $\hat{z}^*$ . In addition ENTRY DRZERO must return  $dr_o^*/d\hat{z}^*$ . FUNCTION RZERO is a subprogram deck of ADYNF supplied by the user. For a given geometry the deck used in ADYNF is identical to that used in PROGRAM VCF, and in fact, the same deck may be used for both programs

#### Deck Setup:

FUNCTION RZERO (ZSTAR)	CARD 1
RZERO = (body radius at ZSTAR)	CARD 2
RETURN	CARD 3
ENTRY DRZERO	CARD 4
RZERO = (Rate of change of body radius with respect to axial distance evaluated at ZSTAR)	CARD 5
RETURN	CARD 6
END	CARD 7

## Description of Input Cards

CARD 1 - Identification. - Card 1 contains any desired identifying information in columns 1-80.

CARD 2 - Flow parameters, characteristic dimensions. - Card 2 contains 6 real numbers, punched in a 12-column field. Columns 73-80 may be used in any desired manner. Card 2 contains the following.

Columns	Variable	Value	Description
1-12	AATACK		Angle of attack in degrees
13-24	LAMBDA		Moment arm, $\lambda$
25-36	LENGTH		Dimensional body length, $l$
37-48	F		Fineness Ratio, $f$
49-60	AW		Characteristic length, $\hat{a}$
61-72	RW		Maximum Radius, $d/2$

CARD 3 - Number of knots, number of data points. - Card 3 contains 2 integers right justified in a 4 column field. The number of knots refers to the number of cubic polynomials used to obtain an approximating function to the data. A cubic polynomial approximates the data between two knots. Card 3 contains the following.

Columns	Variable	Value	Description
1-4	NOKNOT	4-5	The interval is divided into 3 or 4 segments depending on whether NOKNOT is 4 or 5. The endpoints of the segments are the knots.
5-8	LX		The number of data points, $\hat{z}$ , $C_D(\hat{z})$ .

CARD 4,5 ... - Axial distance  $\hat{z}$ , Coefficient of drag  $C_D(\hat{z})$ . - Card 4,5 ... contain values of  $\hat{z}$  and  $C_D(\hat{z})$ , these cards are punched by PROGRAM VCF. The two numbers are punched in the first two 12-column fields of each card.

CARD LAST - Knot positions. - The last card in the input deck to ADYNF contains the location of the knots. Since the nondimensional body length is 1.0, these knot values should be: 0, values contained in the interval [0,1], and 1. The knot values are punched in a 12-column field: 6 to a card. The last card contains the following.

Columns	Variable	Value	Description
1-12	XI(1)	0	Location of first knot
13-24	XI(2)	0 < ( ) < 1	Location of 2nd knot
.	XI(NOKNOT)	1	Location of last knot

#### ADYNF PROGRAM OUTPUT DATA

Program ADYNF output is printed output processed by a standard 132 character-per-line printer. The program printed output consist of:

- (1) The given data [ $\hat{z}$ ,  $c_n(\hat{z})$ ]
- (2) The number of knots
- (3) Initial knot locations
- (4) Optimized knot locations (reference 4)
- (5) The cubic coefficients used to approximate the data in each interval
- (6) The errors involved in approximating the data
- (7) The data point  $\hat{z}$  and the approximation  $c_n(\hat{z})$
- (8) Values of  $\hat{z}$  at .05 increments from 0 to 1.0 and the value of the approximation  $c_n(\hat{z})$
- (9) Intermediate output from the integration subroutine CADRE (see Appendix II for details)
- (10) The approximation to the integral  $\int_0^1 c_n(\hat{z}) d\hat{z}$ . The absolute error, and an indication as to the types of singularities involved in the integration. (see APPENDIX II - CADRE for further details)
- (11) The normal force coefficient  $C_N$
- (12) Similar output for the calculation of the moment coefficient  $C_{M,\lambda}$ .

## ADYNF PROGRAM STRUCTURE

ADYNF is a main program which references the subprograms RZRO, FIT, SPLINEB, CADRE and the user input geometry subprogram RZERO. SPLINE, references 3 and 4, and CADRE are "canned" routines obtained from Purdue University's computing center. SPLINE is a deck of subprograms. ADYNF calls SPLINEB which references other subprograms in the SPLINE deck. Those subprograms are considered to be "black boxes," and are not explained in detail in this report. However listings of the SPLINE deck are included in APPENDIX II. Listings of ADYNF, FIT, and RZRO are given in APPENDIX III. ADYNF designates TAPE 5 as input file and TAPE 6 as output file. No other files are used.

## ADYNF OPERATING INSTRUCTIONS

The program deck, geometry input deck, and data deck are loaded in the following sequence: job card, system control cards, end-of-record card, program deck, geometry input deck, end-of-record card, data deck, end-of-file card. The geometry input deck and the data deck are described in the Program Input Data section.

## APPENDIX I

### PROGRAM VCF AND SUBPROGRAM DESCRIPTIONS

This appendix contains a brief outline of the purpose, method, and use of program VCF and its subroutines. The principal variables and constants in each are listed, and identified as input or output data. The subprograms are listed in alphabetical order.



## PROGRAM VCF

**PURPOSE:** To calculate the local normal force distribution coefficient  $c_n(\hat{z})$ , to predict the line of separation  $\theta_s(\hat{z})$ , and to provide the point vortex distribution,  $(x_{\beta k}, y_{\beta k})$ .

**METHOD:** VCF proceeds in discrete steps of time  $\Delta t_k$ , usually given the value .125. The index  $K$ , initially 0, is incremented by 1 for each step in time, thus  $K=1$  for  $t_1 = t_0 + \Delta t_1$ , where  $t_0$  denotes the initial time. The boundary layer equations are integrated using a finite difference solution developed by M. G. Hall, reference 1. The initial velocity distribution is supplied by Wundt's solution, reference 2, to the impulsive start of a circular cylinder. Once the initial conditions have been calculated the subroutines used in the computations are no longer necessary. By writing all of the pertinent data on a FILE, in this instance either TAPE3 or TAPE4, and then replacing the inert subroutine with a dummy subroutine IC, and reading the data back in, the central memory requirement can be reduced after the first few minutes of computation time. Further, since the boundary layer solution employs a finite difference method, storage must be allocated for a finite difference mesh or grid. However, since separation soon occurs, values at mesh points greater than the separation angle are no longer needed. By stopping execution, saving the necessary data, redimensioning the boundary layer grid, and then reading the data back in, and continuing execution, the central memory requirements can be reduced even further. For the case of the ogive cylinder the central memory requirement could be reduced from 110000 words to 65000 words. The boundary layer grid is DIMENSIONED in the main program and values of  $u^1$ , and  $v^1$  are passed as parameters to subprograms with the DIMENSION parameters IDIM, JDIM. Thus if boundary layer grid values are no longer being used because they are in separated flow the variables  $U$ ,  $W$ ,  $UT$ , and  $UB$  are appropriately DIMENSIONED in the main program.

The boundary layer finite difference scheme is applied either to the top half of the cylinder or the bottom. The entire boundary layer solution could be accomplished by a call to BLBOX with appropriate values of velocity on the upper surface being supplied, and then another call to BLBOX with lower surface values. However, since the solution is basically a small time one, and the flow is expected to be symmetrical, it is only necessary to apply the finite difference solution to half of the cylinder.

Once the velocity distribution in the boundary layer is known, and a separation angle has been determined, vorticity is introduced into the outer flow in the form of point vortices. Due to the symmetry of the problem

separate vortex arrays were created for the vortices born from the top separation angle, and for those coming from the bottom separation angle. In addition when backflow velocities were great enough to generate vorticity on the rear portion of the cylinder two additional top and bottom arrays were created for those point vortices originating from the rear separation angles.

Bernoulli's equation yields the pressure distribution on the cylinder, and numerically integrating  $C_p \cos \theta$  ( $0 < \theta < 2\pi$ ), gives the drag.

The point vortices existing at time  $t_k$  are convected with the fluid and at time  $t_{k+1} = t_k + \Delta t_k$  the tangential velocity on the surface (boundary conditions for the boundary layer equations), will be altered. A new boundary layer velocity profile is calculated, a new separation angle determined, and the cycle is repeated. When  $t_k$  corresponding to  $\hat{z} = 1.0$  is reached, the program stops.

USE:

Input:

INFO	Data identification
AATACK	Angle of attack
RE	Reynolds number based on body length
LENGTH	Dimensional body length
DELT	Finite difference time step
RC	Vortex core cutoff value
SIGMA	Empirical vortex flux factor
KFINAL	Program cycle termination index
TFINAL	Program central processor time termination value
ZFINAL	Nondimensional length termination value
LR	READ continue data from TAPE(LR) if LR=0 no binary continue data is READ
LW	WRITE continue data on TAPE(LW)
KPUN	Vortex positions, velocities, and strengths are punched every KPUN cycles
LEVEL	Printed output level

Output:

PI	$\pi$
DTOR	$\pi/180$
RTOD	$180/\pi$
DMAX	Maximum body diameter
AW	Characteristic length $\tilde{a}$ , of the 2DUS flow
F	Fineness ratio, $f$
SA	Frontal area, $S$
RE	$Re_{2DUS}$
KS	Initially equal to 1000, KS is set equal to K when the first point vortex is born from the b.l.
KR	Initially equal to 1000, KR is set equal to K when the backflow velocity exceeds a value of .1
KT	Equal to the number of t.b.l. vortices in the flow at time $t_k$
KB	Equal to the number of b.b.l. vortices in the flow at time $t_k$
KRT	Equal to the number of t.r.s.l. vortices in the flow at time $t_k$
KRB	Equal to the number of b.r.s.l. vortices in the flow at time $t_k$
INITAL	The initial dimension of the $\theta$ grid in the b.l.
NDIM	Dimension of the vortex arrays, and of the drag array. The number of program cycles must not exceed NDIM
IDIM, JDIM	b.l. grid dimension: $(\theta_i, \bar{r}_j)$ $i = 1, 2, \dots, IDIM$ $j = 1, 2, \dots, JDIM$
PI2	$2\pi$
SQRTPI	$\sqrt{\pi}$

SQA	Square of the sine of the angle of attack
SRE	$\sqrt{RE_{2DUS}}$
ISYM	Symmetric mode index ISYM = 1, symmetric mode ISYM = 0, asymmetric mode
THTASYM	Condition on $\theta_s$ , if THTASYM is greater than $\theta_s$ , the program goes into the asymmetric mode
K	Program time index, initially set equal to 0 at $t_0$ . K is incremented by 1 for each successive step in time
KTS	Index used in the continuation of a run, if $KTS \geq K$ the b.l. grid is calculated
TI	$t_0$
ZHAT	$\hat{z}$
AK	Radius at time $t_k$ , $a(t_k)$
AKTI	$a(t_0)$
AKDOT	$\dot{a}(t_k)$
CDPI	Initial drag coefficient due to pressure = $2\pi a(t_0) \dot{a}(t_0)$
KMINUS1	$K-1$
TH	$t_k - 1/2$
AK	Radius at time $t_k$ , $a(t_k)$
AKDOT	$\dot{a}(t_k)$
AADOT	$a(t_k) \dot{a}(t_k)$
AKSQD	$[a(t_k)]^2$
ZHALF	$\hat{z}(t_k - 1/2)$
AKPHALF	$a(t_k - 1/2)$
AKDOTPH	$\dot{a}(t_k - 1/2)$
KTTEMP	Temporary storage of the value of KT

KBTEMP	Temporary storage of the value of KB
U	Boundary layer velocity, $\bar{u}(\bar{r}, t_k, \theta)$
DGAMMA	$(\Gamma)_t$
SMALLM	$m_k$
CDST	$\int_0^{\theta_s} \tau \sin \theta \, d\theta \quad 0 < \theta_s < \pi$
CLST	$\int_0^{\theta_s} \tau \cos \theta \, d\theta \quad 0 < \theta_s < \pi$
ISEP	An integer denoting the element in the $\theta_1$ array, the value of which is the separation angle
TRAPD	Trapezoidal sum used in the evaluation of CDST and CDSB
TRAPL	Trapezoidal sum used in the evaluation of CLST and CLSB
CDSK	Viscous contribution to the drag coefficient = $\frac{1}{2} \int_0^{2\pi} \tau \sin \theta \, a(t) \, d\theta$
TT	Array of t.b.l. vortex diffusion times
TB	Array of b.b.l. vortex diffusion times
TRT	Array of t.r.s.l. vortex diffusion times
TRB	Array of b.r.s.l. vortex diffusion times
X, Y	Arrays of t.b.l. vortex coordinates
XDOT, YDOT	Arrays of t.b.l. vortex velocities ( $\hat{u}^\circ, \hat{v}^\circ$ )
GAMMA	Array of t.b.l. vortex strengths
XB, YB	Arrays of b.b.l. vortex coordinates
XDOTB, YDOTB	Arrays of b.b.l. vortex velocities

GMAB Array of b.b.l. vortex strengths

XRT, YRT Arrays of t.r.s.l. vortex coordinates

XRDOT, YRDOT Arrays of t.r.s.l. vortex velocities

GMRT Array of t.r.s.l. vortex strengths

XRB, YRB Arrays of b.r.s.l. vortex coordinates

XRDOTB, YRDOTB Arrays of b.r.s.l. vortex velocities

GMRB Array of b.r.s.l. vortex strengths

CDSB  $\int_0^{\theta_s} \tau \sin \theta d\theta \quad \pi < \theta_s < 2\pi$

CLSB  $\int_0^{\theta_s} \tau \cos \theta d\theta \quad \pi < \theta_s < 2\pi$

THETA  $\theta$

THETAS  $\theta_s \quad 0 < \theta < \pi$

THETASB  $\theta_s \quad \pi < \theta < 2\pi$

THIASR  $\theta_s^r$

IPUN Punch index

IPUN  $\geq 1$ , punch vortex arrays  
IPUN  $< 1$ , no vortex array punch

CDPK Drag coefficient due to pressure =  
 $\frac{1}{2} \int_0^{2\pi} C_p \cos \theta a(t) d\theta$

CDK Drag coefficient,  $C_D(t)$

CDN Local normal force distribution coefficient,  $C_n$

TIME Execution time

SUBPROGRAMS  
CALLED:

BLBOX, DQI, DRZRO, NONDIM, PDRAG, RSEP, RVTX, RZRO,  
SECOND, VEL, VM, WRIT

# FUNCTION AN

**PURPOSE:** To calculate the coefficients  $a_n, b_n, c_n$

**METHOD:** Given the b.l. velocity distribution the coefficients  $a_n, b_n, c_n$  are calculated as outlined in reference 1.

**USE:** Function reference to

AN (L, N, IDIM, JDIM, U, W)

## Input:

L, N The b.l. grid point  $(\theta_i, \bar{r}_j)$

IDIM, JDIM b.l. grid dimension  $(\theta_i, \bar{r}_j)$   
 $i = 1, 2, \dots, IDIM$   
 $j = 1, 2, \dots, JDIM$

U  $u(\theta_i, t_k, \bar{r}_j)$

W  $u(\theta_i, t_k, \bar{r}_j)$

DS

DZ8

DZSQ2 See BLBOX

DZSQ4

## Output:

AN Coefficient  $a_n$  in the finite difference solution of the b.l. equations

**CALLED FROM:** BLBOX

**REMARKS:** Alternate ENTRY points to AN are BN, and CN

# SUBROUTINE BLBOX

PURPOSE: To numerically integrate the unsteady b.l. equations

METHOD: A finite difference method is employed to solve the two dimensional unsteady boundary layer equations, (reference 1).

USE: CALL BLBOX (SMALL M, DGAMMA, TAWD, TAWL, U, W, UT, UB, IDIM, JDIM, MODE)

## Input:

U The b.l. velocity distribution  $u(\theta_i, t_{k-1}, \bar{r}_j)$

UT 2-dimensional storage away for  $u(\theta_i, t_{k-1}, \bar{r}_j)$

UB 2-dimensional storage away for  $u(\theta_i, t_{k-1}, \bar{r}_j)$   
 $\pi < \theta_i < 2\pi$

UTNBIG An array the elements of which are the boundary conditions (t.b.l.), for the finite difference scheme

UBNBIG Boundary conditions (b.b.l.)

IDIM, b.l. grid dimension  $(\theta_i, \bar{r}_j)$   
 JDIM  $i = 1, 2, \dots, IDIM$   
 $j = 1, 2, \dots, JDIM$

MODE If MODE = 1 appropriate t.b.l.  $u^i$  values will be input to the b.l. grid. If MODE = 2 b.b.l.  $u^i$  values are input

KTS Index used in the continuation of a run, if  $KTS \geq K$  the b.l. grid is calculated

AK  $a(t_k)$

AKSQD  $[a(t_k)]^2$

AKDOT  $\dot{a}(t_k)$

AKPHALF  $a(t_{k-1/2})$

IXTRSET An integer denoting the element in the S array, the value of which is the t.b.l. separation angle



IXBRSET    An integer denoting the element in the S array, the value of which is the b.b.l. separation angle

NBIG        An integer defining the last element in the AN array

Output:

DELS         $\Delta\theta$  used to define the b.l. grid  $\theta_{i+1} = \theta_i + \Delta\theta$

DS        Defining the elements of the array DS as,  $\Delta\theta_{i+1} = \theta_{i+1} - \theta_i$ , allows for the grid defined to have a variable mesh spacing.

S        Array of  $\theta_i$  values

ST        Array of t.b.l.  $\theta_i$  values

SB        Array of b.b.l.  $\theta_i$  values

DZ        b.l. grid spacing  $\Delta\bar{r} = .14$

DZ2         $1/2 \Delta\bar{r}$

DZSQ2       $1/2 \Delta\bar{r}^2$

DZSQ4       $1/4 \Delta\bar{r}^2$

ZN        Array of  $\bar{r}$  values

U        The b.l. velocity distribution  $u(\theta_i, t_k, \bar{r}_j)$

UT        2-dimensional storage array for  $u(\theta_i, t_k, \bar{r}_j)$   
 $\pi < \theta_i < 2\pi$

UB        2-dimensional storage array for  $u(\theta_i, t_k, \bar{r}_j)$   
 $\pi < \theta_i < 2\pi$

TAUS      Successive estimates of the surface  
 TAUNEW    shear  $\tau$

NCYCLE    The number of iterative cycles, (reference 1)

DUDR       $(\bar{u}), \bar{r}$

TAW         $\tau$

TAWD       $\tau \sin \theta$  evaluated for values of the  $\theta$  grid

TAWL       $\tau \cos \theta$  evaluated for values of the  $\theta$  grid

THETA  $\theta$

THETAS  $\theta_s$   $0 < \theta < \pi$

THETASB  $\theta_s$   $\pi < \theta < 2\pi$

SMALLM Location of vortex born from b.l.,  $m_k$

DGAMMA  $(\Gamma)_t$

CALLED

FROM: VCF

SUBPROGRAMS

CALLED: IC, FREEVTX, POTFLOW, TRID, RITE

REMARKS:

The b.l. subroutine determines the velocity profile for  $0 < \theta < \theta_s$  ( $0 < \theta_s < \pi$ ), or for  $0 < \theta < \theta_s$  ( $\pi < \theta_s < 2\pi$ ).

Thus if the flow is assumed to be symmetric, a finite difference solution is required only on the top half of the cylinder. If the flow is asymmetric, BLBOX is called twice with appropriate top or bottom grid values and boundary conditions being input.

# FUNCTION CPC

**PURPOSE:** To calculate  $C_p$

**METHOD:** The equations for evaluating  $C_p$  are given in part 1

**USE:** Function reference to

CPC (THTA)

Input:

TT

TB

TRT

TRB

X,  
Y

XDOT,  
YDOT

GAMMA

XB,  
YB

XDOTB,  
YDOTB

GMAB

XRT,  
YRT

XRDOT,  
YRDOT

GMRT

XRB,  
YRB

XRDOTB,  
YRDOTB

GMRB

See VCF

K

KT

KB

See VCF

KRT

KRB

XX        X coordinate of the point on the cylinder  
          surface at which  $C_p$  is to be evaluated

YY        Y coordinate of the point on the cylinder  
          surface at which  $C_p$  is to be evaluated

NDIM      Dimension of the vortex arrays

Output:

PHIT       $\phi_t = (\phi_t)^V + (\phi_t)^P$

PHIVT      $(\phi_t)^V$

PHIPT      $(\phi_t)^P$

PSIKR2     $u_\infty$

CPC        Pressure coefficient

CALLED

FROM:

VCF

SUBPROGRAMS

CALLED:

PV, FREEVTX, POTFLOW

REMARKS:

The time derivative of the potential function,  $(\phi_t)$ , see part 1, is computed by first determining the terms due to the point vortices  $(\phi_t)^V$ , adding to that the potential flow solution of a changing radius cylinder in a uniform flow  $(\phi_t)^P$ .

# FUNCTION DN

**PURPOSE:** To determine the coefficient  $d_n$ , (reference 1)

**METHOD:** The equations for the calculation of  $d_n$  are given in reference 1

**USE:** Function reference to

DN (L, N, IDIM, JDIM, U, W)

## Input:

L, N The b.l. grid point  $(\theta_i, \bar{r}_j)$

IDIM, JDIM b.l. grid dimension  $(\theta_i, \bar{r}_j)$   
 $i = 1, 2, \dots, IDIM$   
 $j = 1, 2, \dots, JDIM$

U  $u(\theta_i, t_k, \bar{r}_j)$

W  $v(\theta_i, t_k, \bar{r}_j)$

DS

DZ2 see BLBOX

NBIG

DT2  $1/2 \Delta t_k$

## Output:

DN Coefficient  $d_n$  in the finite difference solution of the b.l. equations

**CALLED**

**FROM:** BLBOX

**SUBPROGRAMS**

**CALLED:** UM, US, UL, AN

# SUBROUTINE DQI

PURPOSE: To evaluate  $\int_0^{2\pi} C_p \cos \theta d\theta$

METHOD: Numerical integration using Simpsons rule

$$\int_{x_0}^{x_2} f(x) dx \sim \frac{h}{3} [f(x_2) + 4f(x_1) + f(x_0)]$$

USE: CALL DQI (FCT, CK, K, N, ISYM)

## Input:

FCT The name of the EXTERNAL FUNCTION SUBPROGRAM used; PDRAG to evaluate drag, PLIFT to evaluate lift.

K Program time index, see VCF

N An even integer which determines the integration stepsize h. The front of the cylinder is divided into 2N equal parts, the front here being  $-60^\circ < \theta < 60^\circ$ , and the back is divided into 8N equal parts. The stepsize,  $h = (60/N)(\pi/180)$ .

ISYM An integer either 0 or 1. A value of 1 denotes a symmetric flow, and the limits of integration are  $(0, \pi)$  and the value of the integral is doubled. A value of 0 denotes an asymmetric flow and the limits of integration are  $(0, 2\pi)$

## Output:

CK Approximation to  $\int_0^{2\pi} C_p \cos \theta d\theta$  by Simpson's Rule

CALLED FROM: VCF

SUBPROGRAMS CALLED: PDRAG

REMARKS: The value of N used in all testing was 6.

## SUBROUTINE FREEVTX

**PURPOSE:** To calculate vortex induced velocities

**METHOD:** Each point vortex and its image induce a velocity at every other point in the field. The distance between the field point and the vortex location is determined and induced velocity calculated, see part 1. Summing the effects of all the point vortices yields the vortex induced velocity.

**USE:** CALL FREEVTX (PSIK1X, PSIK1Y, PSIK1R, IA)

Input:

IA            An integer value from 1 to 5.  
IA = 1    Field point is a t.b.l. vortex  
IA = 2    Field point is a b.b.l. vortex  
IA = 3    Field point is on the cylinder  
IA = 4    Field point is a t.r.s.l. vortex  
IA = 5    Field point is a b.r.s.l. vortex

TT

TB

TRT

TRB

X,  
Y

XDOT,  
YDOT

See VCF

GAMMA

XB,  
YB

XDOTB,  
YDOTB

GMAB

XRT,  
YRT

XRDOT,  
YRDOT

GMRT

XRB,  
YRB

XRDOTB,  
YRDOTB

See VCF

GMRB

KT

KB

TRT

KRB

ALPHA

An integer denoting a particular point vortex,  
the coordinates of which is the point at  
which the velocity is being calculated.

XX

X coordinate of the point vortex at which  
the velocity is being calculated.

YY

Y coordinate of the point vortex at which the  
velocity is being calculated.

Output:

PSIK1X  $(\hat{v}^{\circ})^v$

PSIK1Y  $-(\hat{u}^{\circ})^v$

PSIK1R  $(u^{\circ})^v$

CALLED  
FROM:

BLBOX, VEL, CPC

SUBPROGRAMS  
CALLED:

PSI



# SUBROUTINE IC

**PURPOSE:** To calculate the initial boundary layer profile for the problem of a circular cylinder started impulsively from rest.

**METHOD:** Wundt's solution for the impulsive start of a circular cylinder, (reference 2).

**USE:** CALL IC (AKTI, U, IDIM, JDIM, MODE)

Input:

AKTI  $a(t_0)$

IDIM, b.l. grid dimension ( $\theta_i, \bar{r}_j$ )

JDIM  $i = 1, 2 \dots, IDIM$   
 $j = 1, 2 \dots, JDIM$

MODE MODE = 1  $0 < \theta_i < \pi$   
 MODE = 2  $\pi < \theta_i < 2\pi$

Output:

U  $u(\theta_i, t_0, \bar{r}_j)$

UTNBIG An array, the elements of which are the boundary conditions (t.b.l.) for the finite difference scheme.  $u(\theta_i, t_0, \bar{r}_j)$   
 $j = JDIM \quad 0 < \theta_i < \pi$

UBNBIG Boundary conditions (b.b.l.)  $u(\theta_i, t_0, \bar{r}_j)$   
 $j = JDIM \quad \pi < \theta_i < 2\pi$

**CALLED FROM:** BLBOX

**SUBPROGRAMS CALLED:** PHIO, PHI1, ZTA001, ZTA0011, ZTA02A1, ZTA02B1

**REMARKS:** Subroutine IC is called once from BLBOX when  $t_k = t_0$  (K=1). A dummy subroutine may be substituted thereafter, reducing the central memory requirement. The IC subroutine and the subprograms called from IC are listed in Appendix Ib.

# SUBROUTINE NONDIM

**PURPOSE:** To calculate the characteristic radius  $\tilde{a}$ , the maximum diameter  $d$ , and the reference area  $S$ , for the input body geometry.

**METHOD:** Values of  $r_o^*(\hat{z}^*)$  are obtained from RZERO, the FUNCTION SUBPROGRAM input by the user, for values of  $\hat{z}^*$  along the body axis. The maximum  $r_o^*(\hat{z}^*)$ , doubled, is  $d$ . For a closed end body ( $r_o^*(\ell) = 0$ ) the characteristic radius is obtained by using the trapezoidal rule to approximate the integral  $1/\ell \int_0^{\ell} r_o^*(\hat{z}^*) dz^* = \tilde{a}$ . For open ended geometries ( $r_o^*(\ell) \neq 0$ ), then  $\tilde{a} = d/2$ .

**USE:** CALL NONDIM (DMAX, RW, AW, F, S, L, PI)

## Input:

L            Dimensional body length,  $\ell$

PI            $\pi$

## Output:

DMAX        Maximum body diameter,  $d$

RW            $d/2$

AW           Characteristic length,  $\tilde{a}$

F            Fineness ratio,  $\ell/d$

S            Frontal area =  $\pi d^2/4$

**CALLED**

**FROM:**       VCF

**SUBPROGRAMS**

**CALLED:**     RZERO

# FUNCTION PDRAG

PURPOSE: To calculate  $C_p(\theta) \cos \theta$

METHOD: Function reference to CPC

USE: Function reference to

PDRAG (THETA)

## Input:

THETA  $\theta$

## Output:

PDRAG  $C_p(\theta) \cos \theta$

CALLED

FROM: VCF

SUBPROGRAMS

CALLED: CPC

REMARKS: See DQI

# SUBROUTINE POTFLOW

PURPOSE: To calculate the velocity at a point in the outer flow due to the uniform inviscid flow about a circular cylinder.

METHOD: Evaluate potential flow solution at a field point

USE: CALL POTFLOW (PSIKXP, PSIKYP, PSIKRP, IA)

## Input:

ALPHA Point vortex index

AKSQD  $[a(t_k)]^2$

IA An integer value from 1 to 5  
IA = 1 Field point is a t.b.l. vortex  
IA = 2 Field point is a b.b.l. vortex  
IA = 3 Field point is on the cylinder  
IA = 4 Field point is a t.r.s.l. vortex  
IA = 5 Field point is a b.r.s.l. vortex

X,  
Y

XDOT,  
YDOT

GAMMA

XB,  
YB

XDOTB, See VCF  
YDOTB

GMAB

XRT,  
YRT

XRDOT,  
YRDOT

GMRT

XRB,  
YRB

XRDOTB,  
YRDOTB

See VCF

GMRB

Output:

PSIKXP  $(\dot{v}^o)^P$

PSIKYP  $-(\dot{u}^o)^P$

PSIKRP  $(u^o)^P$

CALLED  
FROM:

BLBOX, VEL, CPC

# SUBROUTINE PSI

**PURPOSE:** To sum the induced vortex velocity

**METHOD:** The equations for the induced velocity of a point vortex are given in part 1.

**USE:** CALL PSI (X, Y, GMA, NDIM, KI, KF, IA, IB, SUM, SUM1, TK)

## Input:

AK  $a(t_k)$

AKSQD  $[a(t_k)]^2$

XX, YY Coordinates of the point at which the velocity is being calculated

X, Y Input arrays of point vortex locations

GMA Input array of point vortex strengths

NDIM Dimension of the input arrays

KI, KF Sum over  $KF - KI + 1$  vortices

TK Input array of vortex diffusion times

RC  $r_c$

IA Field point index (See FREEVTX)

IB Integer which determines if a point vortex is to be ignored in the sum

## Output:

SUM  $\vec{v}^\circ$  induced by input vortex array

SUM1  $-\vec{u}^\circ$  induced by input vortex array

**CALLED FROM:** FREEVTX

# SUBROUTINE PV

**PURPOSE:** To calculate the vortex contribution to  $C_p$

**METHOD:** Equations for the calculation of  $\phi_t$  are given in part 1.

**USE:** CALL PV (X, Y, XDT, YDT, GMA, NDIM, KI, KF, SUM, TK)

## Input:

AK  $a(t_k)$

AKSQD  $[a(t_k)]^2$

XX, YY Coordinates of the point on the cylinder at which  $C_p$  is to be evaluated

X, Y Input arrays of point vortex locations

XDT, YDT Input arrays of point vortex velocities

GMA Input array of point vortex strengths

NDIM Dimension of the input arrays

KI, KF Sum over KF - KI + 1 vortices

TK Input array of vortex diffusion times

RC  $r_c$

## Output:

SUM  $\phi_t$  due to input vortex array

**CALLED  
FROM:**

CPC

# SUBROUTINE RITE

**PURPOSE:** To print the b.l. velocity distribution

**METHOD:** ENCODE is used to create execution time FORMAT statements, so that only the velocity profile for  $0 < \theta < \theta_s$  is printed.

**USE:** CALL RITE (MT, IDIM, JDIM, U, ZN, NX, S, DEG, ZHAT, DELS, K)

## Input:

**MT** An integer value equal to 1 or 2  
If MT = 1 the initial velocity profile is printed  
If MT = 2 the velocity profile at  $t_k$  is printed

**IDIM,** b.l. grid dimension ( $\theta_i, \bar{r}_j$ )  
**JDIM**  $i = 1, 2, \dots, IDIM$   
 $j = 1, 2, \dots, JDIM$

**U**  $u(\theta_i, t_k, \bar{r}_j)$

**ZN** Array of  $\bar{r}_j$  values  $j = 1, 2, \dots, JDIM$

**NX** An array containing a count of the number of iterative cycles (reference 1).

**S** Array of  $\theta_i$  values  $i = 1, 2, \dots, IDIM$

**DEG** Array of  $\theta_i$  values in degrees

**ZHAT**  $\hat{z}$

**DELS**  $\Delta\theta$

**K** Program cycle index

**CALLED**

**FROM:** BLBOX, IC

**REMARKS:** When MT = 1,  $u^i$  is output, when MT = 2  $\bar{u}$  is output.



# SUBROUTINE RSEP

**PURPOSE:** To determine the r.s.l. separation angle

**METHOD:** 
$$\frac{\theta_s^f - \theta_m^f}{\theta_o^f - \theta_m^f} = \frac{\theta_m^r - \theta_s^r}{\theta_m^r - \theta_o^r} \quad (\text{see part 1})$$

**USE:** CALL RSEP (THETASF, THETASR, THETA, UBL, INTX1, INITIAL, MODE)

## Input:

**THETASF:** b.l. separation angle,  $\theta_s^f$   
**THETA** Array of  $\theta_i$  values  $i = 1, 2, \dots, \text{INITIAL}$   
**UBL** Array of  $u_o^o$  ( $\theta_i$ ) values  $i = 1, 2, \dots, \text{INITIAL}$

**INTX1** An integer denoting the element of the THETA array which is the separation angle

**INITIAL** The initial dimension of the b.l. grid, ( $\theta_i = \pi$ )  $i = \text{INITIAL}$

**MODE**  $\text{MODE} = 1 \quad 0 < \theta_i < \pi$   
 $\text{MODE} = 2 \quad \pi < \theta_i < 2\pi$

## Output:

**THETASR** r.s.l. separation angle,  $\theta_s^r$

**CALLED**

**FROM:** VCF

# SUBROUTINE RVTX

**PURPOSE:** To calculate the position and strength of the r.s.l. vortices

**METHOD:** Subroutine RSEP has determined the r.s.l. separation angle. The strength of the vortex that would be born is  $\Gamma = -\Delta t u_0^2/2$ . If this value of  $\Gamma$  does not exceed .1 it is stored in arrays. The next time cycle ( $t_{k+1}$ ), a new  $\theta_s^r$  is calculated, and if the new separation angle exceeds the previous one then the previous point vortex is aborted. However, if the new  $\theta_s^r$  is less than the previous value of  $\theta_s^r$ , the previous point vortex is lumped together with the one now in question. After five time cycles ( $t_k < t < t_{k+5}$ ), or when the lumped vortex strength becomes .1 or greater, the lumped vortex is placed into the outer flow. The angle at which it is placed is the average of the five previous separation angles. See part 1 for equations.

**USE:** CALL RVTX (X, Y, GMA, THTASR, THTASM, THTAS, UZZ, UZZSQ, GAMA, MODE, KR, N, NF, IFLAG, BMATL, NDIM, TK)

## Input:

AK	$a(t_k)$
DELT	$\Delta t_k$
THETAS	$\theta_s$
THTASR	$\theta_s^r$
THTASM	$\theta_s^r$ at the time previous to r.s.l. vortex birth
THTAS	Storage array for $\theta_s^r$ values
UZZ	Storage array for $u_0$ values
UZZSQ	Storage array for $u_0^2$ values
GAMA	Storage array for $\Gamma$ values
MODE	MODE = 1 $0 < \theta < \pi$ MODE = 2 $\pi < \theta < 2\pi$
N	An integer count of the number of time cycles completed since the previous r.s.l. vortex was placed in the outer flow.

NF           Lump parameter, usually  $NF = 5$ . When  
               $N = NF$  a lumped point vortex is placed in  
              the outer flow

NDIM          Dimension of vortex arrays

TK           An array of vortex diffusion times

Output:

GMATL        Lumped vortex strength

IFLAG        If  $IFLAG(N) = 0$ , the point vortex aborted  
              If  $IFLAG(N) = 1$ , the point vortex is lumped

X,           Coordinates of r.s.l. vortex born  
Y

GMA           Strength of r.s.l. vortex born

SMALLM        $m_{rk}$

KRN           The  $KRN^{th}$  element of the r.s.l. vortex arrays

CALLED

FROM:        VCF

SUBPROGRAMS

CALLLED:     FREEVTX, POTFLOW

## FUNCTION RZRO

**PURPOSE:** To calculate the nondimensional body radius  $r_o$  as a function of nondimensional distance  $\hat{z}$  along the body axis.

**METHOD:** The dimensional quantities are multiplied by characteristic dimensions.

**USE:** Function reference to  
RZRO (ZHAT, L, RW)

Input:

ZHAT	$\hat{z}$
L	$l$
RW	$d/2$

Output:

RZRO	$r_o$
------	-------

**CALLED FROM:** VCF

**SUBPROGRAMS CALLED:** RZERO

# FUNCTION UAPRX1

**PURPOSE:** To calculate a first approximation to  $u(\theta_{i+1}, t_k, \bar{r}_j)$

**METHOD:**  $u(\theta_{i+1}, t_k, \bar{r}_j) = u(\theta_{i+1}, t_{k-1}, \bar{r}_j) + u(\theta_i, t_k, \bar{r}_j) - u(\theta_i, t_{k-1}, \bar{r}_j)$   
 See reference 1, for further explanation.

**USE:** Function reference to  
 UAPRX1 (L, N, IDIM, JDIM, U)

Input:

L,	The b.l. grid point $(\theta_i, \bar{r}_j)$
N	
IDIM,	b.l. grid dimension $(\theta_i, \bar{r}_j)$
JDIM	$i = 1, 2, \dots, IDIM$ $j = 1, 2, \dots, JDIM$
U	$u(\theta_i, t_{k-1}, \bar{r}_j)$

Output:

U	First approximation to $u(\theta_{i+1}, t_k, \bar{r}_j)$
---	--

**CALLED FROM:** BLBOX, DN

**REMARKS:** Alternate ENTRY points to UAPRX1 are US, UL, and UM

# SUBROUTINE VEL

**PURPOSE:** To calculate the velocity of the point vortices

**METHOD:** Each point vortex has a velocity due to the uniform flow around a circular cylinder, plus the velocity induced by all of the other point vortices.

**USE:** CALL VEL (X, Y, XDT, YDT, NDIM, KI, KF, IA)

## Input:

X, Input arrays of vortex locations  
Y

NDIM Dimension of the vortex arrays

KI, KF - KI+1 is the number of vortices  
in an array

IA Vortex field point index (see FREEVTX)

## Output:

XDT, Output arrays of vortex velocities  
YDT

**CALLED**

**FROM:** VCF, RVTX

**SUBPROGRAMS** USED: POTFLOW

**CALLED:** FREEVTX, POTFLOW

# SUBROUTINE VM

**PURPOSE:** To calculate the coordinates of the point vortices at time  $t_{k+1}$ .

**METHOD:** Each point vortex travels  $\tilde{u}^\circ \Delta t_k$  in the x direction, and  $\tilde{v}^\circ \Delta t_k$  in the y direction.

**USE:** CALL VM (X, Y, XDT, YDT, NDIM, KI, KF, IA)

## Input:

X, Y Vortex locations at  $t_k$

XDT, YDT Input arrays of vortex velocities

KI, KF  $KF - KI + 1$  is the number of vortices in an array

IA Vortex field point index (see FREEVTX)

## Output:

R Distance from cylinder to vortex

XTEMP, YTEMP Temporary storage of the input vortex locations

X, Y Vortex locations at  $t_{k+1}$

**CALLED FROM:** VCF

**SUBPROGRAMS CALLED:** VMFIX

**REMARKS:** VMFIX is called only if  $R < a(t_k)$

# SUBROUTINE VMFIX

**PURPOSE:** To calculate a corrected point vortex location.

**METHOD:** The  $\Delta t_k$  approximation involved in the motion of the vortices allows for the possibility that a point vortex may cross the cylinder boundary. Since this is physically impossible VMFIX appends the vortex motion and places the point vortex outside of the cylinder. VMFIX calculates the tangent to the cylinder at the point where a vortex has crossed the cylinder boundary. Appended  $\tilde{u}^\circ$ ,  $\tilde{v}^\circ$  are returned to VM such that the point vortex will travel along the tangent line.

**USE:** CALL VMFIX (X, Y, XDOT, YDOT)

## Input:

X, Vortex location inside of cylinder  
Y

XDOT, Original  $\tilde{u}^\circ$ ,  $\tilde{v}^\circ$   
YDOT

DEF Some small parameter (.001), applied to the transformations to insure that the appended velocities will result in a new vortex location outside of the cylinder.

## Output:

L Quadrant in which the point vortex is located

XDOT, Appended  $\tilde{u}^\circ$ ,  $\tilde{v}^\circ$   
YDOT

**CALLED FROM:** VCF

**REMARKS:** VM calls VMFIX if  $R < a(t_k)$  (see VM), upon returning to VM the vortex location is recalculated starting with the original vortex position.



# SUBROUTINE WRIT

PURPOSE: Print, punch, vortex locations, strengths, and velocities.

METHOD: Tape 6 = Output, Tape 7 = Punch

USE: CALL WRIT (X, Y, XDOT, YDOT, GAMMA, XB, YB, GMAB, KIT, KFT, KIB, KFB, K, NDIM, IW)

## Input:

X, Input array of t.b.l. or t.r.s.l. vortex locations  
Y

XDOT, Input array of t.b.l. or t.r.s.l. vortex  
YDOT velocities

GAMMA Input array of t.b.l. or t.r.s.l. vortex  
strengths

XB, Input array of b.b.l. or b.r.s.l. vortex  
YB locations

XDOTB, Input array of b.b.l. or b.r.s.l. vortex  
YDOTB velocities

GMAB Input array of b.b.l. or b.r.s.l. vortex  
strengths

KIT, KFT - KIT + 1 = number of t.b.l. or t.r.s.l.  
KFT vortices to be output

KIB, KFB - KIB + 1 = number of b.b.l. or b.r.s.l.  
KFB vortices to be output

IW IW = 6 Print  
IW = 7 Punch  
IW = 9 Write on TAPE 9

CALLED  
FROM: VCF

## APPENDIX Ia

### PROGRAM ADYNF AND SUBPROGRAM DESCRIPTIONS

This appendix contains a brief outline of the purpose, method, and use of program ADYNF and subroutine FIT. Subroutine RZRO is described in APPENDIX I. Subroutines SPLINEB and CADRE are not described in this APPENDIX but are listed in APPENDIX II.

PURPOSE: To calculate  $C_N$  and  $C_{M,\lambda}$

METHOD: Values of  $C_D(\hat{z})$  and  $\hat{z}$  output from PROGRAM VCF are input on cards to PROGRAM ADYNF. The normal force and moment are given by

$$C_N = (4f/\pi) \int_0^1 c_n d\hat{z}, \text{ and}$$

$$C_{M,\lambda} = - (4f/\pi) \int_0^1 \left[ \hat{z} + \frac{r_o}{4f^2} \frac{dr_o}{d\hat{z}} \right] c_n d\hat{z} + \lambda C_N$$

respectively. Approximations to these integrals are evaluated by first obtaining a least squares cubic spline approximation to the integrand function and then by integrating the approximate function. The integration interval is divided into sections, and a cubic polynomial approximates the integrand in each section. The endpoints of the sections are called "knots" the approximating cubics being continuous up to the third derivative at the "knots."

USE:

Input:

INFO	Data Identification
AATACK	Angle of attack
LAMBDA	Moment arm coefficient
LENGTH	Dimensional body length
F	Fineness Ratio
AW	Characteristic length, $\hat{a}$
RW	Maximum Radius, $d/2$
NOKNOT	Number of knots used to segment the interval [0,1]
LX	The number of $C_D(\hat{z})$ values
X	Array of $\hat{z}$ values

PORCD      Array of  $C_D(\hat{z})$  values

XI          Array of knot positions, the length of the array equals NOKNOT

Output:

ITER        Number of sweeps through opt,(reference 4)

XI          Knot values after optimization

COEFL       Cubic coefficients

ERRL2       Least square error, spline approximation

ERRL1       Average error, spline approximation

ERRL99      Maximum error, spline approximation

XX

$\hat{z}$

FCTL        Spline approximation to integrand at  $\hat{z}$

PRINT       Scaled error, spline approximation

CN          Normal force coefficient  $C_N$

CNI          Approximation to the integral  $\int_0^1 c_n d\hat{z}$

ERROR       Computed absolute error in CNI (See Appendix II - CADRE)

IFLAG       An integer between 1 and 5 indicating what difficulties were met with in obtaining an approximation to CNI (See Appendix II - CADRE)

CM          Moment coefficient,  $C_{M,\lambda}$

CMI          Approximation to the integral

$$\int_0^1 \left[ \hat{z} + \frac{r_o}{4f^2} \frac{dr_o}{d\hat{z}} \right] c_n d\hat{z}$$

SUBPROGRAMS

CALLED:      SPLINEB, CADRE, FIT, RZRO

REMARKS:

VCF punched output  $\hat{z}$ ,  $C_D(\hat{z})$  is input to ADYNF. The first value of  $\hat{z}$  output by VCF is  $\hat{z} = .03$ , and the final value of  $\hat{z}$  is usually slightly less than 1.0. It is known that at  $\hat{z} = 0$ ,  $C_D = 0$ , and by extrapolating the given data to  $\hat{z} = 1.0$ , two additional data points are input to ADYNF. See the ADYNF PROGRAM INPUT DATA section, and APPENDIX IV - ADYNF SAMPLE INPUT, for further explanation of the input data.

To evaluate the  $C_N$  and  $C_{M,\lambda}$  integrals, the integrand functions are approximated using cubic splines. This smooths the data, and allows for the integrand to be approximated at any  $\hat{z}$  which permits the use of the integration routine CADRE. CADRE has been proven to be a very successful numerical integration scheme and errors in the calculation of  $C_N$ ,  $C_{M,\lambda}$  are believed to be less than 2%. Subprograms RZRO and RZERO are called by ADYNF. For listings and use of CADRE and SPLINEB see Appendix II.

# FUNCTION FIT

PURPOSE: To determine the integrand values  $[c_n]$  or  

$$\left[ \hat{z} + \frac{r_o}{4f^2} \frac{dr_o}{d\hat{z}} \right] c_n$$
 for arbitrary values of  $\hat{z}$ ,  $0 < \hat{z} < 1$ .

METHOD: The cubic coefficients have been supplied by SPLINEB.  
 The set of coefficients used to approximate the integrand depends upon knot locations and  $\hat{z}$ .

USE: Function reference to FIT (X)

## Input:

X	$\hat{z}$
XI	Knot locations
COEFL	Cubic coefficients

## Output:

FIT	Cubic spline approximation to the integrand function
-----	--

CALLED  
FROM:

ADYNF

REMARKS: For further information on spline approximations see, references 3 and 4 and SPLINE listing in Appendix II.

## APPENDIX Ib

### SUBROUTINE IC

This appendix contains a listing of SUBROUTINE IC and subprograms referenced by IC. After the first program cycle is completed SUBROUTINE IC and its subprograms are no longer required, and can be replaced by a dummy SUBROUTINE IC. The coding for the dummy program follows the original SUBROUTINE IC listing.

# Description of Parameters

Variable or FUNCTION Subprogram	Description [2]
Q	q
QP	q'
QPP	q''
ETA	$\eta$
ZTA001(ETA)	$\zeta'_{00}(\eta)$
ZTA02A1(ETA)	$\zeta'_{0,2a}(\eta)$
ZTA02B1(ETA)	$\zeta'_{0,2b}(\eta)$
PHIO(ETA)	$\Phi_0(\eta)$
PHI1(ETA)	$\Phi_1(\eta)$
ZTA011(ETA)	$\zeta'_{01}(\eta)$



SUBROUTINE IC(AKT,I,U,IDIM,JDIM,MODE)		
DIMENSION U(IDIM,2,JDIM)	IC	2
DIMENSION NX(53),DEG(53)		
DIMENSION THTA(53)		
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,OTOR,RT00,RC,RCHXSQ,SIGMA,LEVEL		
COMMON/BLOCK20/DX,DZ,INTX1,NBIG1	IC	6
COMMON/BLOCK14/S(53),ST(53),SB(53)		
COMMON/BLOCK30/T,TI,DELT,DELTT,DELTB	IC	7
COMMON/BLBOX2/TAU,PT4,NBIG	IC	8
COMMON/BLBOX12/ZN(51),ISEP	IC	9
COMMON/BLBOX13/KTS,IXRSET,IXBRSET,UTNBIG(53),UBNBIG(53)		
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	IC	13
COMMON/BLBOX4/A2,A0,B1,C0,D2,D0,E1,E0	IC	14
COMMON/BLBOX5/A4A,A2A,A0A,P3A,B1A,C2A,C0A,D3A,D1A,E4A,E2A,E0A,F0A	IC	15
COMMON/BLBOX6/G4A,G2A,G1A,G0A,H3A,H2A,H1A,H0A,I2A,I1A,I0A	IC	16
COMMON/BLBOX7/K4A,K2A,K1A,K0A,L3A,L2A,L1A,L0A	IC	17
COMMON/BLBOX8/A4B,A2B,A0B,B3B,B1B,C2B,C0B,D3B,D1B,E4B,E2B,E0B,F0B	IC	18
COMMON/BLBOX9/G4B,G2B,G1B,G0B,H3B,H2B,H1B,H0B,I2B,I1B,I0B	IC	19
COMMON/BLBOX10/K4B,K2B,K1B,K0B,L3B,L2B,L1B,L0B	IC	20
REAL IP,KP,LP	IC	21
REAL I2,I2A,I2B,I1,I1A,I1B,I0,I0A,I0B	IC	22
REAL K4,K4A,K4B,K2,K2A,K2B,K1,K1A,K1B,K0,K0A,K0B	IC	23
REAL L3,L3A,L3B,L2,L2A,L2B,L1,L1A,L1B,L0,L0A,L0B	IC	24
IF(MODE.EQ.2) GO TO 1	IC	25
C*****	IC	26
C	IC	27
C WUNDT DATA	IC	28
C	IC	29
C*****	IC	30
A2= 1.	IC	31
A0= -.5	IC	32
P1= 1.5	IC	33
C0= .5	IC	34
D2= 3.0+4./(3.*PI)	IC	35
D0= -.5+2./(3.*PI)	IC	36
F1= 2.+2./(3.*PI)	IC	37
E0= -2./(3.*SQRT(PI))	IC	38
A4A=-1.0/3.0	IC	39
A2A=-1.0	IC	40
A0A=1.0/4.0	IC	41
P3A=-2.0/3.0	IC	42
B1A=-2.0	IC	43
C2A=-5.0/12.0	IC	44
C0A=-7.0/6.0	IC	45
D3A=9.0/40.0	IC	46
D1A=133.0/240.0	IC	47
E4A=9.0*SQRT(3.0)/(5.0*PI)	IC	48
E2A=27.0*SQRT(3.0)/(5.0*PI)	IC	49
F0A=27.0*SQRT(3.0)/(20.0*PI)	IC	50
F0A=8.0*SQRT(2.0)/(15.0*SQRT(PI))	IC	51
G4A=-5.0/6.0+2.0/(9.0*PI)	IC	52
G2A=-5.0/2.0+2.0/(3.0*PI)	IC	53
G1A=-4.0/(3.0*SQRT(PI))	IC	54
G0A=3.0/8.0-1.0/(2.0*PI)	IC	55
H3A=-13.0/12.0+1.0/(3.0*PI)	IC	56
H2A=2.0/(3.0*SQRT(PI))	IC	57
H1A=-73.0/24.0+23.0/(18.0*PI)	IC	58
H0A=-1.0/(3.0*SQRT(PI))	IC	59

I2A=-1.0/3.0+1.0/(9.0*PI)	IC	60
I1A=1.0/(3.0*SQR(T(PI)))	IC	61
I0A=-5.0/6.0+4.0/(9.0*PI)	IC	62
K4A=-1.0/2.0-(2.0+27.0*SQR(T(3.0)))/(15.0*PI)-64.0/(135.0*PI**2)	IC	63
K2A=3.0*K4A	IC	64
V1A=-4.0/SQR(T(PI))-16.0/(9.0*PI*SQR(T(PI)))	IC	65
K0A=1.0/8.0-(46.0+81.0*SQR(T(3.0)))/(60.0*PI)-16.0/(45.0*PI**2)	IC	66
L3A=-1.0/2.0-(2.0+27.0*SQR(T(3.0)))/(30.0*PI)-32.0/(135.0*PI**2)	IC	67
L2A=2.0/(3.0*SQR(T(PI)))	IC	68
L1A=-19.0/12.0-(22.0+81.0*SQR(T(3.0)))/(36.0*PI)-16.0/(27.0*PI**2)	IC	69
L0A=(-17.0+8.0*SQR(T(2.0)))/(15.0*SQR(T(PI)))-16.0/(15.0*PI*SQR(T(PI)))	IC	70
A4B=1.0/3.0	IC	71
A2B=0.0	IC	72
A0B=1.0/4.0	IC	73
B3B=7.0/12.0	IC	74
B1B=-3.0/8.0	IC	75
C2B=1.0/3.0	IC	76
C0B=-5.0/12.0	IC	77
D3B=-9.0/160.0	IC	78
D1B=-31.0/320.0	IC	79
E4B=-E4A/4.0	IC	80
E2B=-E2A/4.0	IC	81
E0B=-E0A/4.0	IC	82
F0B=F0A	IC	83
G4B=1.5+2.0/(3.0*PI)	IC	84
G2B=.5+2.0/(3.0*PI)	IC	85
G1B=0.0	IC	86
G0B=5.0/8.0-1.0/(6.0*PI)	IC	87
H3B=7.0/4.0+7.0/(9.0*PI)	IC	88
H2B=0.0	IC	89
H1B=-1.0/8.0+5.0/(6.0*PI)	IC	90
H0B=0.0	IC	91
I2B=0.5+2.0/(3.0*PI)	IC	92
I1B=0.0	IC	93
I0B=-1.0/4.0+2.0/(9.0*PI)	IC	94
K4B=7.0/6.0+(24.0+9.0*SQR(T(3.0)))/(20.0*PI)+32.0/(45.0*PI**2)	IC	95
K2B=0.5+(136.0+81.0*SQR(T(3.0)))/(60.0*PI)+32.0/(15.0*PI**2)	IC	96
K1B=0.0	IC	97
K0B=3.0/8.0+(56.0+81.0*SQR(T(3.0)))/(240.0*PI)+8.0/(15.0*PI**2)	IC	98
L3B=7.0/12.0+(24.0+9.0*SQR(T(3.0)))/(40.0*PI)+16.0/(45.0*PI**2)	IC	99
L2B=0.0	IC	100
L1B=-5.0/24.0+(40.0+27.0*SQR(T(3.0)))/(48.0*PI)+8.0/(9.0*PI**2)	IC	101
L0B=(-2.0+8.0*SQR(T(2.0)))/(15.0*SQR(T(PI)))-8.0/(45.0*PI*SQR(T(PI)))	IC	102
C*****	IC	103
C	IC	104
C    END WUNDT DATA	IC	105
C	IC	106
C*****	IC	107
1  CONTINUE	IC	108
DO 20 I=1,INTX1	IC	109
IF(MODE.EQ.1) S(I)=ST(I)	IC	110
IF(MODE.EQ.2) S(I)=SB(I)	IC	111
THTA(I)=S(I)	IC	112
DEG(I)=THTA(I)*RTOD		
*****  BC  Z=0	IC	113
U(I,1,1)=0.0	IC	114
U(I,2,1)=0.0	IC	115
DO 20 J=2,NBIG	IC	116

C***** B.C. THETA=0.0	IC	117
IF(I.NE.1) GO TO 11	IC	118
U(I,1,J)=0.0	IC	119
GO TO 20	IC	120
11 IF(J.NE.NBIG) GO TO 10	IC	121
U(I,1,NBIG)=2.0*SIN(THTA(I))	IC	122
IF(MODE.EQ.1) UTNBIG(I)=U(I,1,NBIG)	IC	123
IF(MODE.EQ.2) UBNBIG(I)=U(I,1,NBIG)	IC	124
GO TO 20	IC	125
10 CONTINUE	IC	126
ETA=ZN(J)/(2.0*SQRT(TI))	IC	127
Q=2.0*SIN(THTA(I))	IC	128
QP=2.0*COS(THTA(I))	IC	129
QPP=-2.0*SIN(THTA(I))	IC	130
U(I,1,J)=Q*(ZTA001(ETA)+TI*QP*ZTA011(ETA)+TI**2*(QP**2*ZTA02A1	IC	131
1(ETA)+Q*QPP*ZTA02B1(ETA)))	IC	132
20 CONTINUE	IC	133
C..... U AT T=TI GOES TO U(BAR) AT T=TI	IC	134
DO 21 I=1,INTX1	IC	136
UTNBIG(I)=AKTI*UTNBIG(I)	IC	137
UBNBIG(I)=AKTI*UBNBIG(I)	IC	138
DO 21 J=1,NBIG	IC	139
21 U(I,1,J)=AKTI*U(I,1,J)	IC	140
IF(MODE.EQ.2) GO TO 9	IC	141
IF(LEVEL.GE.4)CALL RITE(1,IDIM,JDIM,U,ZN,NX,S,DEG,ZHAT,DELS,K)		
9 CONTINUE	IC	157
WRITE(1)(UTNBIG(I),(U(I,1,J),J=1,NBIG),I=1,INTX1)		
RETURN	IC	163
END	IC	164

SUBROUTINE IC(AKTI,U,IDIM,JDIM,MODE)	IC	1
DIMENSION U(IDIM,2,JDIM)	IC	2
COMMON/BL90X13/KTS,IXTRSET,IXBRSET,UTNBIG(53),UBNBIG(53)	IC	3
READ(1)(UTNBIG(I),(U(I,1,J),J=1,51),I=1,53)	IC	4
RETURN	IC	5
END	IC	6

```

      FUNCTION PHIO(EATA)
      PHI=ERF(EATA)-1.0
      RETURN
      END

```

```

PHIO 1
PHIO 2
PHIO 3
PHIO 4

```

```

FUNCTION PHI1(EATA)
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DLTA
COMMON/BLBOX2/TAU,PT4,NBIG
PHI1=2.0*EXP(-EATA**2)/SQRT(PI)
RETURN
END

```

```

PHI1 1
PHI1 2
PHI1 3
PHI1 4
PHI1 5
PHI1 6

```

CTION ZTA001(EATA)  
ATA  
A001=ERF(E)  
TURN  
ND  
1249

ZTA001 1  
ZTA001 2  
ZTA001 3  
ZTA001 4  
ZTA001 5

```

FUNCTION ZTA011(EATA)
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DLTA
COMMON/BLBOX2/TAU,PT4,NBIG
COMMON/BLBOX4/A2,A0,B1,C0,D2,D0,E1,E0
E=EATA
A2=1.0
A0=-0.5
B1=1.5
C0=0.5
D2=3.0+4.0/(3.0*PI)
D0=-0.5+2.0/(3.0*PI)
E1=2.0+2.0/(3.0*PI)
E0=-2.0/(3.0*SQRTP(PI))
ZTA011=(A2*E*E+A0)*PHI0(E)**2+B1*E*PHI0(E)*PHI1(E)+C0*PHI1(E)**2
ZTA011=ZTA011+(D2*E*E+D0)*PHI0(E)+(E1*E+E0)*PHI1(E)
RETURN
END

```

```

ZTA011 1
ZTA011 2
ZTA011 3
ZTA011 4
ZTA011 5
ZTA011 6
ZTA011 7
ZTA011 8
ZTA011 9
ZTA01 10
ZTA01 11
ZTA01 12
ZTA01 13
ZTA01 14
ZTA01 15
ZTA01 16
ZTA01 17

```

<del>FUNCTION ZTA02A1(EATA)</del>	ZTA02A 1
<del>COMMON/BLBOX5/A4A,A2A,A0A,B3A,B1A,C2A,C0A,D3A,D1A,E4A,E2A,E0A,F0A</del>	ZTA02A 2
<del>COMMON/BLBOX6/G4A,G2A,G1A,G0A,H3A,H2A,H1A,H0A,I2A,I1A,I0A</del>	ZTA02A 3
<del>COMMON/BLBOX7/K4A,K2A,K1A,K0A,L3A,L2A,L1A,L0A</del>	ZTA02A 4
<del>REAL IP,KP,LP</del>	ZTA02A 5
<del>REAL I2,I2A,I2B,I1,I1A,I1B,I0,I0A,I0B</del>	ZTA02A 6
<del>REAL K4,K4A,K4B,K2,K2A,K2B,K1,K1A,K1B,K0,K0A,K0B</del>	ZTA02A 7
<del>REAL L3,L3A,L3B,L2,L2A,L2B,L1,L1A,L1B,L0,L0A,L0B</del>	ZTA02A 8
<del>E=EATA</del>	ZTA02A 9
<del>P0=PHI0(E)</del>	ZTA02 10
<del>P02=PHI0(E)**2</del>	ZTA02 11
<del>P03=PHI0(E)**3</del>	ZTA02 12
<del>P1=PHI1(E)</del>	ZTA02 13
<del>P12=PHI1(E)**2</del>	ZTA02 14
<del>P13=PHI1(E)**3</del>	ZTA02 15
<del>ET2=E**2</del>	ZTA02 16
<del>ET3=E**3</del>	ZTA02 17
<del>ET4=E**4</del>	ZTA02 18
<del>A4=A4A</del>	ZTA02 19
<del>A2=A2A</del>	ZTA02 20
<del>A0=A0A</del>	ZTA02 21
<del>B3=B3A</del>	ZTA02 22
<del>B1=B1A</del>	ZTA02 23
<del>C2=C2A</del>	ZTA02 24
<del>C0=C0A</del>	ZTA02 25
<del>D3=D3A</del>	ZTA02 26
<del>D1=D1A</del>	ZTA02 27
<del>E4=E4A</del>	ZTA02 28
<del>E2=E2A</del>	ZTA02 29
<del>E0=E0A</del>	ZTA02 30
<del>F0=F0A</del>	ZTA02 31
<del>G4=G4A</del>	ZTA02 32
<del>G2=G2A</del>	ZTA02 33
<del>G1=G1A</del>	ZTA02 34
<del>G0=G0A</del>	ZTA02 35
<del>H3=H3A</del>	ZTA02 36
<del>H2=H2A</del>	ZTA02 37
<del>H1=H1A</del>	ZTA02 38
<del>H0=H0A</del>	ZTA02 39
<del>I2=I2A</del>	ZTA02 40
<del>I1=I1A</del>	ZTA02 41
<del>I0=I0A</del>	ZTA02 42
<del>K4=K4A</del>	ZTA02 43
<del>K2=K2A</del>	ZTA02 44
<del>K1=K1A</del>	ZTA02 45
<del>K0=K0A</del>	ZTA02 46
<del>L3=L3A</del>	ZTA02 47
<del>L2=L2A</del>	ZTA02 48
<del>L1=L1A</del>	ZTA02 49
<del>L0=L0A</del>	ZTA02 50
<del>AP=(A4*ET4+A2*ET2+A0)*P03</del>	ZTA02 51
<del>BP=(B3*ET3+B1*E)*P02*P1</del>	ZTA02 52
<del>CP=(C2*ET2+C0)*P0*P12</del>	ZTA02 53
<del>DP=(D3*ET3+D1*E)*P13</del>	ZTA02 54
<del>SQRT2E=SQRT(2.0)*E</del>	ZTA02 55
<del>SQRT3E=SQRT(3.0)*E</del>	ZTA02 56
<del>EP=(E4*ET4+E2*ET2+E0)*PHI0(SQRT3E)</del>	ZTA02 57
<del>FP=F0*PHI0(SQRT2E)*P1</del>	ZTA02 58



GP= (G4*ET4+G2*ET2+G1*E+G0) *P02	ZTA02 59
HP= (H3*ET3+H2*ET2+H1*E+H0) *P0*P1	ZTA02 60
IP= (I2*ET2+I1*E+I0) *P12	ZTA02 61
KP= (K4*ET4+K2*ET2+K1*E+K0) *P0	ZTA02 62
LP= (L3*ET3+L2*ET2+L1*E+L0) *P1	ZTA02 63
ZTA02A1= AP+BP+CP+DP+EP+FP+GP+HP+IP+KP+LP	ZTA02 64
RETURN	ZTA02 65
END	ZTA02 66

FUNCTION ZTA02B1(EATA)	ZTA02B 1
COMMON/BL80X8/A4B,A2B,A0B,B3B,B1B,C2B,C0B,D3B,D1B,E4B,E2B,E0B,F0B	ZTA02B 2
COMMON/BL80X9/G4B,G2B,G1B,G0B,H3B,H2B,H1B,H0B,I2B,I1B,I0B	ZTA02B 3
<del>COMMON/BL80X10/K4B,K2B,K1B,K0B,L3B,L2B,L1B,L0B</del>	<del>ZTA02B 4</del>
REAL IP,KP,LP	ZTA02B 5
REAL I2,I2A,I2B,I1,I1A,I1B,I0,I0A,I0B	ZTA02B 6
REAL K4,K4A,K4B,K2,K2A,K2B,K1,K1A,K1B,K0,K0A,K0B	ZTA02B 7
REAL L3,L3A,L3B,L2,L2A,L2B,L1,L1A,L1B,L0,L0A,L0B	ZTA02B 8
E=EATA	ZTA02B 9
<del>P0=PHI0(E)</del>	<del>ZTA02 10</del>
P02=PHI0(E)**2	ZTA02 11
P03=PHI0(E)**3	ZTA02 12
P1=PHI1(E)	<del>ZTA02 13</del>
P12=PHI1(E)**2	ZTA02 14
P13=PHI1(E)**3	ZTA02 15
<del>ET2=E**2</del>	<del>ZTA02 16</del>
ET3=E**3	ZTA02 17
ET4=E**4	ZTA02 18
A4=A4B	ZTA02 19
A2=A2B	ZTA02 20
A0=A0B	ZTA02 21
<del>B3=B3B</del>	<del>ZTA02 22</del>
B1=B1B	ZTA02 23
C2=C2B	ZTA02 24
C0=C0B	<del>ZTA02 25</del>
D3=D3B	ZTA02 26
D1=D1B	ZTA02 27
<del>E4=E4B</del>	<del>ZTA02 28</del>
E2=E2B	ZTA02 29
E0=E0B	ZTA02 30
F0=F0B	ZTA02 31
G4=G4B	ZTA02 32
G2=G2B	<del>ZTA02 33</del>
<del>G1=G1B</del>	ZTA02 34
G0=G0B	ZTA02 35
H3=H3B	ZTA02 36
H2=H2B	ZTA02 37
H1=H1B	ZTA02 38
H0=H0B	ZTA02 39
<del>I2=I2B</del>	<del>ZTA02 40</del>
I1=I1B	ZTA02 41
I0=I0B	ZTA02 42
K4=K4B	ZTA02 43
K2=K2B	ZTA02 44
K1=K1B	ZTA02 45
<del>K0=K0B</del>	<del>ZTA02 46</del>
L3=L3B	ZTA02 47
L2=L2B	ZTA02 48
<del>L1=L1B</del>	<del>ZTA02 49</del>
L0=L0B	ZTA02 50
AP=(A4*ET4+A2*ET2+A0)*P03	ZTA02 51
<del>BP=(B3*ET3+B1*E)*P02*P1</del>	<del>ZTA02 52</del>
CP=(C2*ET2+C0)*P0*P12	ZTA02 53
DP=(D3*ET3+D1*E)*P13	ZTA02 54
SQRT2E=SQRT(2.0)*E	ZTA02 55
SQRT3E=SQRT(3.0)*E	ZTA02 56
EP=(E4*ET4+E2*ET2+E0)*PHI0(SQRT3E)	ZTA02 57
<del>FP=F0*PHI0(SQRT2E)*P1</del>	<del>ZTA02 58</del>

$GP = (G4 * ET4 + G2 * ET2 + G1 * E + G0) * P02$   
 $HP = (H3 * ET3 + H2 * ET2 + H1 * E + H0) * P0 * P1$   
 $IP = (I2 * ET2 + I1 * E + I0) * P12$   
 $KP = (K4 * ET4 + K2 * ET2 + K1 * E + K0) * P0$   
 $LP = (L3 * ET3 + L2 * ET2 + L1 * E + L0) * P1$   
 $ZTA02B1 = AP + BP + CP + DP + EP + FP + GP + HP + IP + KP + LP$   
 RETURN  
 END

ZTA02 59  
 ZTA02 60  
 ZTA02 61  
 ZTA02 62  
 ZTA02 63  
 ZTA02 64  
 ZTA02 65  
 ZTA02 66

## APPENDIX II

### CANNED SUBROUTINE LISTINGS - CADRE

- SECOND
- SPLINE, ARITH1
- TRID

FUNCTION CADRE(F,A,B,AERR,RERR,LEVEL,ERROR,IFLAG)	CADRE 1
C THIS FUNCTION RETURNS AN ESTIMATE *CADRE* FOR THE NUMBER	CADRE 2
C INT = INTEGRAL OF *F*(X) FROM *A* TO *B*	CADRE 3
C WHICH HOPEFULLY SATISFIES	CADRE 4
C ABS(INT - *CADRE*) .LE. AMAX1(*AERR*, *RERR* TIMES ABS(INT)).	CADRE 5
C THE PROGRAM USES CAUTIOUS ADAPTIVE ROMBERG EXTRAPOLATION.	CADRE 6
C IN THIS SCHEME, THE INTEGRAL IS CALCULATED AS THE SUM OF INTEGRALS	CADRE 7
C OVER SUITABLY SMALL SUBINTERVALS. ON EACH SUBINTERVAL, AN ESTIMATE	CADRE 8
C *VINT*, WITH ESTIMATED ABSOLUTE ERROR *ERRER*, IS FOUND BY CAUTIOUS	CADRE 9
C ROMBERG EXTRAPOLATION. IF *ERRER* IS SMALL ENOUGH, *VINT* IS ACCEPT	CADRE 10
C ED AND ADDED TO *CADRE*, AND *ERRER* IS ADDED TO *ERROR*. OTHERWISE	CADRE 11
C THE SUBINTERVAL IS HALVED, AND EACH HALF IS CONSIDERED SEPARATELY.	CADRE 12
C INFORMATION ABOUT THE OTHER HALF BEING TEMPORARILY STACKED.	CADRE 13
C	CADRE 14
C ***** INPUT *****	CADRE 15
C	CADRE 16
C F THE NAME OF A SINGLE-ARGUMENT REAL FUNCTION SUBPROGRAM	CADRE 17
C THIS NAME MUST APPEAR IN THE CALLING PROGRAM IN AN	CADRE 18
C EXTERNAL STATEMENT.	CADRE 19
C A,B THE TWO ENDPOINTS OF THE INTERVAL OF INTEGRATION	CADRE 20
C AERR DESIRED ABSOLUTE AND RELATIVE ERROR IN THE ANSWER	CADRE 21
C RERR AN INTEGER INDICATING DESIRED LEVEL OF PRINTOUT	CADRE 22
C LEVEL	CADRE 23
C .LE. 1, NO PRINTOUT,	CADRE 24
C = 2, SUCCESS OR FAILURE MESSAGE, AND LIST OF SINGULAR-	CADRE 25
C ITIES ENCOUNTERED (IF ANY).	CADRE 26
C = 3, IN ADDITION, ALL SUBINTERVALS CONSIDERED ARE LISTED	CADRE 27
C TOGETHER WITH THE KIND OF REGULAR BEHAVIOUR FOUND	CADRE 28
C (IF ANY),	CADRE 29
C = 4, IN ADDITION, ALL RATIOS CONSIDERED ARE LISTED AS IS	CADRE 30
C INFO ON WHICH DECISION PROCEDURE IS BASED,	CADRE 31
C .GE. 5, IN ADDITION, ALL T-TABLES ARE LISTED.	CADRE 32
C	CADRE 33
C ***** OUTPUT *****	CADRE 34
C	CADRE 35
C CADRE ESTIMATE OF THE INTEGRAL, RETURNED VIA THE FUNCTION CALL.	CADRE 36
C ERROR ESTIMATED BOUND ON THE ABSOLUTE ERROR OF THE NUMBER *CADRE*	CADRE 37
C IFLAG AN INTEGER BETWEEN 1 AND 5 INDICATING WHAT DIFFICULTIES	CADRE 38
C WERE MET WITH: SPECIFICALLY	CADRE 39
C = 1, ALL IS WELL.	CADRE 40
C = 2, ONE OR MORE SINGULARITIES WERE SUCCESSFULLY HANDLED.	CADRE 41
C = 3, IN SOME SUBINTERVAL(S), THE ESTIMATE *VINT* WAS ACCEPT	CADRE 42
C ED MERELY BECAUSE *ERRER* WAS SMALL, EVEN THOUGH NO	CADRE 43
C REGULAR BEHAVIOUR COULD BE RECOGNIZED.	CADRE 44
C = 4, FAILURE, OVERFLOW OF STACK *TS* (THIS HAS NEVER HAPPEN	CADRE 45
C ED, - SO FAR).	CADRE 46
C = 5, FAILURE, TOO SMALL A SUBINTERVAL IS REQUIRED; THIS MAY	CADRE 47
C BE DUE TO TOO MUCH NOISE IN THE FUNCTION (RELATIVE TO	CADRE 48
C THE GIVEN ERROR REQUIREMENTS) OR DUE TO A PLAIN ORNERY	CADRE 49
C INTEGRAND.	CADRE 50
C A VERY CAUTIOUS MAN WOULD ACCEPT *CADRE* ONLY IF IFLAG IS 1 OR 2;	CADRE 51
C THE MERELY REASONABLE MAN WOULD KEEP THE FAITH EVEN IF IFLAG IS 3.	CADRE 52
C THE ADVENTUROUS MAN IS QUITE OFTEN RIGHT IN ACCEPTING *CADRE*	CADRE 53
C EVEN IF IFLAG IS 4 OR 5.	CADRE 54
C	CADRE 55
C ***** LIST OF MAJOR VARIABLES *****	CADRE 56
C	CADRE 57
C CUREST BEST ESTIMATE SO FAR FOR	CADRE 58
C INT - (INTEGRAL OVER CURRENTLY CONSIDERED SUBINTERVAL).	CADRE 59
C FNSIZE MAXIMUM AVERAGE FUNCTION SIZE SO FAR ENCOUNTERED,	CADRE 60

C	ERRR	RELATIVE ERROR REQUIREMENT USED; DERIVED FROM INPUT *PERR*	CADRF 61
C		AND CHOSEN TO LIE BETWEEN .1 AND 10 TIMES *TOLMCH*.	CADRF 62
C	ERRA	= ABS(*AERR*)	CADRF 63
C	STAGE	(MORE OR LESS) EQUAL TO 2 TO THE -(*ISTAGE*)	CADRF 64
C		THESE FIVE QUANTITIES ARE USED IN THE DETERMINATION OF THE LOCAL	CADRF 65
C		ERROR REQUIREMENT.	CADRF 66
C			CADRF 67
C	STEPMN	MINIMUM SUBINTERVAL LENGTH PERMITTED.	CADRF 68
C	TS	STACK OF VALUES OF F(X) SO FAR COMPUTED BUT NOT YET	CADRF 69
C		SUCCESSFULLY USED.	CADRF 70
C	ISTAGE	AN INTEGER INDICATING THE HEIGHT OF THE STACK OF INTERVALS	CADRF 71
C		YET TO BE PROCESSED.	CADRF 72
C			CADRF 73
C	*****	LIST OF PARAMETERS *****	CADRF 74
C			CADRF 75
C	TOLMCH	DEPENDS ON THE LENGTH OF FLOATING POINT MANTISSA; SHOULD BE	CADRF 76
C		ABOUT 1.E-7 FOR 27 BINARY BIT MANTISSA AND	CADRF 77
C		ABOUT 1.E-13 FOR 48 BINARY BIT MANTISSA.	CADRF 78
C	AITLOW	SHOULD BE SOMEWHAT GREATER THAN 1.	CADRF 79
C	H2TOL.		CADRF 80
C	AITTOL.		CADRF 81
C	JUMPTL	TOLERANCES USED IN THE DECISION PROCESS TO RECOGNIZE	CADRF 82
C		H**2 CONVERGENCE, X**ALPHA TYPE CONVERGENCE, OR	CADRF 83
C		JUMP-TYPE CONVERGENCE OF THE TRAPEZOID SUMS.	CADRF 84
C	MAXTS.		CADRF 85
C	MAXTBL.		CADRF 86
C	MXSTGE	ARE THE THREE DIFFERENT UPPER LIMITS FOR THE DIMENSION OF	CADRF 87
C		THE VARIOUS ARRAYS.	CADRF 88
C			CADRF 89
C	*****	PROGRAM LAYOUT *****	CADRF 90
C			CADRF 91
C		INITIALIZATION	CADRF 92
C	5-6	BEGIN WORK ON NEXT SUBINTERVAL	CADRF 93
C	9-14	GET NEXT TRAPEZOID SUM	CADRF 94
C	15-19	GET RATIOS. PRELIMINARY DECISION PROCEDURE.	CADRF 95
C	20-	ESTIMATE *VINT* ASSUMING SMOOTH INTEGRAND	CADRF 96
C	30-	ESTIMATE *VINT* ASSUMING INTEGRAND HAS X**ALPHA TYPE	CADRF 97
C		SINGULARITY	CADRF 98
C	40-	NO LUCK WITH THIS TRAPEZOID SUM. GET NEXT ONE OR GET OUT.	CADRF 99
C	50-	ESTIMATE *VINT* ASSUMING INTEGRAND HAS JUMP	CADRF100
C	60-	ESTIMATE *VINT* ASSUMING INTEGRAND IS STRAIGHT LINE	CADRF101
C	70-	ESTIMATE *VINT* ASSUMING VARIATION IN INTEGRAND	CADRF102
C		IS MOSTLY NOISE.	CADRF103
C	80-	INTEGRATION OVER CURRENT SUBINTERVAL SUCCESSFUL.	CADRF104
C		SET UP NEXT SUBINTERVAL. IF ANY. OR RETURN.	CADRF105
C	90-	INTEGRATION OVER CURRENT SUBINTERVAL NOT SUCCESSFUL.	CADRF106
C		MARK CURRENT SUBINTERVAL FOR SUBDIVISION AND SET UP	CADRF107
C		NEXT SUBINTERVAL.	CADRF108
C	900-	FAILURE.	CADRF109
C			CADRF110
C		DIMENSION T(10,10),R(10),AIT(10),DIF(10),RN(4),	CADRF111
C	*	TS(2049),IBEGS(30),BEGIN(30),FINIS(30),EST(30)	CADRF112
C		REAL LENGTH, JUMPTL	CADRF113
C		LOGICAL H2CCNV,AITKEN,RIGHT,REGLAR,REGLSV(30)	CADRF114
C		DATA TOLMCH,AITLOW,H2TCL,AITTOL,JUMPTL,MAXTS,MAXTBL,MXSTGE	CADRF115
C	*	/ 2.E-13, 1.1 , .15 , .1 , .01 , 2049, 10 , 30/	CADRF116
C		DATA RN/.71420053,.34662815,.843751..12633046/	CADRF117
C		DATA ALG402 /.3010299956639795/	CADRF118
C		CADRE = 0.	CADRF119
C		ERRCR = 0.	CADRF120
C		IFLAG = 1	CADRF121

LENGTH = ABS(B-A)	CADRE122
IF (LENGTH.EQ. 0.) RETURN	CADRE123
ERRR = AMIN1(.1,AMAX1(ABS(RERR), 10.*TOLMCH))	CADRE124
ERRA = ABS(AERR)	CADRE125
STEPMN = AMAX1(LENGTH/FLOAT(2**MXSTGE),	CADRE126
* AMAX1(LENGTH,ABS(A),ABS(B))*TOLMCH)	CADRE127
STAGE = .5	CADRE128
ISTAGE = 1	CADRE129
CUREST = 0.	CADRE130
FNSIZE = 0.	CADRE131
PREVER = 0.	CADRE132
REGLAR = .FALSE.	CADRE133
C	CADRE134
C THE GIVEN INTERVAL OF INTEGRATION IS THE FIRST INTERVAL CONSIDERED.	CADRE135
BEG = A	CADRE136
FBEG = F(BEG)/2.	CADRE137
TS(1) = FBEG	CADRE138
IBEG = 1	CADRE139
END = B	CADRE140
FEND = F(END)/2.	CADRE141
TS(2) = FEND	CADRE142
IEND = 2	CADRE143
C	CADRE144
5 RIGHT = .FALSE.	CADRE145
C	CADRE146
C INVESTIGATION OF A PARTICULAR SUBINTERVAL BEGINS AT THIS POINT.	CADRE147
C ***** MAJOR VARIABLES *****	CADRE148
C BEG,	CADRE149
C END      ENDCPOINTS OF THE CURRENT INTERVAL	CADRE150
C FBEG,	CADRE151
C FEND      ONE HALF THE VALUE OF F(X) AT THE ENDCPOINTS	CADRE152
C STEP      SIGNED LENGTH OF CURRENT SUBINTERVAL	CADRE153
C ISTAGE    HEIGHT OF CURRENT SUBINTERVAL IN STACK OF SUBINTERVALS	CADRE154
C            YET TO BE DONE	CADRE155
C RIGHT    A LOGICAL VARIABLE INDICATING WHETHER CURRENT SUBINTERVAL	CADRE156
C            IS RIGHT HALF OF PREVIOUS SUBINTERVAL. NEEDED IN 80FF AND	CADRE157
C            90FF TO DECIDE WHAT INTERVAL TO LOCK AT NEXT.	CADRE158
C TS(I), I=IBEG,...,IEND, CONTAINS THE FUNCTION VALUES FOR THIS	CADRE159
C            SUBINTERVAL SO FAR COMPUTED. SPECIFICALLY,	CADRE160
C            TS(I) = F(BEG + (I-IBEG)/(IEND-IBEG)*STEP), ALL I	CADRE161
C            EXCEPT THAT TS(IREG) = FBEG, TS(IEND) = FEND	CADRE162
C REGLAR    A LOGICAL VARIABLE INDICATING WHETHER OR NOT THE CURRENT	CADRE163
C            SUBINTERVAL IS REGULAR (SEE NOTES)	CADRE164
C H2CONV    A LOGICAL VARIABLE INDICATING WHETHER H**2 CONVERGENCE OF	CADRE165
C            THE TRAPEZOID SUMS FOR THIS INTERVAL IS RECOGNIZED,	CADRE166
C AITKEN    A LOGICAL VARIABLE INDICATING WHETHER CONVERGENCE OF RATIOS	CADRE167
C            FOR THIS SUBINTERVAL IS RECOGNIZED	CADRE168
C T            CONTAINS THE FIRST *L* ROWS OF THE ROMBERG T-TABLE FOR THIS	CADRE169
C            SUBINTERVAL IN ITS LOWER TRIANGULAR PART. SPECIFICALLY,	CADRE170
C            T(I,1) = TRAPEZOID SUM (WITHOUT THE FACTOR *STEP*)	CADRE171
C            ON 2**(I-1) + 1 EQUISPACED POINTS, I=1,...,L,	CADRE172
C            T(I,J+1) = T(I,J) + (T(I,J)-T(I-1,J))/(4**J - 1),	CADRE173
C            J=2,...,I-1, I=2,...,L.	CADRE174
C            FURTHER, THE STRICTLY UPPER TRIANGULAR PART OF T CONTAINS	CADRE175
C            THE RATIOS FOR THE VARIOUS COLUMNS OF THE T-TABLE.	CADRE176
C            SPECIFICALLY,	CADRE177
C            T(J,I) = (T(I,J)-T(I-1,J))/(T(I+1,J)-T(I,J)),	CADRE178
C            I=J+1,...,L-1, J=1,...,L-2.	CADRE179
C            FINALLY, THE LAST OR L-TH COLUMN CONTAINS	CADRE180
C            T(J,L) = T(L,J) - T(L-1,J), J=1,...,L-1.	CADRE181
C 6 STEP = END - BEG	CADRE182

<pre> ASTEP = ABS(STEP) IF (ASTEP .LT. STEP*NN)      GO TO 950 IF (LEVEL .GE. 3) WRITE(6,609) BEG,STEP,ISTAGE 609 FORMAT(10H BEG,STEP ,2E16.8,1X) T(1,1) = FBEG + FEND TABS = ABS(FBEG) + ABS(FEND) L = 1 N = 1 H2CONV = .FALSE. AITKEN = .FALSE.  GO TO 10  C 9 IF (LEVEL .GE. 4) WRITE(6,692) L,T(1,LM1) 10 LM1 = L L = L + 1  C CALCULATE THE NEXT TRAPEZOID SUM. T(L,1), WHICH IS BASED ON C *N2* + 1 EQUISPACED POINTS. HERE. N2 = N*2 = 2**(L-1) . N2 = N*2 FN = N2 ISTEP = (IEND - IBEG)/N IF (ISTEP .GT. 1)      GO TO 12 II = IEND IEND = IEND + N IF (IEND .GT. MAXTS)   GO TO 900 HCVN = STEP/FN III = IEND DO 11 I=1,N2,2 TS(III) = TS(II) TS(III-1) = F(END - FLOAT(I)*HCVN) III = III-2 11 II = II-1 ISTEP = 2 12 ISTEP2 = IBEG + ISTEP/2 SUM = 0. SUMABS = 0. DO 13 I=ISTEP2,IEND,ISTEP SUM = SUM + TS(I) 13 SUMABS = SUMABS + ABS(TS(I)) T(L,1) = T(L-1,1)/2. + SUM/FN TABS = TABS/2. + SUMABS/FN ABSI = ASTEP*TABS N = N2  C C GET PRELIMINARY VALUE FOR *VINT* FROM LAST TRAPEZOID SUM AND C UPDATE THE ERROR REQUIREMENT *ERGOAL* FOR THIS SUBINTERVAL. C THE ERROR REQUIREMENT IS NOT PRORATED ACCORDING TO THE LENGTH OF C THE CURRENT SUBINTERVAL RELATIVE TO THE INTERVAL OF INTEGRATION, C BUT ACCORDING TO THE HEIGHT *ISTAGE* OF THE CURRENT SUBINTERVAL C IN THE STACK OF SUBINTERVALS YET TO BE DONE. C THIS PROCEDURE IS NOT HACKED BY ANY RIGOROUS ARGUMENT, BUT C SEEMS TO WORK. IT = 1 VINT = STEP*T(L,1) TABTLM = TABS*TOLMCH FN SIZE = AMAX1(FN SIZE,ABS(T(L,1))) ERGOAL = AMAX1(ASTEP*TOLMCH*FN SIZE, * STAGE*AMAX1(ERRA,ERRR*ABS(CUREST+VINT)))  C COMPLETE ROW L AND COLUMN L OF *T* ARRAY. FEXTRP = 1. </pre>	<pre> CADRE183 CADRE184 CADRE185 CADRE186 CADRE187 CADRE188 CADRE189 CADRE190 CADRE191 CADRE192 CADRE193 CADRE194 CADRE195 CADRE196 CADRE197 CADRE198 CADRE199 CADRE200 CADRE201 CADRE202 CADRE203 CADRE204 CADRE205 CADRE206 CADRE207 CADRE208 CADRE209 CADRE210 CADRE211 CADRE212 CADRE213 CADRE214 CADRE215 CADRE216 CADRE217 CADRE218 CADRE219 CADRE220 CADRE221 CADRE222 CADRE223 CADRE224 CADRE225 CADRE226 CADRE227 CADRE228 CADRE229 CADRE230 CADRE231 CADRE232 CADRE233 CADRE234 CADRE235 CADRE236 CADRE237 CADRE238 CADRE239 CADRE240 CADRE241 CADRE242 CADRE243 </pre>
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DO 14 I=1,LM1
  FEXTRP = FEXTRP*4.
  T(I,L) = T(L,I) - T(L-1,I)
14 T(L,I+1) = T(L,I) + T(I,L)/(FEXTRP-1.)
  ERROR = ASTEP*ABS(T(1,L))
C-----
C--- PRELIMINARY DECISION PROCEDURE -----
C
C IF L = 2 AND T(2,1) = I(1,1), GO TO 60 TO FOLLOW UP THE IMPRESSION
C THAT INTEGRAND IS STRAIGHT LINE.
  IF (L .GT. 2) GO TO 15
  IF (ABS(I(1,2)) .LE. TABTLM) GO TO 60
  GO TO 10
C
C CALCULATE NEXT RATIOS FOR COLUMNS 1,...,L-2 OF T-TABLE
C RATIO IS SET TO ZERO IF DIFFERENCE IN LAST TWO ENTRIES OF
C COLUMN IS ABOUT ZERO.
15 DO 16 I=2,LM1
  DIFF = 0.
  IF (ABS(T(I-1,L)) .GT. TABTLM) DIFF = T(I-1,LM1)/T(I-1,L)
16 T(I-1,LM1) = DIFF
C
C T(1,LM1) IS THE RATIO DERIVED FROM LAST THREE TRAPEZOID SUMS, I.E.,
C  $T(1,LM1) = (T(L-1,1) - T(L-2,1)) / (T(L,1) - T(L-1,1))$ 
C IF THIS RATIO IS ABOUT 4, GO TO 26 FOR ROMBERG EXTRAPOLATION.
C IF THIS RATIO IS ZERO, I.E., IF LAST TWO TRAPEZOID SUMS ARE ABOUT
C EQUAL, GO TO 18 FOR POSSIBLE NOISE CHECK.
C IF THIS RATIO IS ABOUT 2 IN ABSOLUTE VALUE, GO TO 50 WITH THE
C BELIEF THAT INTEGRAND HAS JUMP DISCONTINUITY.
C IF THIS RATIO IS, AT LEAST, ABOUT EQUAL TO THE PREVIOUS RATIO, THEN
C THE INTEGRAND MAY WELL HAVE A NICE INTEGRABLE SINGULARITY.
C GO TO 30 TO FOLLOW UP THIS HUNCH.
  IF (ABS(4.-T(1,LM1)) .LE. H2TOL) GO TO 20
  IF (T(1,LM1) .EQ. 0.) GO TO 18
  IF (ABS(2.-ABS(T(1,LM1))) .LT. JUMPTL) GO TO 50
  IF (L .EQ. 3) GO TO 9
  H2CONV = .FALSE.
  IF (ABS((T(1,LM1)-T(1,L-2))/T(1,LM1)) .LE. AITTOL)
    * GO TO 30
C AT THIS POINT, NO REGULAR BEHAVIOUR WAS DETECTED.
C IF CURRENT SUBINTERVAL IS NOT REGULAR AND ONLY FOUR TRAPEZOID SUMS
C WERE COMPUTED SO FAR, TRY ONE MORE TRAPEZOID SUM.
C IF, AT LEAST, LAST TWO TRAPEZOID SUMS ARE ABOUT EQUAL, THEN
C FAILURE TO RECOGNIZE REGULAR BEHAVIOUR MAY WELL BE DUE TO NOISE.
C GO TO 70 TO CHECK THIS OUT.
C OTHERWISE, GO TO 90 FOR FURTHER SUBDIVISION.
C
17 IF (REGLAR) GO TO 18
  IF (L .EQ. 4) GO TO 9
18 IF (ERROR .LE. ERGOAL) GO TO 70
  IF (LEVEL .GE. 4) WRITE (A,695) L,T(1,LM1)
  GO TO 91
C-----
C--- CAUTIOUS ROMBERG EXTRAPOLATION -----
C
C THE CURRENT, OR L-TH, ROW OF THE ROMBERG T-TABLE HAS L ENTRIES.
C FOR J=1,...,L-2, THE ESTIMATE
C  $STEP * T(L, J+1)$ 
C IS BELIEVED TO HAVE ITS ERROR BOUNDED BY
C  $ABS(STEP * (T(L, J) - T(L-1, J)) / (4 ** J - 1))$ 
C IF THE LAST RATIO

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C      T(J,LM1) = (T(L-1,J)-T(L-2,J))/(T(L,J)-T(L-1,J))
C FOR COLUMN J OF THE T-TABLE IS ABOUT 4**J.
C THE FOLLOWING IS A SLIGHTLY RELAXED EXPRESSION OF THIS BEHAVIOR.
20 IF (LEVEL .GE. 4) WRITE (6,619) L,T(1,LM1)
619 FORMAT(15,E16.8,5X6H2CONV)
    IF (H2CONV) GO TO 21
    AITKEN = .FALSE.
    H2CONV = .TRUE.
    IF (LEVEL .GE. 3) WRITE (4,620) L
620 FORMAT(22H F2 CONVERGENCE AT ROW,13)
21 FEXTRP = 4.
22 IT = IT + 1
    VINT = STEP*T(L,IT)
    ERROR = ABS(STEP/(FEXTRP-1.)*T(IT-1,L))
    IF (ERROR .LE. ERGOAL) GO TO 20
    IF (IT .EQ. LM1) GO TO 40
    IF (T(IT,LM1) .EQ. 0.) GO TO 22
    IF (T(IT,LM1) .LE. FEXTRP) GO TO 40
    IF (ABS(T(IT,LM1)/4.-FEXTRP)/FEXTRP .LT. AITTOL)
      * FEXTRP = FEXTRP*4.
      GO TO 22
C-----
C--- INTEGRAND MAY HAVE X**ALPHA TYPE SINGULARITY-----
C RESULTING IN A RATIO OF *SING* = 2** (ALPHA + 1)
30 IF (LEVEL .GE. 4) WRITE (6,629) L,T(1,LM1)
629 FORMAT(15,E16.8,5X6H2CONV)
    IF (T(1,LM1) .LT. AITLOW) GO TO 91
    IF (AITKEN) GO TO 31
    H2CONV = .FALSE.
    AITKEN = .TRUE.
    IF (LEVEL .GE. 3) WRITE (4,630) L
630 FORMAT(14H AITKEN AT ROW,13)
31 FEXTRP = T(L-2,LM1)
    IF (FEXTRP .GT. 4.5) GO TO 21
    IF (FEXTRP .LT. AITLOW) GO TO 91
    IF (ABS(FEXTRP-T(L-3,LM1))/T(1,LM1) .GT. H2TOL)
      * GO TO 91
    IF (LEVEL .GE. 3) WRITE (6,631) FEXTRP
631 FORMAT(6H RATIO,F12.8)
    SING = FEXTRP
    FEXTM1 = FEXTRP - 1.
    DO 32 I=2,L
    AIT(I) = T(I,1) + (T(I,1)-T(I-1,1))/FEXTM1
    R(I) = T(1,I-1)
32 DIF(I) = AIT(I) - AIT(I-1)
    IT = 2
33 VINT = STEP*AIT(L)
    IF (LEVEL .LT. 5) GO TO 333
    WRITE (6,632) (R(I+1),I=IT,LM1)
    WRITE (6,632) (AIT(I),I=IT,L)
    WRITE (6,632) (DIF(I+1),I=IT,LM1)
632 FORMAT(1X,8E16.8)
333 ERROR = ERROR/FEXTM1
    IF (ERROR .GT. ERGOAL) GO TO 34
    ALPHA = ALOG10(SING)/ALOG10(2) - .5.
    IF (LEVEL .GE. 2) WRITE (4,633) ALPHA,REG,END
633 FORMAT(11X42HINTEGRAND SHOWS SINGULAR BEHAVIOR OF TYPE
      * 4HX**(F4.2,9H) BETWEEN F5.8,4H AND F5.8)
    IFLAG = MAX0(IFLAG,2)
      GO TO 20
34 IT = IT + 1

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IF (IT .EG. LM1)	GO TO 40	CADRE366
IF (IT .GT. 3)	GO TO 35	CADRE367
H2NEXT = 4.		CADRE368
SINGNX = 2.*SING		CADRE369
35 IF (H2NEXT .LT. SINGNX)	GO TO 36	CADRE370
FEXTRP = SINGNX		CADRE371
SINGNX = 2.*SINGNX		CADRE372
	GO TO 37	CADRE373
36 FEXTRP = H2NEXT		CADRE374
H2NEXT = 4.*H2NEXT		CADRE375
37 DO 38 I=IT,LM1		CADRE376
R(I+1) = 0.		CADRE377
38 IF (ABS(DIF(I+1)) .GT. TABTLM) R(I+1) = DIF(I)/DIF(I+1)		CADRE378
IF (LEVEL .GE. 4) WRITE (6,63R) FEXTRP,R(L-1),R(L)		CADRE379
638 FORMAT(16H FEXTRP = ,R1105,3E15.8)		CADRE380
H2TFEX = -H2TOL*FEXTRP		CADRE381
IF (R(L) - FEXTRP .LT. H2TFEX)	GO TO 40	CADRE382
IF (R(L-1)-FEXTRP .LT. H2TFEX)	GO TO 40	CADRE383
ERRER = ASTEP*ABS(DIF(L))		CADRE384
FEXTM1 = FEXTRP - 1.		CADRE385
DO 39 I=IT,L		CADRE386
AIT(I) = AIT(I) + DIF(I)/FEXTM1		CADRE387
39 DIF(I) = AIT(I) - AIT(I-1)		CADRE388
	GO TO 33	CADRE389
C-----		
CURRENT TRAPEZOID SUM AND RESULTING EXTRAPOLATED VALUES DID NOT GIVE		
C A SMALL ENOUGH *ERRER*.		CADRE391
C IF LESS THAN FIVE TRAPEZOID SUMS WERE COMPUTED SO FAR, TRY NEXT		CADRE392
C TRAPEZOID SUM.		CADRE393
C OTHERWISE, DECIDE WHETHER TO GO ON OR TO SUBDIVIDE AS FOLLOWS.		CADRE394
C WITH T(L,IT) GIVING THE CURRENTLY BEST ESTIMATE, GIVE UP ON DEVELOP		CADRE395
C ING THE T-TABLE FURTHER IF L .GT. IT*2. I.E., IF EXTRAPOLATION		CADRE396
C DID NOT GO VERY FAR INTO THE T-TABLE.		CADRE397
C FURTHER, GIVE UP IF REDUCTION IN *ERRER* AT THE CURRENT RATE		CADRE398
C DOES NOT PREDICT AN *ERRER* LESS THAN *ERGOAL* BY THE TIME		CADRE399
C *MAXTRL* TRAPEZOID SUMS HAVE BEEN COMPUTED.		CADRE400
C ---NOTE---		CADRE401
C HAVING PREVER .LT. ERRER IS AN ALMOST CERTAIN SIGN OF BEGINNING		CADRE402
C TROUBLE WITH NOISE IN THE FUNCTION VALUES. HENCE,		CADRE403
C A WATCH FOR, AND CONTROL OF, NOISE SHOULD BEGIN HERE.		CADRE404
40 FEXTRP = AMAX1(PREVER/ERRER,ATTLOW)		CADRE405
PREVER = ERRER		CADRE406
IF (L .LT. 5)	GO TO 10	CADRE407
IF (LEVEL .GE. 3) WRITE (6,641) ERRER,ERGOAL,FEXTRP,IT		CADRE408
641 FORMAT(23H ERRER,ERGOAL,FEXTRP,IT,2E15.8,E14.5,I3)		CADRE409
IF (L-IT .GT. 2 .AND. ISTAGE .LT. MYSTGE) GO TO 90		CADRE410
IF (ERRER/FEXTRP*(MAXTRL-1) .LT. ERGOAL) GO TO 10		CADRE411
	GO TO 90	CADRE412
C-----		
C--- INTEGRAND HAS JUMP (SEE NOTES) -----		
50 IF (LEVEL .GE. 4) WRITE (6,649) L,T(1,LM1)		CADRE414
649 FORMAT(15,E16.8,5X4FJUMP)		CADRE415
IF (ERRER .GT. ERGOAL)	GO TO 90	CADRE416
C NOTE THAT 2*FN = 2*L		CADRE417
DIFF = ABS(T(1,L))*2.*FN		CADRE418
IF (LEVEL .GE. 2) WRITE (6,655) DIFF,BEG,END		CADRE419
650 FORMAT(13X36HINTEGRAND SEEMS TO HAVE JUMP OF SIZEE13.6,		CADRE420
* 8H BETWEENE15.8,4H ANDE15.8)		CADRE421
	GO TO 80	CADRE422
C-----		
C--- INTEGRAND IS STRAIGHT LINE -----		
		CADRE423
		CADRE424
		CADRE425
		CADRE426

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C TEST THIS ASSUMPTION BY COMPARING THE VALUE OF THE INTEGRAND AT
C FOUR *RANDOMLY CHOSEN* POINTS WITH THE VALUE OF THE STRAIGHT LINE
C INTERPOLATING THE INTEGRAND AT THE TWO ENDPOINTS OF THE SUB-
C INTERVAL. IF TEST IS PASSED, ACCEPT *VINT*.
60 IF (LEVEL .GE. 4) WRITE (6,666) L
660 FORMAT(15,21X13HSTRAIGHT LINE)
    SLOPE = (FEND-FBEG)*2.
    FBEG2 = FBEG*2.
    DO 61 I=1,4
    DIFF = ABS(F(REG+RN(I)*STEP) - FBEG2-RN(I)*SLOPE)
    IF (DIFF .GT. TARTLM) GO TO 72
61 CONTINUE
    IF (LEVEL .GE. 3) WRITE (6,667) REG, END
667 FORMAT(27X43HINTEGRAND SEEMS TO BE STRAIGHT LINE BETWEEN
    * E15.8,4H AND E15.8)
    GO TO 80
C-----
C----- NOISE MAY BE DOMINANT FEATURE -----
C ESTIMATE NOISE LEVEL BY COMPARING THE VALUE OF THE INTEGRAND AT
C FOUR *RANDOMLY CHOSEN* POINTS WITH THE VALUE OF THE STRAIGHT LINE
C INTERPOLATING THE INTEGRAND AT THE TWO ENDPOINTS. IF SMALL
C ENOUGH, ACCEPT *VINT*.
70 IF (LEVEL .GE. 4) WRITE (6,670) L,T(1,LM1)
670 FORMAT(15,E16.8,5X5HNOISE)
    SLOPE = (FEND-FBEG)*2.
    FBEG2 = FBEG*2.
    I = 1
71 DIFF = ABS(F(REG+RN(I)*STEP) - FBEG2-RN(I)*SLOPE)
72 ERROR = AMAX1(ERROR,ASTEP*DIFF)
    IF (ERROR .GT. ERGOAL) GO TO 91
    I = I+1
    IF (I .LE. 4) GO TO 71
    IF (LEVEL .GE. 3) WRITE (6,671) REG,END
671 FORMAT(15H NOISE BETWEEN ,E15.8,4H AND,E15.8)
    IFLAG = 3
C-----
C--- INTEGRATION OVER CURRENT SUBINTERVAL SUCCESSFUL -----
C ADD *VINT* TO *CADRE* AND *ERROR* TO *ERROR*, THEN SET UP NEXT
C SUBINTERVAL, IF ANY.
80 CADRE = CADRE + VINT
    ERROR = ERROR + ERREF
    IF (LEVEL .LT. 3) GO TO 83
    IF (LEVEL .LT. 5) GO TO 82
    DO 81 I=1,L
81 WRITE (6,692) I,(T(I,J),J=1,L)
82 WRITE (6,682) VINT,ERROR,L,IT
682 FORMAT(12H INTEGRAL IS,E16.8,7H, ERROR,E15.8,9H FROM T(,
    * I1.1H,,I1,jH))
C
83 IF (RIGHT) GO TO 85
    ISTAGE = ISTAGE + 1
    IF (ISTAGE .EQ. 0) RETURN
C
    REGLAR = REGLSV(ISTAGE)
    BEG = BEGIN(ISTAGE)
    END = FINIS(ISTAGE)
    CUREST = CUREST - EST(ISTAGE+1) + VINT
    IEND = IBEG + 1
    FEND = IS(IEND)
    IBEG = IBEGS(ISTAGE)
    GO TO 94

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85 CUREST = CUREST + VINT		CADRE488
STAGE = STAGE*2.		CADRE489
IEND = IBEG		CADRE490
IBEG = IBEGS(ISTAGE)		CADRE491
END = BEG		CADRE492
BEG = BEGIN(ISTAGE)		CADRE493
FEND = FBEG		CADRE494
FBEG = TS(IBEG)		CADRE495
	GO TO 5	CADRE496
C-----		CADRE497
C--- INTEGRATION OVER CURRENT SUBINTERVAL IS UNSUCCESSFUL-----		CADRE498
C MARK SUBINTERVAL FOR FURTHER SUBDIVISION. SET UP NEXT SUBINTERVAL.		CADRE499
90 REGLAR = .TRUE.		CADRE500
91 IF (ISTAGE .GE. MXSTGE)	GO TO 950	CADRE501
IF (LEVEL .LT. 5)	GO TO 93	CADRE502
DO 92 I=1,L		CADRE503
92 WRITE (6,692) I, (T(I,J), J=1,L)		CADRE504
692 FORMAT(15,7E16.8/3E16.8)		CADRE505
93 IF (RIGHT)	GO TO 95	CADRE506
REGLSV(ISTAGE+1) = REGLAR		CADRE507
BEGIN(ISTAGE) = BEG		CADRE508
IBEGS(ISTAGE) = IBEG		CADRE509
STAGE = STAGE/2.		CADRE510
94 RIGHT = .TRUE.		CADRE511
BEG = (BEG+END)/2.		CADRE512
IBEG = (IBEG+IEND)/2		CADRE513
TS(IBEG) = TS(IBEG)/2.		CADRE514
FBEG = TS(IBEG)		CADRE515
	GO TO 6	CADRE516
95 NNLEFT = IBEG - IBEGS(ISTAGE)		CADRE517
IF (IEND+NNLEFT .GE. MAXTS)	GO TO 900	CADRE518
III = IBEGS(ISTAGE)		CADRE519
II = IEND		CADRE520
DO 96 I=III,IBEG		CADRE521
II = II + 1		CADRE522
96 TS(II) = TS(I)		CADRE523
DO 97 I=IBEG,II		CADRE524
TS(III) = TS(I)		CADRE525
97 III = III + 1		CADRE526
IEND = IEND + 1		CADRE527
IBEG = IEND - NNLEFT		CADRE528
FEND = FBEG		CADRE529
FBEG = TS(IBEG)		CADRE530
FINIS(ISTAGE) = END		CADRE531
END = BEG		CADRE532
BEG = BEGIN(ISTAGE)		CADRE533
BEGIN(ISTAGE) = END		CADRE534
REGLSV(ISTAGE) = REGLAR		CADRE535
ISTAGE = ISTAGE + 1		CADRE536
REGLAR = REGLSV(ISTAGE)		CADRE537
EST(ISTAGE) = VINT		CADRE538
CUREST = CUREST + EST(ISTAGE)		CADRE539
	GO TO 5	CADRE540
C-----		CADRE541
C--- FAILURE TO HANDLE GIVEN INTEGRATION PROBLEM-----		CADRE542
900 IF (LEVEL .GE. 2) WRITE (6,6900) BEG, END		CADRE543
6900 FORMAT(37H TOO MANY FUNCTION EVALUATIONS AROUND/		CADRE544
* 10X,E15.8,4H AND,E15.8)		CADRE545
IFLAG = 4		CADRE546
	GO TO 999	CADRE547
950 IFLAG = 5		CADRE548

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IF (LEVEL .LT. 2)          GO TO 999
IF (LEVEL .LT. 5)          GO TO 959
DO 958 I=1,L
958 WRITE (6,692) I,(T(I,J),J=1,L)
959 WRITE (6,695) BEG, END
6959 FORMAT(12X38HINTEGRAND SHOWS SINGULAR BEHAVIOUR OF
*      20HUNKNOWN TYPE BETWEEN E15.8,4H AND E15.8)
999 CADRE = CUREST + VINI
      RETURN
END

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IDENT	SECOND		SECON	1
ENTRY	SECOND		SECON	2
SPACE	4		SECON	3
***	SECCND	= RETURN ACCUMULATED CPU TIME IN SECONDS.	SECON	4
*	DAVID S. CODSON.	09/21/71.	SECON	5
	SPACE	4	SECON	6
***	FORTRAN	CALL.	SECON	7
*			SECON	8
*			SECON	9
*	CALL	SECOND (X)	SECON	10
*		X = VARIABLE FOR RETURN OF ACCUMULATED CPU TIME IN	SECON	11
*		SECONDS AS A REAL NUMBER ACCURATE TO	SECON	12
*		MILLISECONDS. THIS ROUTINE USES THE	SECON	13
*		*TIMEMS* REQUEST WHICH IS A NON-STANDARD	SECON	14
*		FEATURE OF THE PURDUE OPERATING SYSTEM.	SECON	15
	TITLE	SECOND = RETURN ACCUMULATED CPL TIME IN SECONDS.	SECON	16
	TITLE	MAIN PROGRAM	SECON	17
SECOND	BSSZ	1 ENTRY/EXIT	SECON	18
	TIMEMS	READ ACCUMULATED CPU TIME IN MILLISECONDS	SECON	19
	SX1	1000 DIVIDE BY 1000	SECON	20
	OX1	X1	SECON	21
	NX1	X1	SECON	22
	PX6	X6	SECON	23
	NX6	X6	SECON	24
	FX6	X6/X1	SECON	25
	SA6	B1 STORE RESULT	SECON	26
	EQ	SECOND RETURN	SECON	27
	SPACE	4	SECON	28
	END		SECON	29

C	SUBROUTINE SPLINE(NOKNOT)	***** 1
C	NONLINEAR SPLINE APPROXIMATION	SPLIN 2
C	PROGRAM WRITTEN BY CARL DE BOOR AND JOHN RICE	SPLIN 3
C	PURDUE UNIVERSITY	SPLIN 4
C	SUPPORTED BY THE NATIONAL SCIENCE FOUNDATION GP-4052,GP-7163	SPLIN 5
C	PLEASE REPORT ANY CASES OF INOPERATION TO THE AUTHORS.	SPLIN 6
C	THANKS	SPLIN 7
C	**** NUMERICAL ANALYSIS CONTROL ****	SPLIN 8
C	CONTROL PARAMETERS FUNCTION	SPLIN 9
C	ITER NO. OF SWEEPS THRU OPT	SPLIN 10
C	BD (IN OPT) IMPROVEMENT NEEDED TO REPEAT	SPLIN 11
C	EPSERR (IN SWEEP) IMPROVEMENT NEEDED TO REPEAT	SPLIN 12
C	DIST (IN OPT NEAR 30.80) KEEPS KNOTS SEPARATED	SPLIN 13
C	INDLP NO. OF PASSES THRU OPT	SPLIN 14
C	THE FOLLOWING IS THE MAIN PROGRAM FOR VARYKNOT	SPLIN 15
C	DIMENSION INFO(16)	SPLIN 16
C	COMMON INPUT SERVES AS INPUT TO FXDKNT	SPLIN 17
C	SEE FXDKNT FOR DEFINITIONS OF VARIABLES	SPLIN 18
C	COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE	SPLIN 19
C	COMMON OUTPUT SERVES AS OUTPUT FROM FXDKNT	SPLIN 20
C	SEE FXDKNT FOR DEFINITIONS OF VARIABLES	SPLIN 21
C	COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),	SPLIN 22
C	VORDL(28,2),KNCT,LMAX,INTERV	SPLIN 23
C	COMMON OTHER SERVES AS COMMUNICATION BETWEEN OPT,SWEEP AND HERE	SPLIN 24
C	LXI = NUMBER OF INTERIOR KNOTS, LXI1 = LXI+1, LXI2 = LXI+2	SPLIN 25
C	G = NUMERICAL CONTROL VARIABLE USED BETWEEN OPT AND SWEEP	SPLIN 26
C	CHANGE = DITTO	SPLIN 27
C	ERROR = CURRENT VALUE OF THE L-2 ERROR = SQUARED	SPLIN 28
C	ACC = DESIRED ACCURACY OF L-2 ERROR	SPLIN 29
C	XI(28) = ARRAY FOR KNOTS	SPLIN 30
C	COMMON/ OTHER / LXI,LXI1,LXI2,G,CHANGE,ERROR,ACC, XI(28)	SPLIN 31
C	ACC = .1 AND ITER = 4 TO 8 SEEM TO BE GOOD VALUES FOR TYPICAL USES	SPLIN 32
C	ACC = .1	SPLIN 33
C	ITER = 8	SPLIN 34
C	***INFO IS SIMPLY AN IDENTIFICATION OF THE DATA***	SPLIN 35
C	READ IN NO. OF POINTS=LX AND THE DATA XX AND U	SPLIN 36
C	*** IF NOKNOT.GE.2, THEN READ IN LXI2=NOKNOT KNOTS***	SPLIN 37
C	*** OTHERWISE PROGRAM CHOOSES LXI2 =NOKNOT EQUISPACED KNOTS ***	SPLIN 38
C	LXI2 = IABS(NOKNOT)	SPLIN 39
C	IF *NOKNOT* IS .GT. 2, READ IN NOKNOT KNOTS (INCL.BOUNDARY POINTS.)	SPLIN 40
C	601 FORMAT(6F12.6)	SPLIN 41
C	***CHECK ON GIVEN DATA	SPLIN 42
C	AND FROM PRESENTING UNORDERED XX ARRAY	SPLIN 43
C	IERROR = 0	SPLIN 44
C	IF (LX .GE. LXI2+2 .AND. LX .LE. 100) GO TO 3	SPLIN 45
C	WRITE(6,662) LX	SPLIN 46
C	IERROR = 1	SPLIN 47
C	GO TO 7	SPLIN 48
C	3 IF (LXI2 .GE. 3 .AND. LXI2 .LE. 28) GO TO 4	SPLIN 49
C	WRITE(6,660) NOKNOT	SPLIN 50



	IERROR = 1	SPLIN 67
4	DO 6 L=2,LX	SPLIN 68
	IF (XX(L)-XX(L-1)) 5,6,6	SPLIN 69
5	WRITE(6,664) L,XX(L),U(L)	SPLIN 70
	IERROR = IERROR + 1	SPLIN 71
6	CONTINUE	SPLIN 72
	IF (IERROR .LT. 1) GO TO 14	SPLIN 73
7	WRITE(6,666) IERROR	SPLIN 74
	STOP	**** 2
C		SPLIN 76
C	**INITIALIZE	SPLIN 77
14	IF (NOKNOT .GT. 0) GO TO 30	SPLIN 78
C		SPLIN 79
C	WHEN NOKNOT IS NEG., INTRODUCE -NOKNOT EQUISPACED KNOTS	SPLIN 80
	XI(1) = XX(1)	SPLIN 81
	XI(LXI2) = XX(LX)	SPLIN 82
	DEL = (XX(LX) - XX(1))/FLOAT(LXI2-1)	SPLIN 83
	DO 26 J = 3,LXI2	SPLIN 84
26	XI(J-1) = XI(J-2) + DEL	SPLIN 85
C		SPLIN 86
C	SET UP INITIAL APPROXIMATION	SPLIN 87
30	ADDXI(1) = XI(1)	SPLIN 88
	ADDXI(2) = XI(LXI2)	SPLIN 89
	LXI1 = LXI2-1	SPLIN 90
	LXI = LXI1-1	SPLIN 91
	MODE = 0	SPLIN 92
	JADD = LXI2	SPLIN 93
	DO 35 J = 3,LXI2	SPLIN 94
35	ADDXI(J) = XI(J-1)	SPLIN 95
	ERROR = FXDKNT(0)	SPLIN 96
C	***NOTE. MODE HAS BEEN SET EQUAL TO 1	SPLIN 97
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN 98
	WRITE(6,611) (L,XX(L),U(L),L=1,LX)	SPLIN 99
	WRITE(6,612) NOKNOT,ITER	SPLIN100
	WRITE(6,900) (XI(I), I=1,LXI2)	SPLIN101
900	FORMAT(28H KNOTS PRIOR TO OPTIMIZATION/(9F12.6))	SPLIN102
C		SPLIN103
C	OPTIMIZE KNOTS	SPLIN104
	CALL SWEEP(ITER)	SPLIN105
C		SPLIN106
	WRITE(6,640)	SPLIN107
640	FORMAT(49X,22H*** FINAL OUTPUT ***/))	SPLIN108
	MODE = 1	SPLIN109
	JADD = 0	SPLIN110
	DUMB = FXDKNT(1)	SPLIN111
	RETURN	***** 3
C		SPLIN114
610	FORMAT(2I4, / (9F12.8))	SPLIN115
611	FORMAT(11H GIVEN DATA// (I4,2F14.8))	SPLIN116
612	FORMAT(1H /32H NO. OF INITIAL KNOTS = I3/	SPLIN117
1	7H ITER = I3)	SPLIN118
660	FORMAT(32H KNOT CONTROL PARAMETER NOKNOT = I3,19H NOT WITHIN BOUNDS	SPLIN119
*)		SPLIN120
662	FORMAT(26H NO. OF DATA POINTS, LX = I4,44H NO1 WITHIN THE BOUNDS	SPLIN121
*)	BS(NCKNOT)*2 AND 100)	SPLIN122
664	FORMAT(12H DATA POINT I4,2F14.8,24H NOT IN ASCENDING ORDER.)	SPLIN123
666	FORMAT(23H *** CORRECT INDICATED I3,28H INPUT ERROR(S) AND RESTART	SPLIN124
*)		SPLIN125

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SUBROUTINE SWEEP(I TRR)
C
C   KVARy.i = INDEX OF KNOT      BEING VARIED
C   SUBROUTINE OPT(I) OPTIMIZES ITH INTERIOR KNOT
C
COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE
COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),
*   VORDL(28,2),KNCT,LMAX,INTERV
COMMON/ OTHER / LXI,LXI1,LXI2,C,CHANGE,ERROR,ACC,   XI(28)
C   AT ALL TIMES, ERROR CONTAINS (L2 ERROR)**2 OF CURRENT B.A.
C
C   ITER = I TRR
C   **NEXT      CARDS SET NUMERICAL ANALYSIS CONTROLS
C   EPSERR =   ACC/2.5
C   CHANGE = .4*FLOAT(LXI)
C
10 KVARy = LXI
C   Q = CHANGE/FLOAT(LXI)
C   *** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***
C*** WRITE (6,902) ITER,Q
C*902 FORMAT (8H ITER, Q, I5,E20.8)
C   CHANGE = 0.
C   PREVER = ERROR
C   MODE = 2
C   JADD = 0
C   KNCT = KNCT - 1
C   DUMB = FXDKNT(0)
C   20 CONTINUE
C   *** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***
C*** WRITE (6,900) KVARy
C*+00 FORMAT (1H ///8H VARYING, I4, 16H ITH INTERIOR KNOT)
C*** WRITE (6,901) ERROR
C*901 FORMAT (16H SQ. OF L2-ERROR, E16.6)
C
C   CALL OPT(KVARy)
C   KVARy = KVARy - 1
C   JADD = JADD + 1
C   IF (JADD .LE. 1 )      GO TO 22
C   K = JADD
C   DO 21 I = 2, JADD
C   K = K + 1
C   21 ADDXI(K+1) = ADDXI(K)
C   22 ADDXI(1) = XI(KVARy + 2)
C   KNCT = LXI1 - JADD
C   MODE = 2
C   DUMB = FXDKNT(0)
C   IF ( KVARy .NE. 0 )      GO TO 20
C   THE LAST CALL TO FXDKNT PRODUCES THE B.A. USING ALL KNOTS.
C   SINCE THEN ADDXI CONTAINS ALL KNOTS
C   ERROR = DUMB
C   *** THE FOLLOWING TWO CARDS PRODUCE PRINTED OUTPUT OF L1,L2,L-INF
C** JADD = 0
C** DUMB = FXDKNT(2)
C
C   **IF CHANGE IN ERROR IS BIG ENOUGH MAKE ANOTHER SWEEP, ELSE QUIT
C   IF (PREVER-ERROR .LE. EPSERR*PREVER)      GO TO 60
C   ITER = ITER+1

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C	**CHECK NUMBER OF PASSES THROUGH SWEEP	SPLIN188
	IF(ITER.EQ.0) GO TO 40	SPLIN189
	GO TO 10	SPLIN190
40	CONTINUE	SPLIN191
C		SPLIN192
C	IN FINAL VERSION GO TO 40; GO TO 60 ARE REPLACED BY RETURN	SPLIN193
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN194
C***	WRITE(6,620)	SPLIN195
	RETURN	SPLIN196
60	CONTINUE	SPLIN197
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN198
C***	WRITE(6,610)	SPLIN199
	RETURN	SPLIN200
C*610	FORMAT(54H *** SWEEP DISCONTINUED - INSUFFICIENT CHANGE IN ERROR)	SPLIN201
C*620	FORMAT(36H *** NO. OF ALLOWABLE SWEEPS USED UP)	SPLIN202
	END	SPLIN203
C		SPLIN204
C	*****	SPLIN205
C		SPLIN206

```

C SUBROUTINE OPT(II)
C
C I REFERS TO THE ITH INTERIOR KNOT
C OPT FINDS THE OPTIMAL ITH KNOT BETWEEN THE I-1ST AND I+1ST KNOTS
C THE REMAINING KNOTS ARE HELD FIXED.
C INCLP = A BOUND ON THE NUMBER OF TRIES ALLOWED
C FOR IMPROVEMENT OF THE ITH KNOT
C G = MULTIPLICATION FACTOR WHICH SHOULD DECREASE AS A
C FUNCTION OF THE NO. OF SHEEPS THRU SWEEP
C G IS ALTERED IN SWEEP
C
COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE
COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),
* VORDL(28,2),KNCT,LMAX,INTERV
COMMON/ OTHER / LXI,LXI1,LXI2,G,CHANGE,ERROR,ACC, XI(28)
C
C I = II
C **NUMERICAL ANALYSIS PARAMETERS SET HERE
INCLP=9
BD = ACC*ERROR/FLOAT(LXI)
DIST = .0625
H = XI(I+2)-XI(I)
ALCW = XI(I) + DIST*H
AHIGH = XI(I+2) - DIST*H
LPCNT= 0
MODE = 3
C
C **BEGIN SEARCH = FIND THREE VALUES FOR THE ITH KNOT
C SUCH THAT L2-ERROR AT MIDDLE VALUE, A, IS LESS THAN
C ERROR AT LEFT VALUE, ALEFT, AND AT RIGHT VALUE, ARIGHT
A = XI(I+1)
E = FXDKNT(A)
ALEFT = A + G*(XI(I)-A)
ELEFT = FXDKNT(ALEFT)
C *** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***
C*** ARIGHT = 0.
C*** ERIGHT = 0.
C*** WRITE (6,900) ELEFT,E,ERIGHT,ALEFT,A,ARIGHT
SGN = SIGN(1.,ELEFT-E)
IF (SGN.GE.0.) GO TO 20
GO TO 60
C
C **SEARCHING FOR NEW KNOT TO THE RIGHT
10 ALEFT = A
ELEFT = E
A = ARIGHT
E = ERIGHT
20 ARIGHT = A + G*(XI(I+2)-A)
C
C **BUFFER TO PREVENT COALESCING OF KNOTS
30 IF (AHIGH.GE.ARIGHT) GO TO 40
AA = AHIGH
C *** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***
C**** WRITE(6,610) I
GO TO 199
C
40 ERIGHT = FXDKNT(ARIGHT)
C *** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***

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SPLIN264

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C***	WRITE (6,900) ELEFT,E,ERIGHT,ALEFT,A,ARIGHT	SPLIN265
	IF (E.LE.ERIGHT) GO TO 100	SPLIN266
C		SPLIN267
C	**CHECK TO STOP OPT	SPLIN268
	IF(E -ERIGHT.LE.80 .OR. LPCNT .GT. INDLP ) GO TO 240	SPLIN269
50	LPCNT = LPCNT+1	SPLIN270
	IF(SGN.GT.0.) GO TO 10	SPLIN271
C		SPLIN272
C	<del>**SEARCHING FOR NEW KNOT TO THE LEFT</del>	SPLIN273
60	ARIGHT = A	SPLIN274
	ERIGHT = E	SPLIN275
	<del>A = ALEFT</del>	SPLIN276
	E = ELEFT	SPLIN277
70	ALEFT = A + Q*(XI(I)-A)	SPLIN278
C		SPLIN279
C		SPLIN280
C	**BUFFER TO PREVENT COALESCING OF KNOTS	SPLIN281
80	IF (ALEFT.GE.AL0W) GO TO 90	SPLIN282
	AA = AL0W	SPLIN283
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN284
C***	WRITE(6,620) I	SPLIN285
	GO TO 199	SPLIN286
C		SPLIN287
90	ELEFT = FXOKNT(ALEFT)	SPLIN288
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN289
C***	WRITE (6,900) ELEFT,E,ERIGHT,ALEFT,A,ARIGHT	SPLIN290
	IF (E.LE.ELEFT) GO TO 100	SPLIN291
C		SPLIN292
C	**CHECK TO STOP OPT	SPLIN293
	IF(E - ELEFT.LE.80 .OR. LPCNT .GT. INDLP ) GO TO 230	SPLIN294
	GO TO 50	SPLIN295
C		SPLIN296
C	<del>**REQUIRED 3 VALUES HAVE BEEN FOUND</del>	SPLIN297
C	FOLLOWING CODE FINDS PT. AT WHICH MIN OF PARABOLA CURVE PASSIN	SPLIN298
C	THRU THE ERROR VALUES AT THE PTS ALEFT, A, ARIGHT OCCURS	SPLIN299
100	DXLEFT = ALEFT - A	SPLIN300
	DXRGHT = ARIGHT - A	SPLIN301
	DYLEFT = (ELEFT-E)/DXLEFT	SPLIN302
	DYRGHT = (ERIGHT-E)/DXRGHT	SPLIN303
	DIFF = DYLEFT - DYRGHT	SPLIN304
	IF (DIFF .EQ. 0.) GO TO 200	SPLIN305
	DEL = .5/DIFF*(DXRGHT*DYLEFT-DXLEFT*DYRGHT)	SPLIN306
	EPRED = E+DEL*(DYRGHT+(DXRGHT-DEL)/(ARIGHT-ALEFT)*DIFF)	SPLIN307
	ABEST = A + DEL	SPLIN308
	EBEST = FXOKNT(ABEST)	SPLIN309
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN310
C***	WRITE (6,900) ELEFT,EBEST,ERIGHT,ALEFT,ABEST,ARIGHT	SPLIN311
C		SPLIN312
C	**DETERMINE WHETHER ABEST GIVES BEST APPRX AND MAKE APPROPRIATE	SPLIN313
C	SWITCHING OF THE AI'S DEPENDING ON SIGN OF DEL	SPLIN314
	IF (EBEST.LE.E)	SPLIN315
	IF(DEL)110,200,120	SPLIN316
110	ALEFT = ABEST	SPLIN317
	ELEFT = EBEST	SPLIN318
	GO TO 170	SPLIN319
120	ARIGHT = ABEST	SPLIN320
	ERIGHT = EBEST	SPLIN321
	GO TO 170	SPLIN322

130	IF(DEL)140,200,150	SPLIN323
140	ARIGHT = A	SPLIN324
	ERIGHT = E	SPLIN325
	GO TO 160	SPLIN326
150	ALEFT = A	SPLIN327
	ELEFT = E	SPLIN328
160	A = ABEST	SPLIN329
	E = EBEST	SPLIN330
C		SPLIN331
C	**FOLLOWING TESTS DETERMINE WHETHER OR NOT TO	SPLIN332
C	REITERATE PARABOLA MINIMIZATION PHASE	SPLIN333
170	IF (ABS(EPRED-EBEST).LT.5.*80) GO TO 210	SPLIN334
	IF(LPCNT.GT.INDLP) GO TO 200	SPLIN335
	LPCNT = LPCNT+1	SPLIN336
	GO TO 100	SPLIN337
C		SPLIN338
199	ETRY = FXDKNT(AA)	SPLIN339
	IF (E.LT.ETRY) GO TO 200	SPLIN340
	A = AA	SPLIN341
	E = ETRY	SPLIN342
200	CHANGE = CHANGE + ABS(A - XI(I+1))/H	SPLIN343
	XI(I+1) = A	SPLIN344
	ERROR = E	SPLIN345
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN346
C***	WRITE(6,900) ELEFT,E,ERIGHT,ALEFT,A,ARIGHT	SPLIN347
	RETURN	SPLIN348
C		SPLIN349
C	IN FINAL VERSION GO TO 210, IS REPLACED BY GO TO 200	SPLIN350
210	CONTINUE	SPLIN351
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN352
C***	WRITE(6,640) LPCNT	SPLIN353
	GO TO 200	SPLIN354
230	A = ALEFT	SPLIN355
	E = ELEFT	SPLIN356
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN357
C***	WRITE(6,640) LPCNT	SPLIN358
	GO TO 200	SPLIN359
240	A = ARIGHT	SPLIN360
	E = ERIGHT	SPLIN361
C	*** THIS IS TEMPORARY DEBUGGING AND TESTING OUTPUT ***	SPLIN362
C***	WRITE(6,640) LPCNT	SPLIN363
	GO TO 200	SPLIN364
C*610	FORMAT(46H *** OPT DISCONTINUED - KNOT BEING OPTIMIZED (,I2,35H) MS	SPLIN365
C****	MOVED TOO CLOSE TO RIGHT NEIGHBOR)	SPLIN366
C*620	FORMAT(46H *** OPT DISCONTINUED - KNOT BEING OPTIMIZED (,I2,34H) MS	SPLIN367
C****	MOVED TOO CLOSE TO LEFT NEIGHBOR)	SPLIN368
C*640	FORMAT(24H *** OPT DISCONTINUED AT,I4,31H - INSUFFICIENT CHANGE IN	SPLIN369
C***	* ERROR)	SPLIN370
C*900	FORMAT(25H PARABOLA - ERROR VALUES ,3E20.6/12X,13HAI VALUES ,	SPLIN371
C***	1 3E20.6)	SPLIN372
	END	SPLIN373
C-----		SPLIN374
		SPLIN375
		SPLIN376

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FUNCTION FXDKNT (ARG)
C          THE FUNCTION RETURNS THE SQUARE OF THE L2-ERROR
C LOGICAL MODES
C** IT MAY BE NECESSARY ON SOME SYSTEMS TO MENTION ALL COMMON BLOCKS
C LISTED HERE IN THE PROGRAM CALLING *FXDKNT*, TOO, TO INSURE THAT
C THE INFO IN THESE BLOCKS DOES NOT DIE BETWEEN CALLS TO *FXDKNT*
COMMON / WANDT / TREND(100),TRPZWT(100),PRINT(100)
COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE
C      U(L) = FCT TO BE APPR AT XX(L), L=1,LX.
C      XX(L) IS ASSUMED TO BE NONDECREASING WITH L
C      ADDXI(I) = I-TH KNOT TO BE INTRODUCED, I=1,JADD
C      MODE = 0,1,2,3. SEE COMMENTS BELOW (AND IN NUBAS)
COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),
*      VORDL(28,2),KNOT,LMAX,INTERV
C      UERROR(L) = ERROR OF B.L2 A. TO U, L=1,LX
C      KNOT = CURRENT NO. OF KNOTS (INCL BDRY KNOTS)
C      INTERV = KNOT - 1 = CURRENT NO. OF INTERVALS (POL.PIECES)
C      XIL(K),K=1,KNOT, CURRENT (ORDERED) SET OF KNOTS
C      THE MAXIMUM ERROR OCCURS AT XX(LMAX)
C      IF ARG=1, FCTL(L) CONTAINS THE CURRENT B.AB TO U AT XX(L)
C      COEFL(I,.) CONTAINS THE POL.COEFL. ON I-TH INTERVAL FOR B.A.
C      VORDL(I,.) CONTAINS VALUE AND DERIV. OF B.A. AT XIL(I)
COMMON/ BASIS /FCT(100,30),VORD(30,28,2),BC(30),ILAST
C** A CHANGE IN THE COLUMN LENGTH OF *FCT* FORCES CHANGE IN ST.NO.69
C IN *NUBAS* .
C      FCT (L,M) = BASIS FCT M AT XX(L)
C      VORD(M,K,L) CONTAINS THE ORDS (L=1) AND SLOPES (L=2) OF FCT M
C      AT THE KNOT INTRODUCED AS K-TH. CORRELATION TO ORDERING OF
C      KNOTS BY SIZE IS DONE VIA IORDER, I.E., ORD AND SLOPE AT
C      XIL(K) ARE IN VORD(M,IORDER(K),.).
C      BC(I) = COORDINATE OF U (AND OF B.A. TO U) WRTO I-TH O.N.FCT
C      ILAST = CURRENT NO. OF BASIS FCTNS
COMMON/ LASTB /IORDER(28),INSIRT(30),XKNOT
C      THE FCT ILAST (TO BE) INTRODUCED LAST HAS ADDITIONAL KNOT
C      XKNOT, THE KNOT JUST INTRO-
C      DUCED HAS INDEX INSERT IN XIL,INSERT IS SAVED IN INSIRT(ILAST
C      FOR POSSIBLE REPLACEMENT OF KNOTS LATER ON (SEE MODE=2,3).
C ***LOCAL VARIABLES
COMMON /LOCAL/ XSCALE,KNOTSV,ERBUT1,CUBERR(100),WEIGHT(100),MODE3
C      XSCALE = XX(LX) - XX(1), USED TO NORMALIZE INNER PRODUCT
C      = LENGTH OF THE INTERVAL OF INTEGRATION
C      KNOTSV = NO. OF KNOTS USED IN MOST RECENT CALL TO FXDKNT
C      ERBUT1 = SQ. OF L2-ERROR OF APPR USING ALL BUT THE ONE
C      KNOT BEING VARIED ( USED IN MODE = 3)
C      CUBERR = UERROR OF B.A. BY CUBIC POL-S (NEEDED FOR MODE = 2)
C      MODE3 = TRUE OR FALSE DEP. ON WHETHER PREV. CALL WAS IN
C      MODE=3 OR NOT
EQUIVALENCE (IPRINT,CHANGE)
C      ARG IS EITHER FIXED POINT (MODE.NE.3) TO PICK PRINT-OUT OPTIS
C      OR IS FLOATING POINT (MODE=3) TO GIVE NEW VALUE OF KNOT VARIS
CHANGE = ARG
IF (MODE.GT.0)
C          GO TO 29
C *** MODE=0* COMPUTE BASIS FCT 1 THROUGH 4 AND B.A. TO U WRTO THE
C      THEN SET MODE = 1 AND PUT UERROR INTO U.
C      XSCALE = XX(LX) - XX(1)
C      DO 10 I=5,30
10 INSIRT(I) = 0

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DO 11 L=1,LX	SPLIN435
UERROR(L) = U(L)	SPLIN436
<del>TREND(L) = 1/(XX(L))</del>	SPLIN437
11 WEIGHT(L) = W(XX(L))	SPLIN438
DO 12 L=2,LX	SPLIN439
12 TRPZWT(L-1) = (XX(L)-XX(L-2))/2.*WEIGHT(L-1)	SPLIN440
TRPZWT(1) = (XX(2)-XX(1))/2.*WEIGHT(1)	SPLIN441
TRPZWT(LX) = (XX(1)-XX(LX-1))/2.*WEIGHT(LX)	SPLIN442
<del>XIL(1) = ADDXI(1)</del>	SPLIN443
<del>XIL(2) = ADDXI(2)</del>	SPLIN444
<del>IORDER(1) = 1</del>	SPLIN445
<del>IORDER(2) = 2</del>	SPLIN446
<del>KNOT = 2</del>	SPLIN447
<del>INTERV = 1</del>	SPLIN448
<del>DO 19 I=1,4</del>	SPLIN449
<del>ILAST = I</del>	SPLIN450
<del>CALL NUBAS</del>	SPLIN451
<del>DO 19 L=1,LX</del>	SPLIN452
19 UERROR(L) = UERROR(L) - BC(I)*FCT(L,I)	SPLIN453
<del>MODE = 1</del>	SPLIN454
<del>DO 20 L = 1,LX</del>	SPLIN455
20 CUBERR(L) = UERROR(L)	SPLIN456
IF (JADD.LE.2), ONLY B.A. BY CUBICS IS COMPUTED	SPLIN457
OTHERWISE, ADDXI(I), I.GT.2, CONTAINS ADDITIONAL KNOTS	SPLIN458
JADD = JADD - 2	SPLIN459
IF (JADD.LE.0) GO TO 60	SPLIN460
DO 21 I=1,JADD	SPLIN461
21 ADDXI(I) = ADDXI(I+2)	SPLIN462
GO TO 51	SPLIN463
GO TO (40,40,30),MODE	SPLIN464
*** MODE=3 *** MERELY REPLACE THE LAST KNOT INTRODUCED BY	SPLIN465
CHANGE AND RECOMPUTE L2 ERROR. CHANGE ENTERS	SPLIN466
VIA THE ARGUMENT JPRINT = CHANGE.	SPLIN467
THIS MODE SHOULD BE USED FOR	SPLIN468
MINIMIZING THE L2-ERROR WRTO THE KNOT	SPLIN469
INTRODUCED LAST AS IT MINIMIZES THE COMP WORK	SPLIN470
IF MODE3 = TRUE (I.E., THE PRECEDING CALL TO FXDKNT	SPLIN471
WAS IN MODE=3), THE PROGR WILL ASSUME THAT CHANGES	SPLIN472
HAS THE SAME ORDER REL TO THE OTHER KNOTS AS THE	SPLIN473
PREV INTRODUCED VALUE FOR KNOT. OTHERWISE	SPLIN474
IF MODE3=FALSE (THE PRECEDING CALL WAS IN SOME OTHER	SPLIN475
, A FCT IS ADDED WITH CHANGE AS THE ADD. KNOT.	SPLIN476
UERROR IS ASSUMED TO CONTAIN ERROR OF B.A. TO U	SPLIN477
ALL PREV FCTNS. **NOTE** IF THE NEXT CALL TO FXD	SPLIN478
IS IN A MODE OTHER THAN 3, THE CHANGE PROPOSED	SPLIN479
NOW WILL BE MADE PERMANENT.	SPLIN480
30 XKNOT = CHANGE	SPLIN481
IF (MODE3) GO TO 35	SPLIN482
MODE3 = .TRUE.	SPLIN483
ERBUT1 = FXDKNT	SPLIN484
MODE = 2	SPLIN485
CALL NUBAS	SPLIN486
KNOTSV = KNOT	SPLIN487
MODE = 3	SPLIN488
	SPLIN489
	SPLIN490
	SPLIN491
	SPLIN492



	GO TO 36	SPLIN493
35 CALL NUBAS		SPLIN494
36 FXDKNT = ABSTERBUT1 - BC(ILAST)/XSCALE*BC(ILAST)		SPLIN495
	RETURN	SPLIN496
C -----		SPLIN497
C ***MODE=1,2***	RETAIN THE FIRST KNOT KNOTS INTRODUCED EARLIER	SPLIN498
C	(HENCE THEIR CORRESP FCTNS) BUT REPLACE FURTHER	SPLIN499
C	FCTNS (IF ANY) BY FCTNS HAVING ADDITIONAL	SPLIN500
C	KNOTS ADDXI(I), I=1, JADD	SPLIN501
C	IF KNOT.LT.KNOTSV (=NO.OF KNOTS USED IN PREV CALLS)	SPLIN502
C	40 THROUGH 49 RESTORES ARRAYS IORDER, XIL, UERROR TO THE STATE OF	SPLIN503
C	ILAST = KNOT + 2, INVERTING THE ACTION OF DO 11 ... TO 14 IN	SPLIN504
40 IF (KNOT.LT.KNOTSV)	GO TO 42	SPLIN505
KNOT = KNOTSV		SPLIN506
IF 1.NOT.MODE3	GO TO 50	SPLIN507
DO 41 L=1, LX		SPLIN508
41 UERROR(L) = UERROR(L) - BC(ILAST)*FCT(L, ILAST)		SPLIN509
	GO TO 49	SPLIN510
42 DO 43 L=1, LX		SPLIN511
43 UERROR(L) = CUBERR(L)		SPLIN512
IF (KNOT.LE.2)	GO TO 48	SPLIN513
IDUM = KNOT + 1		SPLIN514
DO 45 IO=IDUM, KNOTSV		SPLIN515
INSERT = INSERT(ILAST)		SPLIN516
ILM3 = ILAST - 3		SPLIN517
DO 44 K=INSERT, ILM3		SPLIN518
IORDER(K) = IORDER(K+1)		SPLIN519
44 XIL(K) = XIL(K+1)		SPLIN520
45 ILAST = ILAST-1		SPLIN521
DO 47 I=5, ILAST		SPLIN522
DO 47 L=1, LX		SPLIN523
47 UERROR(L) = UERROR(L) - BC(I)*FCT(L, I)		SPLIN524
	GO TO 49	SPLIN525
48 XIL(2) = XIL(ILAST-2)		SPLIN526
IORDER(2) = 2		SPLIN527
KNOT = 2		SPLIN528
49 IF (JADD.GT.0)	GO TO 51	SPLIN529
ILAST = KNOT + 2		SPLIN530
INTERV = KNOT - 1		SPLIN531
	GO TO 60	SPLIN532
C		SPLIN533
C ***MODE=1,2***	ADD JADD BASIS FCTNS, I.E., FOR IO=1, JADD,	SPLIN534
C	CONSTRUCT FCT ILAST WITH ONE MORE KNOT, VIZ.	SPLIN535
C	XKNOT=ADDXI(IO), THAN THE PREVIOUS LAST FCT,	SPLIN536
C	ORTHONORMALIZE IT OVER ALL PREVIOUS FCTNS, THEN	SPLIN537
C	COMPUTE THE COORDINATE BC(ILAST) OF U WRTO IT,	SPLIN538
C	SUBTRACT OUT ITS COMPONENT FROM UERROR.	SPLIN539
50 IF (JADD.LE.0)	GO TO 61	SPLIN540
51 DO 52 IO=1, JADD		SPLIN541
XKNOT = ADDXI(IO)		SPLIN542
CALL NUBAS		SPLIN543
DO 52 L=1, LX		SPLIN544
52 UERROR(L) = UERROR(L) - BC(ILAST)*FCT(L, ILAST)		SPLIN545
C		SPLIN546
60 FXDKNT= DOT(31,2)/XSCALE		SPLIN547
KNOTSV = KNOT		SPLIN548
61 MODE3 = .FALSE.		SPLIN549
IF (IPRINT.EQ.0)	RETURN	SPLIN550

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C      VARIOUS PRINTING IS DONE DEP ON THE ARG = IPRINT
C                                     GO TO (70,80,90),IPRINT
C
C      COMPUTE COEFFICIENTS OF B.A. AND PRINT
C      ****      BEST APPROXIMATION PRINTOUT      ****
C      FORMAT IS
C      KNOTS XI(J)      CUBIC COEFFICIENTS P(I,J) IN
C                        INTERVAL (XI(J), XI(J+1))
C                        ERROR CURVE (SCALED)
C
C      THE FOLLOWING FORTRAN CODE FINDS VALUES AT X OF THE
C      APPROXIMATION FROM THIS OUTPUT----
C      I=LXI2
C      1 A=X-XI(I)
C      IFTA) 2,4,4
C      2 I=I-1
C      IF(I) 3,3,1
C      3 I=1
C      4 V=P(I,1)+A*(P(I,2)+A*(P(I,3)+A*(P(I,4))))
C      ..... FOR A SUBPROGRAM USE COMMON/OUTPUT/..., COMMON/OTHER/...,
C      ..... THE P BECOME COEFL(I,1),COEFL(I,2),COEFL(I,3),COEFL(I,4)
C
C      70 WRITE(6,610)
C      DO 72 I=1,KNOT
C      ILOC = IORDER(I)
C      DO 72 L=1,2
C      72 VORD(I,L) = -ARITH1(0.,ILAST,80,I,VORD(I,ILOC,L),I)
C      SEE COMMENT IN *DOT* ABOUT THE *ARITH1* ROUTINE.
C      CALL EVAL
C      DO 73 I=1,INTERV
C      WRITE(6,620) I,XIL(I)
C      73 WRITE (6,630) (J,COEFL(I ,J),J=1,4)
C      WRITE (6,620) KNOT,XIL(KNOT)
C      610 FORMAT(42X,5HKNOTS,22X,18HCUBIC COEFFICIENTS//)
C      620 FORMAT(35X, 3HXI(, I2, 3H) =, F12.6)
C      630 FORMAT(67X,2HC(,I1,3H) =,E16.6)
C
C      **COMPUTE L2, L1, MAX ERRORS AND PRINT
C      80 ERRL2 = SQRT(FXOKNT)
C      ERRL1 = 0.
C      ERRL99= 0.
C      DO 82 L=1,LX
C      DIF = ABS(UERROR(L)*WEIGHI(L))
C      IF(ERRL99.GT.DIF)      GO TO 81
C      LMAX = L
C      ERRL99 = DIF
C      81 ERRL1 = ERRL1+ DIF
C      82 CONTINUE
C      ERRL1 = ERRL1/FLOAT(LX)
C      WRITE(6,623) ERRL2, ERRL1, ERRL99,XX(LMAX)
C      *** THE FOLLOWING CARD IS TEMPORARY
C      GO TO (90,96,96),IPRINT
C
C      ** SCALE ERROR CURVE AND PRINT
C      90 IE = 0
C      SCALE = 1.
C      IF (ERRL99.GE.10.)      GO TO 92
C      DO 91 IE=1,9

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SCALE = SCALE*10.			SPLIN617
IF (ERR199*SCALE.GE.10.)	GO TO 92		SPLIN618
91 CONTINUE			SPLIN619
92 DO 93 L=1,LX			SPLIN610
93 PRINT (L) = UERROR(L)*SCALE			SPLIN611
	GO TO (94,95,95),IPRINT		SPLIN612
94 WRITE (6,621) IE,(L,XX(L),FCTL(L),PRINT(L),L=1,LX)			SPLIN613
	GO TO 96		SPLIN614
95 WRITE (6,622) IE,(L,XX(L),PRINT(L),L=1,LX)			SPLIN615
96	RETURN		SPLIN616
621 FORMAT(1H //45X,36HAPPROXIMATION AND SCALED ERROR CURVE/38X,			SPLIN617
*10HDATA POINT,7X,13HAPPROXIMATION,3X,16HDEVIATION X 10E+,I1/			SPLIN618
*(31X,I4,F16.8,F16.8,F17.6))			SPLIN619
622 FORMAT(1H //58X, 11HERROR CURVE/38X, 10HDATA POINT, 23X,			SPLIN620
116HDEVIATION X 10E+,I1/(31X,I4,F16.8,16X,F17.6))			SPLIN621
623 FORMAT(1H ///40X20HLEAST SQUARE ERROR =,E20.6/			SPLIN622
1	40X20HAVERAGE ERROR	=,E20.6/	SPLIN623
2	40X20HMAXIMUM ERROR	=,E20.6,3H AT,F12.6///)	SPLIN624
END			SPLIN625
C			SPLIN626
C*****			SPLIN627
C			SPLIN628

C	SUBROUTINE INTERP	SPLIN629
C		SPLIN630
C	COMPUTE THE SLOPES VORDL(I,2), I=2,KNOT-1 AT INTERIOR	SPLIN631
C	KNOTS OF CUBIC SPLINE FOR GIVEN VALUES VORDL(I,1),I=1,KNOT,	SPLIN632
C	AT ALL THE KNOTS AND GIVEN BOUNDARY DERIVATIVES	SPLIN633
	DIMENSION D(28), DIAG(28)	SPLIN634
	COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),	SPLIN635
	* VORDL(28,2),KNOT,LMAX,INTERV	SPLIN636
	DATA DIAG(1),D(1)/1.,0./	SPLIN637
	DO 10 M=2,KNOT	SPLIN638
	D(M) = XIL(M) - XIL(M-1)	SPLIN639
10	DIAG(M) = (VORDL(M,1)-VORDL(M-1,1))/D(M)	SPLIN640
	DO 20 M=2,INTERV	SPLIN641
	VORDL(M,2) = 3.*(D(M)*DIAG(M+1) + D(M+1)*DIAG(M))	SPLIN642
20	DIAG(M) = 2.*(D(M)+D(M+1))	SPLIN643
	DO 30 M=2,INTERV	SPLIN644
	G = -D(M+1)/DIAG(M-1)	SPLIN645
	DIAG(M) = DIAG(M) + G*D(M-1)	SPLIN646
30	VORDL(M,2) = VORDL(M,2) + G*VORDL(M-1,2)	SPLIN647
	NJ = KNOT	SPLIN648
	DO 40 M=2,INTERV	SPLIN649
	NJ = NJ - 1	SPLIN650
40	VORDL(NJ,2) = (VORDL(NJ,2) - D(NJ)*VORDL(NJ+1,2))/DIAG(NJ)	SPLIN651
	RETURN	SPLIN652
	END	SPLIN653
C	*****	SPLIN654
C	*****	SPLIN655
C	*****	SPLIN656

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C      FUNCTION DOT (M,INDEX)
C      COMPUTE INNER PRODUCT OF FCT M WITH FCT ILAST (INDEX=1) OR
C      UERROR (INDEX=2)
COMMON / WANDT / TREND(100),TRPZWT(100),G(100)
COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE
COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(26),COEFL(27,4),
      VORDL(26,2),KNOT,LMAX,INTERV
COMMON/ BASIS /FCT(100,30),VORD(30,26,2),BC(30),ILAST
      GO TO (10,30),INDEX
10 IF (M.EQ.ILAST)
   DO 11 L=1,LX
11 G(L) = FCT(L,M)*FCTL(L)
      GO TO 80
20 DO 21 L=1,LX
21 G(L) = FCTL(L)*FCTL(L)
      GO TO 80
30 IF (M.EQ.31)
   DO 31 L=1,LX
31 G(L) = FCTL(L)*UERROR(L)
      GO TO 80
40 DO 41 L=1,LX
41 G(L) = UERROR(L)*UERROR(L)
C
C      EFFICIENTLY PROGRAMMED DOUBLE PRECISION ACCUMULATION OF SCALAR
C      PRODUCTS IS CALLED FOR HERE. AT PURDUE, WE USE
C      D = ARITH1(C,N,A,IA,B,IB)
C      WHICH RETURNS THE VALUE OF
C      D = C - SUM(A(1+J*IA) * B(1+J*IB), J=0,...,N-1)
C
80 DOT = -ARITH1(0.,LX,G,1,TRPZWT,1)
      RETURN
END
C
C *****
C

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	SUBROUTINE EVAL	SPLIN692
C	COMPUTE POL. COEFF COEFL(I,K) OF FCT ILAST FROM VORDL,	SPLIN693
C	THEN COMPUTE FCTL(L) = (FCT ILAST)*TREND AT XX(L),L=1,LX	SPLIN694
C		SPLIN695
	COMMON / WANDT / TREND(100),TRPZWT(100),G(100)	SPLIN696
	COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE	SPLIN697
	COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),	SPLIN698
	* VORDL(28,2),KNOT,LMAX,INTERV	SPLIN699
	DO IL I=1,INTERV	SPLIN700
	COEFL(I,1) = VORDL(I,1)	SPLIN701
	COEFL(I,2) = VORDL(I,2)	SPLIN702
	DX = XIL(I+1) - XIL(I)	SPLIN703
	DUM1 = (VORDL(I+1,1)-VORDL(I,1))/DX	SPLIN704
	DUM2 = VORDL(I,2)+VORDL(I+1,2)-2.*DUM1	SPLIN705
	COEFL(I,3) = (DUM1-DUM2-VORDL(I,2))/DX	SPLIN706
10	COEFL(I,4) = DUM2/DX/DX	SPLIN707
C		SPLIN708
	J = 1	SPLIN709
	ISWTCH = 1	SPLIN710
	DO 20 L=1,LX	SPLIN711
	GO TO (11,13),ISWTCH	SPLIN712
11	IF (J.EQ.INTERV)	SPLIN713
	GO TO 12	
	IF (XX(L).LT.XIL(J+1))	SPLIN714
	GO TO 13	
	J = J + 1	SPLIN715
	GO TO 11	SPLIN716
12	ISWTCH = 2	SPLIN717
13	DX = XX(L) - XIL(J)	SPLIN718
20	FCTL(L) = (COEFL(J,1)+DX*(COEFL(J,2)+DX*(COEFL(J,3)	SPLIN719
	+DX*COEFL(J,4))))*TREND(L)	SPLIN720
	RETURN	SPLIN721
	END	SPLIN722
C		SPLIN723
C	*****	SPLIN724
C		SPLIN725

	SUBROUTINE NUBAS		SPLIN726
	COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE		SPLIN727
	<del>COMMON/ OUTPUT /UERROR(100),FCTL(100),XIL(28),COEFL(27,4),</del>		<del>SPLIN728</del>
	<del>VORDL(28,2),KNOT,LMAX,INTERV</del>		<del>SPLIN729</del>
	COMMON/ BASIS /FCT(100,30),VORD(30,28,2),BC(30),ILAST		SPLIN730
	COMMON/ LASTB /IORDER(28),INSIRT(30),XKNOT		<del>SPLIN731</del>
C	COEF(IC,.) CONTAINS THE POL COEFFICIENTS OF FCT M FOR INTER-		SPLIN732
C	VAL TO THE RIGHT OF XI(IC), IC=ICH,ICH*M-3,		SPLIN733
C	WITH ICH = M*(M-7)/2 + 10 (WITH OBVIOUS MODS FOR M.LE.4)		SPLIN734
C	THE FCT ILAST (TO BE) INTRODUCED LAST, HAS ITS VALUES AT THE		SPLIN735
C	POINTS XX(L) IN FCTL(L), HAS FIRST INDEX ICLASS		SPLIN736
C	IN COEF AND XI, HAS ADDITIONAL KNOT XKNOT, THE KNOT KNOTS		SPLIN737
C	FOR IT ARE CONTAINED, IN INCREASING ORDER, IN XIL,ITS COR-		SPLIN738
C	RESPONDING ORDS AND SLOPES ARE IN VORDL, THE KNOT JUST INTRO-		SPLIN739
C	DUCE HAS INDEX INSERT IN XIL,INSERT IS SAVED IN INSIRT(ICLASS		<del>SPLIN740</del>
C	FOR POSSIBLE REPLACEMENT OF KNOTS LATER ON (SEE MODE=2,3).		SPLIN741
	DIMENSION TEMP(30),XI(381),COEF(381,4)		SPLIN742
	<del>IF (MODE.GT.0)</del>	<del>GO TO 8</del>	<del>SPLIN743</del>
C	<del>***CONSTRUCT FCT ILAST FOR ILAST.LE.4</del>		SPLIN744
	XI(ILAST) = XIL(1)		SPLIN745
	<del>ICLAST = ILAST</del>		<del>SPLIN746</del>
	ILM1 = ILAST-1		SPLIN747
	IF(ILAST.GT.2)	GO TO 7	SPLIN748
	<del>IF(ILAST.EQ.2)</del>	<del>GO TO 6</del>	<del>SPLIN749</del>
C	FIRST BASIS FCT IS A CONSTANT		SPLIN750
	VORDL(1,1)=1.		SPLIN751
	<del>VORDL(2,1)=1.</del>		<del>SPLIN752</del>
	VORDL(1,2)=0.		SPLIN753
	VORDL(2,2)=0.		SPLIN754
		GO TO 67	<del>SPLIN755</del>
C	SECOND BASIS FCT IS A STRAIGHT LINE		SPLIN756
	6 VORDL(2,2) = VORDL(1,1)/(XIL(2) - XIL(1))*2.		SPLIN757
	<del>VORDL(1,2) = -VORDL(2,2)</del>		<del>SPLIN758</del>
C			SPLIN759
	7 VORDL(2,1) = - VORDL(2,1)		SPLIN760
	<del>VORDL(2,2) = - VORDL(2,2)</del>		<del>SPLIN761</del>
		GO TO 59	SPLIN762
C	<del>8</del>	<del>GO TO (10,10,14),MODE</del>	<del>SPLIN763</del>
C	<del>***SET UP CONSTANTS DEP.ON ILAST. INSERT NEW KNOT INTO XIL</del>		<del>SPLIN764</del>
C	AND UPDATE VORD FOR FCT M,M=1,ILAST-1		SPLIN765
	10 KNOT = KNOT + 1		SPLIN766
	ILAST = KNOT + 2		SPLIN767
	ICLAST = ILAST*(ILAST-7)/2 + 10		SPLIN768
	<del>ILM1 = ILAST-1</del>		<del>SPLIN769</del>
	INTERV = KNOT - 1		SPLIN770
	DO 11 INSERT=2,INTERV		SPLIN771
	<del>IF (XKNOT.LT.XIL(INSERT))</del>	<del>GO TO 12</del>	<del>SPLIN772</del>
	11 CONTINUE		SPLIN773
		GO TO 95	SPLIN774
	<del>12 IF (XKNOT.LE.XIL(INSERT-1))</del>	<del>GO TO 95</del>	<del>SPLIN775</del>
	IO = KNOT		SPLIN776
	DO 13 L=INSERT,INTERV		SPLIN777
	<del>IO = IO - 1</del>		<del>SPLIN778</del>
	XIL(IO+1) = XIL(IO)		SPLIN779
	13 IORDER(IO+1) = IORDER(IO)		SPLIN780
	<del>IORDER(INSERT) = KNOT</del>		<del>SPLIN781</del>
C			SPLIN782

14	XIL(INSERT) = XKNOT		SPLIN784
	DX = XKNOT - XIL(1)		SPLIN785
	<del>DO 15 I=1,4</del>		SPLIN786
	VORD(I,KNOT,1)=COEF(I,1)+DX*(COEF(I,2)+DX*(COEF(I,3)		SPLIN787
	<del>* DX*COEF(I,4)))</del>		SPLIN788
15	VORD(I,KNOT,2)=COEF(I,2)+DX*(2.*COEF(I,3)+DX*3.*COEF(I,4))		SPLIN789
	IF(ILM1.LT.5) GO TO 20		SPLIN790
	ID = 4		SPLIN791
	IBOUND = 4		SPLIN792
	DO 19 I=5,ILM1		SPLIN793
	ID = ID + I - 4		SPLIN794
	<del>IBOUND = IBOUND + I - 3</del>		SPLIN795
17	IF (ID.EQ.IBOUND)	GO TO 18	SPLIN796
	IF (XKNOT.LT.XI(ID+1))	GO TO 18	SPLIN797
	<del>ID = ID + 1</del>		SPLIN798
		GO TO 17	SPLIN799
18	DX = XKNOT - XI(ID)		SPLIN800
	VORD(I,KNOT,1)=COEF(ID,1)+DX*(COEF(ID,2)+DX*(COEF(ID,3)		SPLIN801
	<del>* DX*COEF(ID,4)))</del>		SPLIN802
19	VORD(I,KNOT,2)=COEF(ID,2)+DX*(COEF(ID,3)*2.+DX*3.*COEF(ID,4))		SPLIN803
C	<del>-----</del>		SPLIN804
C	-----DEFINE LAST BASIS FUNCTION		SPLIN805
	20 CONTINUE		SPLIN806
		GO TO (30,40,50),MODE	SPLIN807
C	*** MODE=1 ***	ADD ILAST-TH BASIS FUNCTION. CONSTRUCT FROM FCT	SPLIN808
C		ILAST-1 BY REFLECTING THE PART OF THE LATTER TO	SPLIN809
C		THE RIGHT OF XKNOT ACROSS THE X-AXIS, THEN INTERSPLIN810	
C		POLATING. THIS SHOULD INDUCE ONE MORE OSCILLATIO	SPLIN811
C		N IN FCT ILAST THAN IN FCT ILAST-1	SPLIN812
C			SPLIN813
29	MODE = 1		SPLIN814
30	VORDL(1,2) = VORD(ILM1,1,2)		SPLIN815
	<del>DO 31 K=1,INSERT</del>		SPLIN816
	<del>*LOC = IORDER(K)</del>		SPLIN817
31	VORDL(K,1) = VORD(ILM1,ILOC,1)		SPLIN818
	<del>DO 32 K=INSERT,INTERV</del>		SPLIN819
	<del>ILOC = IORDER(K+1)</del>		SPLIN820
32	VORDL(K+1,1) = -VORD(ILM1,ILOC,1)		SPLIN821
	<del>VORDL(KNOT,2) = -VORD(ILM1,2,2)</del>		SPLIN822
		GO TO 55	SPLIN823
C			SPLIN824
C	*** MODE=2 ***	REPLACE FCT ILAST BY INTERPOLATING IT AT THE	SPLIN825
C		CURRENT SET OF KNOTS. IF FCT ILAST HAS NOT BEEN	SPLIN826
C		PREVIOUSLY DEF (INSIRT(ILAST)=0) (SEE 9 ABOVE,	SPLIN827
C		ALSO MAIN AT 10)) SET MODE=1, PROCEED IN THAT MOD	SPLIN828
C			SPLIN829
40	IF (INSIRT(ILAST).EQ.0)	GO TO 29	SPLIN830
	VORDL(1,1)=VORD(ILAST,1,1)		SPLIN831
	VORDL(1,2)=VORD(ILAST,1,2)		SPLIN832
	ID = ICLAST		SPLIN833
	<del>IBOUND = ICLAST + ILAST = 4</del>		SPLIN834
	<del>DO 43 K=2,INTERV</del>		SPLIN835
41	IF (ID.EQ.IBOUND)	GO TO 42	SPLIN836
	IF (XIL(K).LT.XI(ID+1))	GO TO 42	SPLIN837
	ID = ID + 1		SPLIN838
		GO TO 41	SPLIN839
42	DX = XIL(K) - XI(ID)		SPLIN840
43	VORDL(K,1) = COEF(ID,1)+DX*(COEF(ID,2)+DX*(COEF(ID,3)		SPLIN841



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      *
      VORDL(KNOT,1)=VORD(ILAST,2,1)
      VORDL(KNOT,2)=VORD(ILAST,2,2)
      GO TO 55
      *** MODE=3 *** CHANGE FCT ILAST BY CHANGING JUST THE KNOT INTRODUCED LAST
      50 ID = ICLAST + INSERT - 1
      DX = XKNOT - XI(ID)
      XI(ID) = XKNOT
      IF (DX.GE.0.)
      ID = ID - 1
      DX = XKNOT - XI(ID)
      51 VORDL(INSERT,1) = COEF(ID,1) + DX*(COEF(ID,2) + DX*(COEF(ID,3)
      *
      *
      *** INTERPOLATE
      55 CALL INTERP
      GO TO (57,57,59),MODE
      57 ID = ICLAST - 1
      DO 56 IO=1,INTERV
      ID = ID + 1
      56 XI(ID) = XIL(IO)
      INSIRT(ILAST) = INSERT
      C-----
      C-----*** ORTHONORMALIZE FCT ILAST OVER PREVIOUS (ORTHONORMAL) SET
      C-----THEN COMPUTE THE COMPONENT BC(ILAST) OF UERROR WRTO IT
      C-----FINALLY,STORE THE VARIOUS REPRESENTATIONS OF FCT ILAST
      C-----
      59 CALL EVAL
      DO 60 I=1,ILM1
      60 TEMP(I) = DOT(I,1)
      DO 69 L=1,LX
      69 FCTL(L) = ARITH1(FCTL(L),ILM1,TEMP,1,FCT(L,1),100)
      C SEE COMMENT IN *DOT* ABOUT THE *ARITH1* ROUTINE
      DO 61 K=1,KNOT
      ILOC = IORDER(K)
      DO 61 L=1,2
      61 VORDL(K,L) = ARITH1(VORDL(K,L),ILM1,TEMP,1,VORD(1,ILOC,L),1)
      C SEE COMMENT IN *DOT* ABOUT *ARITH1* ROUTINE
      67 CALL EVAL
      C = SQRT(DOT(ILAST,1))
      IF (C.EQ. 0.) C = 1.
      BC(ILAST) = DOT(ILAST,2) / C
      DO 62 K=1,KNOT
      ILOC = IORDER(K)
      DO 62 L=1,2
      VORDL(K,L) = VORDL(K,L)/C
      62 VORD(ILAST,ILOC,L) = VORDL(K,L)
      ID = ICLAST - 1
      DO 63 IO=1,INTERV
      ID = ID + 1
      DO 63 L=1,4
      63 COEF(ID,L) = COEFL(IO,L)/C
      DO 64 L=1,LX
      64 FCT(L,ILAST) = FCTL(L)/C
      C-----

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	RETURN	SPLIN900
C		SPLIN901
C	*** THIS OUTPUT INDICATES A FAILURE CONDITION ***	SPLIN902
	95 WRITE (6,950) XKNOT,ILAST	SPLIN903
	950 FORMAT (15H *** NEW KNOT,E20.8,13H FOR FUNCTION,I3,50H OUT OF BOS	SPLIN904
	*UNDS OR COINCIDENT WITH A PREVIOUS KNOT./36H *** EXECUTION CANNOS	SPLIN905
	*T BE CONTINUED)	SPLIN906
	STOP	SPLIN907
C		SPLIN908
	END	SPLIN909
C		SPLIN910
C	*****TREND AND WEIGHT FUNCTIONS*****	SPLIN911
C		SPLIN912

FUNCTION T(Z)

T = 1.

RETURN

END

SPLIN913

SPLIN914

SPLIN915

SPLIN916

SPLIN917

FUNCTION W(Z)

W = 1.

RETURN

END

SPLIN918

SPLIN919

SPLIN920

SPLIN922

SPLIN923

C-----

IDENT ARITH1  
 ARITH1 - ARITHMETIC PACKAGE FOR LINEQ1 AND DTMT1.

DAVID S. DODSON. 06/01/70.

FUNCTION.

GIVEN REAL SCALAR C AND N-VECTORS A AND B, THIS  
 PACKAGE COMPUTES THE FUNCTION:

$$ARITH1 = C - \sum_{I=1}^N A(I) * B(I)$$

USAGE.

FORTRAN FUNCTION REFERENCE TO ARITH1 OF FORM:

Y=ARITH1(C,N,A,KA,R,KB)

WHERE: A AND B ARE THE NAMES OF THE TWO VECTORS AND  
 KA AND KB ARE THE INCREMENTS BETWEEN SUCCESSIVE  
 ELEMENTS OF THE A AND B VECTORS IN MEMORY.

COMPATABILITY.

THIS ROUTINE IS EQUIVALENT TO THE FORTRAN SUBPROGRAM:

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      FUNCTION ARITH1 (C,N,A,KA,B,KB)
      DOUBLE PRECISION T
      REAL A(KA,N),B(KB,N)
      T=DBLE(C)
      IF(N.EQ.0)GO TO 5
      DO 4 I=1,N
      4 T=T-DBLE(A(1,I))*DBLE(B(1,I))
      5 ARITH1=T
      RETURN
      END
  
```

EJECT  
 ENTRY ARITH1

LOOP

SA1	B3	FETCH NEXT A
SB3	B3+B4	
SA2	B5	FETCH NEXT B
SB5	B5+B6	
FX0	X1*X2	(X0,X1) = (X1) * (X2)
DX1	X1*X2	
FX2	X6-X0	(X6,X7) = (X6,X7) - (X0,X1)
DX3	X6-X0	
FX0	X7-X1	
NX2	X2	
FX1	X0+X2	
FX0	X1+X2	
NX3	X0	
DX1	X1+X2	

ARITH 1  
 ARITH 2  
 ARITH 3  
 ARITH 4  
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 ARITH 60

NX2	X1		ARITH 61
FX6	X2+X3		ARITH 62
DX7	X2+X3		ARITH 63
SB2	B2-B1	COUNT TERM	ARITH 64
NZ	B2+LOOP	LOOP TO COMPUTE INNER PRODUCT	ARITH 65
ARITH1	RSSZ	1	ARITH 66
	SA1	B1	ARITH 67
	BX6	X1	ARITH 68
	MX7	0	ARITH 69
	DX7	X6+X7	ARITH 70
	SB1	1	ARITH 71
	SA1	B2	ARITH 72
	SB2	X1	ARITH 73
	ZR	X1, ARITH1	ARITH 74
		RETURN IF N = 0	ARITH 75
	SA1	B4	ARITH 76
	SB4	X1	ARITH 77
	SA1	B6	ARITH 78
	SB6	X1	ARITH 79
	EQ	LOOP	ARITH 80
	SPACE	4	ARITH 81
	END		ARITH 82

SUBROUTINE TRID (M,SUP,SUB,DIAG,B)

.....

SUBROUTINE TRID

DECKS USED  
TRID

PURPOSE  
SOLVES THE MATRIX EQUATION  $AX=B$ , WHERE A IS TRIDIAGONAL.

USAGE  
CALL TRID(M,SUP,SUB,DIAG,B)

DESCRIPTION OF PARAMETERS

M - ORDER OF MATRIX A.  
SUP - (M X 1) SUPER DIAGONAL OF A.  
       $SUP(I)=A(I,I+1) \quad I=1,M-1$   
SUB - (M X 1) SUB DIAGONAL OF A.  
       $SUB(I)=A(I+1,I) \quad I=1,M-1$   
DIAG - (M X 1) MAIN DIAGONAL OF A.  
       $DIAG(I)=A(I,I) \quad I=1,M$   
B - (M X 1) CONSTANT VECTOR. (SOLUTION RETURNED  
   IN B)

REMARKS

THE ARRAYS MUST HAVE THE FOLLOWING DIMENSIONS  
SUP(M),SUB(M),DIAG(M),B(M)

SUB AND SUP CONTAIN M-1 ELEMENTS.

METHOD

DECOMPOSES MATRIX A INTO  $L*U$ , THEN SOLVES THE EQUATIONS  
 $*Z=R$  AND  $U*X=Z$ . SOLUTION IS RETURNED IN B VECTOR.

.....

DIMENSION SUP(M),SUB(M),DIAG(M),B(M)

N = M

NN = N-1

SUP(1) = SUP(1)/DIAG(1)

B(1) = B(1)/DIAG(1)

DO 10 I=2,N

II = I-1

DECOMPOSE A TO FORM  $A=LU$  WHERE L IS LOWER TRIANGULAR  
" IS UPPER TRIANGULAR

DIAG(I) = DIAG(I)-SUP(II)\*SUB(II)

IF (I.EQ. N) GO TO 10

SUP(I) = SUP(I)/DIAG(I)

COMPUTE Z WHERE  $LZ=B$

B(I) = (B(I)-SUB(II)\*B(II))/DIAG(I)

COMPUTE X BY BACK SUBSTITUTION WHERE  $UX=Z$

DO 20 K=1,NN

I = N-K

B(I) = B(I)-SUP(I)\*B(I+1)

RETURN

END

TRID	1
TRID	2
TRID	3
TRID	4
TRID	5
TRID	6
TRID	7
TRID	8
TRID	9
TRID	10
TRID	11
TRID	12
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TRID	57
TRID	58

### APPENDIX III

#### PROGRAM LISTING - VCF

- ADYNF

- SUBROUTINES



PROGRAM VCF8 (INPUT, OUTPUT, PUNCH, TAPE3, TAPE4,	VCF8	2
1 TAPE5=INPUT, TAPE6=OUTPUT, TAPE7=PUNCH)		
DIMENSION U(32,2,51), W(32,51), UT(32,51), UB(32,51)	VCF8	4
DIMENSION INFO(16)	VCF8	5
DIMENSION THASRT(6), UZZT(6), UZZSQT(6), GAMART(6), IFLGT(6)	VCF8	6
DIMENSION THASRB(6), UZZB(6), UZZSQB(6), GAMARB(6), IFLGB(6)	VCF8	7
DIMENSION COK(100), COPK(100), CDSK(100)	VCF8	8
DIMENSION CLSK(100)	VCF8	9
DIMENSION TAWD(53), TAWL(53)	VCF8	10
COMMON ALPHA, PI, PI2, RE, SRE, SQRTPI, DTOR, RTOD, RC, RCHAXSQ, SIGMA, LEVEL	VCF8	11
COMMON/KAYS/K, KS, KR, KT, KB, KRT, KRB	VCF8	12
COMMON/ELIPS2/AKPHALF, AKDOTPH	VCF8	13
COMMON/BLOCK1/X(100), Y(100), XB(100), YB(100), XRT(100), YRT(100),	VCF8	14
1 XRB(100), YRB(100)	VCF8	15
COMMON/BLOCK2/GAMMA(100), GMAB(100), GMRT(100), GMRB(100)	VCF8	16
COMMON/BLOCK3/XDOT(100), YDOT(100), XDOTB(100), YDOTB(100),	VCF8	17
1 XRDOT(100), YRDOT(100), XRDOTB(100), YRDOTB(100)	VCF8	18
COMMON/BLOCK4/TT(100), TR(100), TRT(100), TRB(100)	VCF8	19
COMMON/BLOCK5/AK, AKSQD, AKHALF, AKDOT	VCF8	20
COMMON/BLOCK10/THETAS, THETASB, THETA	VCF8	21
COMMON/BLOCK11/DS(52), DZ2, DZ8, DZSQ, DZSQ2, DZSQ4, DT2	VCF8	22
COMMON/BLOCK20/DX, DZ, INTX1, NBIG1	VCF8	23
COMMON/BLOCK30/T, TI, DELT, DELTT, DELTB	VCF8	24
COMMON/BLBOX2/TAU, PT4, NBIG	VCF8	25
COMMON/BLBOX12/ZN(51), ISEP	VCF8	26
COMMON/BLBOX13/KTS, IXRSET, IXBRSET, UTNBIG(53), UBNBIG(53)	VCF8	27
COMMON/BLOCK14/S(53), ST(53), SB(53)	VCF8	28
COMMON/BLBOX14/ZHAT, AKTI	VCF8	29
EXTERNAL CPC, DRAG, PLIFT	VCF8	30
INTEGER ALPHA	VCF8	31
REAL NOR, NU, MU	VCF8	32
REAL L, LB	VCF8	33
REAL LENGTH	VCF8	34
C ..... LENGTH=DIMENSIONAL LENGTH	VCF8	35
C ..... AATAACK=ANGLE OF ATTACK IN DEGREES	VCF8	36
C ..... A FUNCTION SUBPROGRAM NAMED RZERO(ZSTAR) MUST BE	VCF8	37
C ..... SUPPLIED BY THE USER TO ENTER THE BODY GEOMETRY.	VCF8	38
C ..... ZSTAR IS THE DIMENSIONAL DISTANCE ALONG THE BODY AXIS,	VCF8	39
C ..... AND RZERO IS THE CORRESPONDING DIMENSIONAL RADIUS.	VCF8	40
C ..... IF THE BODY GEOMETRY IS IN TABULAR FORM THEN RZEROT(ZSTAR	VCF8	41
C ..... IS AN APPROXIMATING FUNCTION	VCF8	42
C ..... V=FREE STREAM VELOCITY	VCF8	43
C ..... NU=KINEMATIC VISCOSITY	VCF8	44
C ..... INFO ..... DATA IDENTIFICATION	VCF8	45
READ(5,705) (INFO(I), I=1,16)	VCF8	46
WRITE(6,605) (INFO(I), I=1,16)	VCF8	47
READ(5,706) AATAACK, RE, LENGTH	VCF8	48
READ(5,706) DELT, RC, SIGMA	VCF8	49
READ(5,708) KFINAL, TFINAL, ZFINAL	VCF8	50
READ(5,709) LR, LW, LEVEL, KPUN	VCF8	51
PI=4.0*ATAN(1.0)	VCF8	52
DTOR=PI/180.0	VCF8	53
RTOD=180.0/PI	VCF8	54
CALL NONDIM(DMAX, RW, AW, F, SA, LENGTH, PI)	VCF8	55
WRITE(6,611) DMAX, AW, F, SA	VCF8	56
WRITE(6,606) AATAACK, RE	VCF8	57
AATAACK=DTOR*AATAACK	VCF8	58
RE=PE*SIN(AATAACK)*AW/LENGTH	VCF8	

WRITE(6,601) RE, DELT, RC, SIGMA, KFINAL, TFINAL, ZFINAL, LR, LW, LEVEL, KPUN	VCF8	59
FTA=F*TAN(AATACK)	VCF8	60
C ..... OUTPUT PARAMETERS	VCF8	61
IPUN=0	VCF8	62
C ..... COUNTERS	VCF8	63
KT=KB=0	VCF8	64
KRT=KRB=0	VCF8	65
KR=KS=KSB=1000	VCF8	66
IXTRSET=IXBRSET=INITAL=53	VCF8	67
C ..... NDIM IS THE K DIMENSION	VCF8	68
C ..... NDIM MUST BE PUT IN FREEVTX, CPC, AND RVTX	VCF8	69
NDIM=100	VCF8	70
C ..... IDIM=DIMENSION OF THETA GRID IN B.L. ROUTINE	VCF8	71
C ..... JDIM= DIMENSION OF R GRID IN B.L. ROUTINE	VCF8	72
IDIM=32		
JDIM=51	VCF8	74
C ..... CONSTANTS	VCF8	75
PI2=2.0*PI	VCF8	76
PINF=132.3/.1189	VCF8	77
SQRTPI=SQRT(PI)	VCF8	78
SQA=SIN(AATACK)**2	VCF8	79
DELT=.125	VCF8	80
SRE=SQRT(RE)	VCF8	81
C ..... ISYM=1 IS THE SYMMETRIC CASE	VCF8	82
C ..... ISYM=0 IS THE ASYMMETRIC CASE	VCF8	83
ISYM=1	VCF8	84
THTASYM=0.0	VCF8	85
C***** INITIAL CONDITIONS	VCF8	86
C***** START OF LOOP	VCF8	87
K=0	VCF8	88
IF(LR.EQ.0) GO TO 219	VCF8	89
READ(LR) K, KS, KR, KT, KB, KRT, KRB, T, DELT, NBIG, IXTRSET, IXBRSET	VCF8	90
READ(LR) (UTNBIG(I), (UT(I,J), J=1, NBIG), I=1, IXTRSET)	VCF8	91
IF(ISYM.EQ.0) READ(LR) (UBNBIG(I), (UB(I,J), J=1, NBIG), I=1, IXBRSET)	VCF8	92
IF(K.LT.KS) GO TO 219	VCF8	93
READ(LR) (X(I), Y(I), XDOT(I), YDOT(I), GAMMA(I), TT(I), I=1, KT)	VCF8	94
READ(LR) (XB(I), YB(I), XDOTB(I), YDOTB(I), GMAB(I), TB(I), I=1, KB)	VCF8	95
IF(KRT.EQ.0) GO TO 220	VCF8	96
READ(LR) (XRT(I), YRT(I), XRDOT(I), YRDOT(I), GMRT(I), TRT(I), I=1, KRT)	VCF8	97
READ(LR) (XRB(I), YRB(I), XRDOTB(I), YRDOTB(I), GMRB(I), TRB(I),	VCF8	98
1I=1, KRB)	VCF8	99
220 CONTINUE	VCF8	100
IF(K.LT.KR) GO TO 219	VCF8	101
READ(LR) THTASMT, THTASRT, UZZT, UZZSQT, GAMART, IFLGT, THTASMB,	VCF8	102
1THTASRB, UZZB, UZZSQB, GAMARB, IFLGB, NT, NB, NBT, NFB, GMTLT, GMTLB	VCF8	103
219 CONTINUE	VCF8	104
IF((K/KPUN)*KPUN.EQ.K) IPUN=2	VCF8	105
KTS=K+1	VCF8	106
IF(K.NE.0) GO TO 69	VCF8	107
T=TI=(RW/AW)*2.0*FTA*.03	VCF8	108
ZHAT=T*(AW/(RW*2.0*FTA))	VCF8	109
AK=RW/AW*RZRO(ZHAT, LENGTH, RW)	VCF8	110
AKT I=AK	VCF8	111
AKDOT=DRZRO(ZHAT, LENGTH, RW)/(2.0*FTA)	VCF8	112
CDPI=PI2*AK*AKDOT	VCF8	113
WRITE(6,620) T, ZHAT, AK, AKDOT, CDPI	VCF8	114
69 K=K+1	VCF8	115
KMI MUST=K-1	VCF8	116

T=T+DELT	VCF8 117
TH=T-DELT/2.0	VCF8 118
ZHAT=T*(AW/(RW*2.0*FTA))	VCF8 119
AK=RW/AW*RZRO(ZHAT,LENGTH,RW)	VCF8 120
AKDOT=DRZRO(ZHAT,LENGTH,RW)/(2.0*FTA)	VCF8 121
AADOT=AK*AKDOT	VCF8 122
AKSQ=AK**2	VCF8 123
ZHALF=TH*(AW/(RW*2.0*FTA))	VCF8 124
AKPHALF=AKHALF=RW/AW*RZRO(ZHALF,LENGTH,RW)	VCF8 125
AKDOTPH=DRZRO(ZHALF,LENGTH,RW)/(2.0*FTA)	VCF8 126
C ..... RCMAXSQ AND RCSQ ARE THE MAX CORE RADIUS SQUARED AND CORE	VCF8 127
C ..... RADIUS SQUARED	VCF8 128
IF(KS.LE.K)RCMAXSQ=5.04*T/RE	VCF8 129
IF(KS.LE.K)RCMAX=SQRT(RCMAXSQ)	VCF8 130
KTTEMP=KT	VCF8 131
KBTEMP=KB	VCF8 132
KT=KT+1	VCF8 133
KB=KB+1	VCF8 134
CALL BLBOX(SMALLM,DGAMMA,TAWD,TAWL,U,W,UT,UB,IDIM,JDIM,1)	VCF8 135
KT=KTTEMP	VCF8 136
KB=KBTEMP	VCF8 137
C ..... SHEAR DRAG	VCF8 138
CDST=0.0	VCF8 139
CLST=0.0	VCF8 140
INTX=ISEP-1	VCF8 141
DO 1 I=1,INTX	VCF8 142
TRAPD=DS(I)/2.0*(TAWD(I)+TAWD(I+1))	VCF8 143
TRAPL=DS(I)/2.0*(TAWL(I)+TAWL(I+1))	VCF8 144
CDST=CDST+TRAPD	VCF8 145
1 CLST=CLST+TRAPL	VCF8 146
CDSK(K)=.50*AK*CDST	VCF8 147
CLS K(K)=.50*AK*CLST	VCF8 148
C ..... UPPER HALF OF CYLINDER	VCF8 149
2 IF(K.LT.KS) GO TO 3	VCF8 150
KT=KT+1	VCF8 151
TT(KT)=T	VCF8 152
GAMMA(KT)=DELT*DGAMMA	VCF8 153
GAMMA(KT)=SIGMA*GAMMA(KT)	VCF8 154
X(KT)=(AK+SMALLM)*COS(THETAS)	VCF8 155
Y(KT)=(AK+SMALLM)*SIN(THETAS)	VCF8 156
IF(ISYM.EQ.0) GO TO 3	VCF8 157
KB=KB+1	VCF8 158
XB(KB)=X(KT)	VCF8 159
YB(KB)=-Y(KT)	VCF8 160
GMA B(KB)=-GAMMA(KT)	VCF8 161
TB(KB)=T	VCF8 162
3 CONTINUE	VCF8 163
IF(THETAS.LT.THTASYM.OR.ISYM.EQ.0) GO TO 100	VCF8 164
GO TO 101	VCF8 165
C***** SYMMETRIC CASE	VCF8 166
100 KBTEMP=KB	VCF8 167
KB=KB+1	VCF8 168
CALL BLBOX(SMALLM,DGAMMA,TAWD,TAWL,U,W,UT,UB,IDIM,JDIM,2)	VCF8 169
KB=KBTEMP	VCF8 170
C ..... ASYMMETRIC CASE	VCF8 171
C ..... LOWER HALF OF CYLINDER	VCF8 172
C ..... SHEAR DRAG	VCF8 173
CDSB=0.0	VCF8 174

2	CLSB=0.0	VCF8	175
3	INT X=ISEP-1	VCF8	176
4	DO 5 I=1,INTX	VCF8	177
5	TRAPD=DS(I)/2.0*(TAWD(I)+TAWD(I+1))	VCF8	178
6	TRAPL=DS(I)/2.0*(TAWL(I)+TAWL(I+1))	VCF8	179
7	CDSB=CDSB+TRAPD	VCF8	180
8	CLSB=CLSB+TRAPL	VCF8	181
9	CDSK(K)=CDSK(K)-.50*AK*CDSB	VCF8	182
10	CLSK(K)=CLSK(K)-.50*AK*CLSB	VCF8	183
11	IF(K.LT.KSB) GO TO 7	VCF8	184
12	KB=KB+1	VCF8	185
13	TB(KB)=T	VCF8	186
14	GMA B(KB)=-DELT*DGAMMA	VCF8	187
15	GMA P(KB)=SIGMA*GMA B(KB)	VCF8	188
16	XB(KB)=(AK+SMALLM)*COS(THETASB)	VCF8	189
17	YB(KB)=(AK+SMALLM)*SIN(THETASB)	VCF8	190
18	CONTINUE	VCF8	191
19	GO TO 9	VCF8	192
20	101 CONTINUE	VCF8	193
21	C ..... SYMMETRIC CASE	VCF8	194
22	CDSK(K)=2.0*CDSK(K)	VCF8	195
23	CLSK(K)=0.0	VCF8	196
24	DO 102 I=1,IXTRSET	VCF8	197
25	UBNBIG(I)=-UTNBIG(I)	VCF8	198
26	DO 102 J=1,NBIG	VCF8	199
27	102 UB(I,J)=-UT(I,J)	VCF8	200
28	IXBPSET=IXTRSET	VCF8	201
29	THETASB=PIZ-THETAS	VCF8	202
30	KSB=KS	VCF8	203
31	KB=KT	VCF8	204
32	CONTINUE	VCF8	205
33	C ..... XDOT,YDOT CALCULATIONS	VCF8	206
34	IF(K.LT.KS) GO TO 85	VCF8	207
35	CALL VEL(X,Y,XDOT,YDOT,NDIM,1,KT,1)	VCF8	208
36	IF(ISYM.EQ.0) GO TO 81	VCF8	209
37	DO 80 I=1,KT	VCF8	210
38	XDOTB(I)=XDOT(I)	VCF8	211
39	YDOTB(I)=-YDOT(I)	VCF8	212
40	80 CONTINUE	VCF8	213
41	GO TO 82	VCF8	214
42	81 CONTINUE	VCF8	215
43	CALL VEL(XB,YB,XDOTB,YDOTB,NDIM,1,KB,2)	VCF8	216
44	82 CONTINUE	VCF8	217
45	IF(KRT.EQ.0) GO TO 85	VCF8	218
46	CALL VEL(XRT,YRT,XRDOT,YRDOT,NDIM,1,KRT,4)	VCF8	219
47	IF(ISYM.EQ.0) GO TO 81	VCF8	220
48	DO 83 I=1,KRT	VCF8	221
49	XRDOTB(I)=XRDOT(I)	VCF8	222
50	YRDOTB(I)=-YRDOT(I)	VCF8	223
51	83 CONTINUE	VCF8	224
52	GO TO 85	VCF8	225
53	84 CONTINUE	VCF8	226
54	CALL VEL(XRB,YRB,XRDOTB,YRDOTB,NDIM,1,KRB,5)	VCF8	227
55	85 CONTINUE	VCF8	228
56	C ..... END XDOT,YDOT CALCULATIONS	VCF8	229
57	C ..... PRINTOUT	VCF8	230
58	C .....	VCF8	231
59	IPUN=IPUN-1	VCF8	232

IF(K/KPUN)*KPUN.EQ.K) IPUN=2	VCF8 233
IW=6	VCF8 234
IF(IPUN.GE.1) IW=7	VCF8 235
IF(K.GE.KS) WRITE(6,600)	VCF8 236
IF(K.GE.KS) CALL WRIT(X,Y,XDOT,YDOT,GAMMA,XB.YB,XDOTB,YDOTB,GHAB,	VCF8 237
11,KT,1,KB,K,NDIM,IW)	VCF8 238
IF(KRT.GT.0) WRITE(6,602)	VCF8 239
IF(KRT.GT.0) CALL WRIT(XRT,YRT,XRDOT,YRDOT,GMRT,XRB,YRB,XRDOTB,	VCF8 240
*YRDOTB,GMRB,1,KRT,1,KRB,K,NDIM,IW)	VCF8 241
C ..... END PRINTOUT	VCF8 242
CDP=4.0*PI*AKDOT	VCF8 243
SEPDEG=THETAS*RTOD	VCF8 244
IF(K.GE.KS.AND.LEVEL.GE.4) WRITE(6,622)T,ZHAT,AK,AKDOT,SEPDEG	VCF8 245
IF(K.GE.KS) CALL DQI(PDRAG,CDP,K,5,ISYM)	VCF8 246
CDPK(K)=.5*AK*CDP	VCF8 247
CDK(K)=CDSK(K)+CDPK(K)	VCF8 248
CDN=(AW/RW)*CDK(K)*SQA	VCF8 249
WRITE(6,603)K,CDPK(K),CDSK(K),CDK(K),CDN	VCF8 250
IF(KPUN.NE.0) WRITE(7,755)ZHAT,CDK(K),T,K	VCF8 251
IF(K.LT.KR) GO TO 78	VCF8 252
KTEMP=KRT	VCF8 253
CALL RSEP(THETAS,THTASR,ST,UTNBIG,IXTRSET,INITAL,1)	VCF8 254
CALL RVTX(XRT,YRT,GMRT,THTASR,THTASMT,THTASRT,UZZT,UZZSQT,GAMART,	VCF8 255
11,KRT,NT,NFT,IFLGT,GMTLT,NDIM,TRT)	VCF8 256
IF(KTEMP.EQ.KRT) GO TO 78	VCF8 257
KRB=KRT	VCF8 258
TRB(KRB)=TRT(KRT)	VCF8 259
GMRB(KRB)=-GMRT(KRT)	VCF8 260
XRb(KRB)=XRT(KRT)	VCF8 261
YRB(KRB)=-YRT(KRT)	VCF8 262
CALL VEL(XRT,YRT,XRDOT,YRDOT,NDIM,KRT,KRT,4)	VCF8 263
XRDOTB(KRB)=XRDOT(KRT)	VCF8 264
YRDOTB(KRB)=-YRDOT(KRT)	VCF8 265
IF(ISYM.EQ.1) GO TO 79	VCF8 266
KTEMP=KRB	VCF8 267
CALL RSEP(THETASB,THTASR,SB,UBNBIG,IXBRSET,INITAL,2)	VCF8 268
CALL RVTX(XRB,YRB,GMRB,THTASR,THTASMB,THTASRB,UZZB,UZZSQB,GAMARB,	VCF8 269
12,KRB,NB,NFB,IFLGB,GMTLB,NDIM,TRB)	VCF8 270
IF(KTEMP.EQ.KRB) GO TO 78	VCF8 271
CALL VEL(XRB,YRB,XRDOTB,YRDOTB,NDIM,KRB,KRB,5)	VCF8 272
79 CONTINUE	VCF8 273
78 CONTINUE	VCF8 274
C ..... VORTEX MOTION	VCF8 275
IF(K.LT.KS) GO TO 95	VCF8 276
CALL VM(X,Y,XDOT,YDOT,NDIM,1,KT,DELT)	VCF8 277
IF(ISYM.EQ.0) GO TO 91	VCF8 278
DO 90 I=1,KT	VCF8 279
XB(I)=X(I)	VCF8 280
YB(I)=-Y(I)	VCF8 281
90 CONTINUE	VCF8 282
GO TO 92	VCF8 283
91 CONTINUE	VCF8 284
CALL VM(XB,YB,XDOTB,YDOTB,NDIM,1,KB,DELT)	VCF8 285
92 CONTINUE	VCF8 286
IF(KRT.EQ.0) GO TO 95	VCF8 287
CALL VM(XRT,YRT,XRDOT,YRDOT,NDIM,1,KRT,DELT)	VCF8 288
IF(ISYM.EQ.0) GO TO 94	VCF8 289
DO 93 I=1,KRT	VCF8 290

1	XRB(I)=XRT(I)	VCF8 291
2	YRB(I)=-YRT(I)	VCF8 292
993	CONTINUE	VCF8 293
994	GO TO 95	VCF8 294
994	CONTINUE	VCF8 295
994	CALL VM(XRB,YRB,XRDOTB,YRDOTB,NDIM,1,KRB,DELT)	VCF8 296
995	CONTINUE	VCF8 297
995	END VORTEX MOTION	VCF8 298
995	CALL SECOND(TIME)	VCF8 299
995	WRITE(6,612) TIME	VCF8 300
995	IF(K.EQ.KFINAL.OR.TIME.GE.TFINAL.OR.ZHAT.GE.ZFINAL) GO TO 221	VCF8 301
995	GO TO 69	VCF8 302
221	CONTINUE	VCF8 303
221	WRITE(LW) K,KS,KR,KT,KB,KRT,KRB,T,DELT,NBIG,IXTRSET,IXBRSET	VCF8 304
221	WRITE(LW) (UTNBIG(I),(UT(I,J),J=1,NBIG),I=1,IXTRSET)	VCF8 305
221	IF(ITYM.EQ.0)WRITE(LW)(UBNBIG(I),(UB(I,J),J=1,NBIG),I=1,IXBRSET)	VCF8 306
221	IF(K.LT.KS) GO TO 223	VCF8 307
221	WRITE(LW) (X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I),TT(I),I=1,KT)	VCF8 308
221	WRITE(LW) (XRB(I),YRB(I),XRDOTB(I),YRDOTB(I),GMAB(I),TB(I),I=1,KB)	VCF8 309
221	IF(KRT.EQ.0) GO TO 222	VCF8 310
221	WRITE(LW) (XRT(I),YRT(I),XRDOT(I),YRDOT(I),GMRT(I),TRT(I),I=1,KRT)	VCF8 311
221	WRITE(LW) (XRB(I),YRB(I),XRDOTB(I),YRDOTB(I),GMRB(I),TRB(I),	VCF8 312
221	I=1,KRB)	VCF8 313
222	CONTINUE	VCF8 314
222	IF(K.LT.KR) GO TO 223	VCF8 315
222	WRITE(LW)THTASMT,THTASRT,UZZT,UZZS, GAMART,IFLGT,THTASMB,	VCF8 316
222	1THTASRB,UZZB,UZZSOB,GAMARB,IFLGB,NT.NB,NFT.NFB,GMTLT,GMTLB	VCF8 317
223	CONTINUE	VCF8 318
600	FORMAT(/50X*POINT VORTEX LOCATIONS*/27X*TOP BOUNDARY LAYER*44X	VCF8 319
600	1*BOTTOM BOUNDARY LAYER*//,	VCF8 320
600	1 * A K*6X*X(A)*8X*Y(A)*7X*XDOT(A)*4X*YDOT(A)*6X	VCF8 321
600	1*GAMMA(A)*3X*XB(A)*7X*YB(A)*6X*XDOTB(A)*4X*YDOTB(A)*6X*GMAB(A)*	VCF8 322
601	FORMAT( * 2DUS REYNOLDS NO.=*F11.2,/* 2DUS PARAMETERS*/	VCF8 323
601	1*DELT=*F5.3,/* RC=*F5.3,/* SIGMA=*F5.3,/* PROGRAM CONTROL*7	VCF8 324
601	2* KFINAL=*I3,/* TFINAL=*F6.1,/* ZFINAL=*F5.3,/* LR=*I3,/* LW=*I3,/*	VCF8 325
601	4* LEVEL=*I3,/* KPUN=*I3)	VCF8 326
602	FORMAT(/25X*TOP REAR SHEAR LAYER*44X*BOTTOM REAR SHEAR LAYER*//,	VCF8 327
602	1 * A K*6X*XRT(A)*6X*YRT(A)*5X*XRDOT(A)*3X*YRDOT(A)*5X	VCF8 328
602	1*GMRT(A)*4X*XRB(A)*5X*YRB(A)*4X*XRDOTB(A)*2X*YRDOTB(A)*4X	VCF8 329
602	1*GMAB(A)*	VCF8 330
603	FORMAT(//* K=*I3,/* CDPK=*F12.6,/* CDSK=*F12.6,/* CDK=*F12.6,	VCF8 331
603	1/* CON=*F12.6)	VCF8 332
605	FORMAT(1H1,20X,16A5 //)	VCF8 333
606	FORMAT(* ANGLE OF ATTACK=*F5.1,* DEGREES/* 3DS REYNOLDS NO.=*F11.	VCF8 334
606	12)	VCF8 335
611	FORMAT(/42X*DMAX=*F7.4,42X* AM=*F7.4,42X* F=*F7.4,42X,	VCF8 336
611	1* S=*F7.4,//)	VCF8 337
612	FORMAT(* ELAPSED TIME=*F12.6)	VCF8 338
620	FORMAT(* ..... TI=*F12.6,* ..... ZHAT(TI)=*F12.6,/* ..... AK(TI)=*	VCF8 339
620	1F12.6,* ..... AKDOT(TI)=*F12.6,* ..... CDPI=*F12.6)	VCF8 340
622	FORMAT(1H1,40X*PRESSURE DISTRIBUTION*/14X*T=*F7.4,5X*ZHAT=*F7.4,5X	VCF8 341
622	1*AK=*F7.4,5X*AKDOT=*F7.4,5X*THETAS=*F7.2,/*3X*DEG*8X*PHIVT*8X	VCF8 342
622	2*PHIPT*8X*2(PHIT)*6X*-PSIKSQ*5X*CPK*10X*PORAG*8X*UTAN*)	VCF8 343
705	FORMAT(16A5)	VCF8 344
706	FORMAT(3F12.6)	VCF8 345
708	FORMAT(I3,9X,2F12.6)	VCF8 346
709	FORMAT(4I2)	VCF8 347
755	FORMAT(3F12.6,I3)	VCF8 348

```

FUNCTION AN(L,N,IDIM,JDIM,U,W)
DIMENSION U(IDIM,2,JDIM),W(IDIM,JDIM)
COMMON/ALOCK11/DS(52),DZ2,DZ8,DZSQ,DZSQ2,DZSQ4,DT2
AN=DZ8*W(L,N)-DZSQ4
RETURN
ENTRY BN
DX4=.25/DS(L)
BN=DT2+DX4*(U(L+1,2,N)+U(L+1,1,N))+DZSQ2
RETURN
ENTRY CN
CN=-DZ8*W(L,N)-DZSQ4
RETURN
END

```

AN	1
AN	2
AN	3
AN	4
AN	5
AN	6
AN	7
AN	8
AN	9
AN	10
AN	11
AN	12
AN	13

SUBROUTINE BLBOX(SMALLM,DGAMMA,TAWD,TAWL,U,W,UT,UB,IDIM,JDIM,MODE)	BLBOX	1
DIMENSION U(IDIM,2,JDIM),W(IDIM,JDIM),UT(IDIM,JDIM),UB(IDIM,JDIM)	BLBOX	2
DIMENSION SUP(49),SUB(49),DIAG(49),R(49)	BLBOX	3
DIMENSION TAWD(53),TAWL(53)	BLBOX	4
DIMENSION THTA(53)	BLBOX	5
DIMENSION NX(53),DEG(53)	BLBOX	6
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RMAXSQ,SIGMA,LEVEL	BLBOX	7
COMMON/KAYS/K,KS,KR,KT,KB,KRT,KRB	BLBOX	8
COMMON/ELIPS2/AKPHALF,AKDOTPH	BLBOX	9
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	BLBOX	10
COMMON/BLOCK10/THETAS,THETASB,THETA	BLBOX	11
COMMON/BLOCK11/DS(52),DZ2,DZ8,DZSQ,DZSQ2,DZSQ4,DT2	BLBOX	12
COMMON/BLOCK28/OX,DZ,INTX1,NBIG1	BLBOX	13
COMMON/BLOCK30/T,TT,DELT,DELTT,DELTB	BLBOX	14
COMMON/BLBOX2/TAU,PT4,NBIG	BLBOX	15
COMMON/BLBOX12/ZN(51),ISEP	BLBOX	16
COMMON/BLBOX13/KTS,IXTRSET,IXBRSET,UTNBIG(53),UBNBIG(53)	BLBOX	17
COMMON/BLBOX14/ZHAT,AKTI	BLBOX	18
COMMON/BLOCK14/S(53),ST(53),SB(53)	BLBOX	19
C***** MODE1 IMPLIES 0 DEGREES.LT.THETA.LT. 80 DEGREES	BLBOX	20
C***** MODE2 IMPLIES -80 DEGREES.LT.THETA.LT. 0 DEGREES	BLBOX	21
C***** RBAR CORRESPONDS TO Z	BLBOX	22
C***** THETA CORRESPONDS TO X	BLBOX	23
LEVEL=5	BLBOX	24
IF(K.GT.KTS.OR.MODE.EQ.2) GO TO 9	BLBOX	25
C***** INITIAL DETERMINES INITIAL GRID POINTS	BLBOX	26
RTOD=180.0/PI	BLBOX	27
DTOR=PI/180.0	BLBOX	28
INITAL=53	BLBOX	29
INTX1=IXTRSET	BLBOX	30
IF(IXBRSET.GT.IXTRSET) INTX1=IXBRSET	BLBOX	31
DELS=5.0*DTOR	BLBOX	32
ST(1)=0.0	BLBOX	33
SB(1)=PI2	BLBOX	34
DO 19 I=2,INITAL	BLBOX	35
IF(I.LE.15.OR.I.GE.36) GO TO 18	BLBOX	36
ST(I)=ST(I-1)+DELS/5.0	BLBOX	37
SB(I)=SB(I-1)-DELS/5.0	BLBOX	38
GO TO 19	BLBOX	39
18 ST(I)=ST(I-1)+DELS	BLBOX	40
SB(I)=SB(I-1)-DELS	BLBOX	41
19 CONTINUE	BLBOX	42
Z0=0.0	BLBOX	43
INT Z=50	BLBOX	44
INT Z1=INTZ+1	BLBOX	45
NBIG1=INTZ	BLBOX	46
NBIG=INT Z1	BLBOX	47
DZ=.14	BLBOX	48
DZ2=0.5/DZ	BLBOX	49
DZ8=0.125/DZ	BLBOX	50
DZSQ=1.0/(DZ*DZ)	BLBOX	51
DZSQ2=0.5/(DZ*DZ)	BLBOX	52
DZSQ4=0.25/(DZ*DZ)	BLBOX	53
ZN(1)=Z0	BLBOX	54
C***** RBAR VARIATION	BLBOX	55
DO 22 J=2,NBIG	BLBOX	56
RJ=J	BLBOX	57
Z=Z0+(RJ-1.0)*DZ	BLBOX	58



72	ZN(J)=Z	BLBOX	59
	E=10.0** -5	BLBOX	60
	THE TAS=ST(IXTRSET)	BLBOX	61
	THE TASB=SB(IXBRSET)	BLBOX	62
C*****	THETA VARIATION	BLBOX	63
9	CONTINUE	BLBOX	64
C*****	TOP HALF	BLBOX	65
	INTX1=ISEP=IXTRSET	BLBOX	66
	IF(MODE.EQ.2)INTX1=ISEP=IXBRSET	BLBOX	67
	INTX=INTX1-1	BLBOX	68
	IF(K.EQ.1)CALL IC(AKI,U,IDIM,JOIM,MODE)	BLBOX	69
	DO 200 I=1,INITAL	BLBOX	70
	GO TO(204,206) MODE	BLBOX	71
204	S(I)=ST(I)	BLBOX	72
	GO TO 208	BLBOX	73
206	S(I)=SB(I)	BLBOX	74
208	THTA(I)=S(I)	BLBOX	75
	DEG(I)=THTA(I)*RTOD	BLBOX	76
	IF(I.EQ.1) GO TO 213	BLBOX	77
	DS(I-1)=S(I)-S(I-1)	BLBOX	78
	DS(I-1)=DS(I-1)*AKHALF**2	BLBOX	79
C*****	B.C. RBAR=0	BLBOX	80
213	IF(I.GT.INTX1) GO TO 214	BLBOX	81
	U(I,1,1)=0.0	BLBOX	82
	U(I,2,1)=0.0	BLBOX	83
	JI=2	BLBOX	84
	GO TO 215	BLBOX	85
214	JI=NBIG	BLBOX	86
215	DO 200 J=JI,NBIG	BLBOX	87
C*****	B.C. THETA=0	BLBOX	88
	IF(1.NE.1) GO TO 201	BLBOX	89
	U(I,1,J)=0.0	BLBOX	90
	U(I,2,J)=0.0	BLBOX	91
	GO TO 200	BLBOX	92
201	IF(J.NE.NBIG) GO TO 202	BLBOX	93
C*****	B.C. RBAR=INF	BLBOX	94
	THETA=THTA(I)	BLBOX	95
	CALL FREEVTX(PSIK1X,PSIK1Y,PSIK1R,3)	BLBOX	96
	CALL POTFLOW(PSIKXP,PSIKYP,PSIKRP,3)	BLBOX	97
	IF(1.GT.INTX1) GO TO 203	BLBOX	98
	U(I,2,NBIG)=AK*(PSIK1R+PSIKRP)	BLBOX	99
	GO TO (205,207) MODE	BLBO	100
203	GO TO (211,212) MODE	BLBO	101
205	U(I,1,NBIG)=UTNBIG(I)	BLBO	102
211	UTNBIG(I)=AK*(PSIK1R+PSIKRP)	BLBO	103
	GO TO 200	BLBO	104
207	U(I,1,NBIG)=UBNBIG(I)	BLBO	105
212	UBNBIG(I)=AK*(PSIK1R+PSIKRP)	BLBO	106
	GO TO 200	BLBO	107
202	IF(K.EQ.1) GO TO 200	BLBO	108
	GO TO(209,210) MODE	BLBO	109
209	U(I,1,J)=U(I,1,J)	BLBO	110
	GO TO 200	BLBO	111
210	U(I,1,J)=UB(I,J)	BLBO	112
200	CONTINUE	BLBO	113
40	CONTINUE	BLBO	114
	DT2=.5/DELT	BLBO	115
	DO 180 I=1,INTX	BLBO	116

NCYCLE=0	BLBO 117
TAUNEW=0.0	BLBO 118
W(I,1)=0.0	BLBO 119
50 NCYCLE=NCYCLE+1	BLBO 120
DO 140 J=2,NBIG1	BLBO 121
TAUS=TAUNEW	BLBO 122
Z=ZN(J)	BLBO 123
90 IF (NCYCLE.GT.1) GO TO 100	BLBO 124
U(I+1,2,J)=UAPRX1(I,J,IDIM,JDIM,U)	BLBO 125
100 DZDX=DZ/(4.0*DS(I))	BLBO 126
W(I,J)=W(I,J-1)-DZDX*(U(I+1,2,J)+U(I+1,2,J-1)+	BLBO 127
1UL(I,J,IDIM,JDIM,U)+UL(I,J-1,IDIM,JDIM,U))	BLBO 128
W(I,J)=W(I,J)-DZ*AKDOTPH/AKPHALF	BLBO 129
IF(J.EQ.2) GO TO 110	BLBO 130
SUB(J-2)=CN(I,J,IDIM,JDIM,U,W)	BLBO 131
110 DIAG(J-1)=BN(I,J,IDIM,JDIM,U,W)	BLBO 132
IF (J.EQ.NBIG1) GO TO 120	BLBO 133
SUP(J-1)=AN(I,J,IDIM,JDIM,U,W)	BLBO 134
120 R(J-1)=DN(I,J,IDIM,JDIM,U,W)	BLBO 135
140 CONTINUE	BLBO 136
160 CALL TRID(49,SUP,SUB,DIAG,R)	BLBO 137
DO 170 JJ=2,NBIG1	BLBO 138
U(I+1,2,JJ)=R(JJ-1)	BLBO 139
IF(MODE.EQ.1) UT(I+1,JJ)=R(JJ-1)	BLBO 140
IF(MODE.EQ.2) UB(I+1,JJ)=R(JJ-1)	BLBO 141
170 CONTINUE	BLBO 142
C ***** WALL FRICTION AT EACH X STATION	BLBO 143
TAUNEW=2.0*U(I+1,2,2)/DZ	BLBO 144
IF(NCYCLE.GE.20) GO TO 179	BLBO 145
IF(ABS(TAUNEW-TAUS).GT.E.OR.NCYCLE.LE.2) GO TO 50	BLBO 146
179 CONTINUE	BLBO 147
NX(I+1)=NCYCLE	BLBO 148
180 CONTINUE	BLBO 149
C..... UI GOES TO UBAR	BLBO 150
C..... UI REMAINS IN UT AND UB ARRAYS	BLBO 151
DO 182 I=1,INTX1	BLBO 152
DO 182 J=1,NBIG	BLBO 153
182 U(I,2,J)=U(I,2,J)/AK	BLBO 154
IF(MODE.EQ.2) GO TO 28	BLBO 155
IF(LEVEL.GE.4)CALL RITE(2,IDIM,JDIM,U,ZN,NX,S,DEG,ZHAT,DELS,K)	BLBO 156
28 CONTINUE	BLBO 157
C .SEARCH ALONG SURFACE FOR ZERO SHEAR POINT	BLBO 158
300 DO 302 I=1,INTX1	BLBO 159
DUDR=(U(I,2,2)-U(I,2,1))/DZ	BLBO 160
TAW=(2.0/SRE)*DUDR	BLBO 161
GO TO(305,306) MODE	BLBO 162
305 IF(I.EQ.1.OR.I.EQ.INITAL.OR.TAW.GT.0.0) GO TO 301	BLBO 163
ISEP=I-1	BLBO 164
GO TO 303	BLBO 165
306 IF(I.EQ.1.OR.I.EQ.INITAL.OR.TAW.LT.0.0) GO TO 301	BLBO 166
ISEP=I-1	BLBO 167
GO TO 303	BLBO 168
301 TAWL(I)=TAW*COS(THTA(I))	BLBO 169
302 TAWD(I)=TAW*SIN(THTA(I))	BLBO 170
303 CONTINUE	BLBO 171
C .FLOW HAS NOT SEPARATED... SKIP W CALC	BLBO 172
IF(ISEP.EQ.INITAL) GO TO 309	BLBO 173
C .FLOW HAS SEPARATED ... SEPARATION POINT	BLBO 174

C		.DEFINED 5 DEGREES UPSTREAM	BL80 175
	310	IF(MODE.NE.1) GO TO 304	BL80 176
C		.TOP	BL80 177
		IXTRSET=ISEP	BL80 178
		THE TAS=THTA(ISEP)	BL80 179
		IF(KS.EQ.1000) KS=K	BL80 180
		GO TO 307	BL80 181
C		.BOTTOM	BL80 182
	304	IXBRSET=ISEP	BL80 183
		THE TASB=THTA(ISEP)	BL80 184
		IF(KSB.EQ.1000) KSB=K	BL80 185
	307	IFLAG=0	BL80 186
		PSIKR=U(ISEP,2,NBIG)	BL80 187
		U00=ABS(PSIKR)	BL80 188
		SMALLM=DELT*U00/PI2	BL80 189
		DGAMMA=(U00**2)/2.0	BL80 190
	309	CONTINUE	BL80 191
		WRITE(6,602) DGAMMA, SMALLM	BL80 192
	602	FORMAT(//* DGAMMA=*F12.6,5X*SMALLM=*F12.6)	BL80 193
		RETURN	BL80 194
		END	BL80 195

FUNCTION CPC(THTA)	CPC	1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RMAXSQ,SIGMA,LEVEL	CPC	2
COMMON/KAYS/K,KS,KR,KT,KB,KRT,KRB	CPC	3
COMMON/PSURE/XX,YY,SINE,COSINE	CPC	4
COMMON/BLOCK1/X(100),Y(100),XB(100),YB(100),XRT(100),YRT(100),	CPC	5
1 XRB(100),YRB(100)	CPC	6
COMMON/BLOCK2/GAMMA(100),GMAB(100),GMRT(100),GMRB(100)	CPC	7
COMMON/BLOCK3/XDOT(100),YDOT(100),XDOTB(100),YDOTB(100),	CPC	8
1 XRDOT(100),YRDOT(100),XRDOTB(100),YRDOTB(100)	CPC	9
COMMON/BLOCK4/TT(100),TB(100),TRT(100),TRB(100)	CPC	10
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	CPC	11
COMMON/BLOCK7/PHIVT,PHIPT,P1,P2,P3,P4	CPC	12
COMMON/BLOCK10/THETAS,THETASB,THETA	CPC	13
INTEGER A	CPC	14
REAL L,LB	CPC	15
THETA=THTA	CPC	16
NDIM=100	CPC	17
PHIVT=0.0	CPC	18
SINE=SIN(THETA)	CPC	19
COSINE=COS(THETA)	CPC	20
IF(KT.LE.1) GO TO 10	CPC	21
XX=AK*COSINE	CPC	22
YY=AK*SINE	CPC	23
KMINUS1=KT-1	CPC	24
CALL PV(X,Y,XDOT,YDOT,GAMMA,NDIM,1,KMINUS1,SUM,TT)	CPC	25
PHIVT=PHIVT+SUM	CPC	26
IF(KRT.EQ.0) GO TO 10	CPC	27
CALL PV(XRT,YRT,XRDOT,YRDOT,GMRT,NDIM,1,KRT,SUM,TRT)	CPC	28
PHIVT=PHIVT+SUM	CPC	29
10 IF(KB.LE.1) GO TO 20	CPC	30
KMINUS1=KB-	CPC	31
CALL PV(XB,YB,XDOTB,YDOTB,GMAB,NDIM,1,KMINUS1,SUM,TB)	CPC	32
PHIVT=PHIVT+SUM	CPC	33
IF(KRB.EQ.0) GO TO 20	CPC	34
CALL PV(XRB,YRB,XRDOTB,YRDOTB,GMRB,NDIM,1,KRB,SUM,TRB)	CPC	35
PHIVT=PHIVT+SUM	CPC	36
20 CONTINUE	CPC	37
PHIPT=2.0*AKDOT*COSINE	CPC	38
PHIT=PHIPT+PHIVT	CPC	39
P1=2.0*PHIT	CPC	40
CALL FREEVTX(Psik1X,PSik1Y,PSik1R,3)	CPC	41
CALL POTFLOW(PsikXP,PSikYP,PSikRP,3)	CPC	42
PSIKR2=PSIK1R+PSIKRP	CPC	43
IF(PSIKR2.LE.-.1.AND.KR.EQ.1000) KR=K	CPC	44
P4=PSIKR2	CPC	45
PSIKSQD=PSIKR2**2	CPC	46
P2=-PSIKSQD	CPC	47
CPC=2.0*PHIT-PSIKSQD	CPC	48
P3=CPC	CPC	49
RETURN	CPC	50
END	CPC	51

FUNCTION DN(L,N,JDIM,JOIM,U,W)	DN	1
DIMENSION U(IDIM,2,JDIM),W(IDIM,JDIM)	DN	2
COMMON/BLBOX2/TAU,PT4,NBIG	DN	3
COMMON/BLOCK11/DS(52),DZ2,DZ8,DZSQ,DZSQ2,DZSQ4,DT2	DN	4
COMMON/BLOCK20/DX,DZ,INTX1,NBIG1	DN	5
DX8=.125/DS(L)	DN	6
DX2=.5/DS(L)	DN	7
DN=DX8*U(L+1,2,N)**2-DT2*UM(L,N,JDIM,JOIM,U)-	DN	8
1DX2*US(L,N,JDIM,JOIM,U)*UL(L,N,JDIM,JOIM,U)	DN	9
DN=DN+DT2*(U(L+1,2,NBIG)+UM(L,NBIG,JDIM,JOIM,U))	DN	10
DN=DN+DX2*(U(L+1,2,NBIG)/4.0+US(L,NBIG,JDIM,JOIM,U))	DN	11
1*(U(L+1,2,NBIG)+UL(L,NBIG,JDIM,JOIM,U))	DN	12
UNS1=US(L,N+1,JDIM,JOIM,U)	DN	13
UNS2=US(L,N+1,JDIM,JOIM,U)-2.0*US(L,N,JDIM,JOIM,U)	DN	14
IF(N.EQ.1) GO TO 30	DN	15
UNS1=UNS1-US(L,N-1,JDIM,JOIM,U)	DN	16
UNS2=UNS2+US(L,N-1,JDIM,JOIM,U)	DN	17
30 DN=DN-DZ2*UNS1*W(L,N)+DZSQ*UNS2	DN	18
IF (N.LT.NBIG1) GO TO 40	DN	19
DN=DN-AN(L,NBIG1,JDIM,JOIM,U,W)*U(L+1,2,NBIG)	DN	20
40 RETURN	DN	21
END	DN	22

	SUBROUTINE DQI(FCT,CK,K,N,ISYM)	DQI	1
	. THE FRONT OF THE CYLINDER IS DIVIDED INTO 2N EQUAL PARTS	DQI	2
C	. THE FRONT IS DEFINED AS -60 DEG.LE.THETA.LE.60 DEG	DQI	3
C	. THE BACK OF THE CYLINDER IS DIVIDED INTO 8N EQUAL PARTS	DQI	4
C	. N MUST BE AN EVEN INTEGER	DQI	5
	PI=4.0*ATAN(1.0)	DQI	6
	IFLAG=0	DQI	7
	XX=0.0	DQI	8
	SIMP=0.0	DQI	9
	H=6.0/N*PI/180.0	DQI	10
	NB=2*N	DQI	11
	H3=H/3.0	DQI	12
	NF=N/2	DQI	13
	F0=FCT(XX)	DQI	14
10	DO 1 I=1,NF	DQI	15
	XX=XX+H	DQI	16
	F1=FCT(XX)	DQI	17
	XX=XX+H	DQI	18
	F2=FCT(XX)	DQI	19
	SIMP=SIMP+H3*(F2+4.0*F1+F0)	DQI	20
1	F0=F2	DQI	21
	IF(IFLAG.EQ.1) GO TO 5	DQI	22
	H=H/2.0	DQI	23
	H3=H/3.0	DQI	24
20	DO 2 I=1,NB	DQI	25
	XX=XX+H	DQI	26
	F1=FCT(XX)	DQI	27
	XX=XX+H	DQI	28
	F2=FCT(XX)	DQI	29
	SIMP=SIMP+H3*(F2+4.0*F1+F0)	DQI	30
2	F0=F2	DQI	31
	IF(IFLAG.EQ.0) GO TO 30	DQI	32
	H=H*2.0	DQI	33
	H3=H/3.0	DQI	34
	GO TO 10	DQI	35
30	KMINUS1=K-1	DQI	36
	IF(ISYM.EQ.0) GO TO 4	DQI	37
	CK=2.0*SIMP	DQI	38
	RETURN	DQI	39
4	IFLAG=1	DQI	40
	GO TO 20	DQI	41
5	CK=SIMP	DQI	42
	RETURN	DQI	43
	END	DQI	44

SUBROUTINE FREEVTX(PSIK1X,PSIK1Y,PSIK1R,IA)	FREEVT 1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,OTOR,RTOD,RC,RCHXSQ,SIGMA,LEVEL	FREEVT 2
COMMON/KAYS/K,KS,KR,KT,KB,KRT,KRB	FREEVT 3
COMMON/BLOCK1/X(100),Y(100),XB(100),YB(100),XRT(100),YRT(100),	FREEVT 4
1 XRB(100),YRB(100)	FREEVT 5
COMMON/BLOCK2/GAMMA(100),GMAB(100),GMRT(100),GMRB(100)	FREEVT 6
COMMON/BLOCK4/TT(100),TB(100),TRT(100),TRB(100)	FREEVT 7
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	FREEVT 8
COMMON/BLOCK10/THETAS,THETASB,THETA	FREEVT 9
COMMON/VTX1/XX,YY	FREEV 10
INTEGER A,B,ALPHA	FREEV 11
REAL LB,L	FREEV 12
NDIM=100	FREEV 13
PSIK1R=0.0	FREEV 14
PSIK1X=0.0	FREEV 15
PSIK1Y=0.0	FREEV 16
GO TO(1,2,3,4,5) IA	FREEV 17
1 XX=X(ALPHA)	FREEV 18
YY=Y(ALPHA)	FREEV 19
C ..... DERIVATIVE OF PSI W.R.T. X	FREEV 20
C ..... VORTEX MOTION TOP	FREEV 21
GO TO 20	FREEV 22
2 XX=XB(ALPHA)	FREEV 23
YY=YB(ALPHA)	FREEV 24
C ..... DERIVATIVE OF PSI W.R.T. Y	FREEV 25
C ..... VORTEX MOTION BOTTOM	FREEV 26
GO TO 20	FREEV 27
4 XX=XRT(ALPHA)	FREEV 28
YY=YRT(ALPHA)	FREEV 29
GO TO 20	FREEV 30
5 XX=XRB(ALPHA)	FREEV 31
YY=YRB(ALPHA)	FREEV 32
20 IF(KT.LE.1) GO TO 23	FREEV 33
KMINUS1=KT-1	FREEV 34
CALL PSI(X,Y,GAMMA,NDIM,1,KMINUS1,IA,1,SUM,SUM1,TT)	FREEV 35
PSIK1X=PSIK1X+SUM	FREEV 36
PSIK1Y=PSIK1Y+SUM1	FREEV 37
IF(KRT.EQ.0) GO TO 23	FREEV 38
CALL PSI(XRT,YRT,GMRT,NDIM,1,KRT,IA,4,SUM,SUM1,TRT)	FREEV 39
PSIK1X=PSIK1X+SUM	FREEV 40
PSIK1Y=PSIK1Y+SUM1	FREEV 41
23 IF(KB.LE.1) RETURN	FREEV 42
KMINUS1=KB-1	FREEV 43
CALL PSI(XB,YB,GMAB,NDIM,1,KMINUS1,IA,2,SUM,SUM1,TB)	FREEV 44
PSIK1X=PSIK1X+SUM	FREEV 45
PSIK1Y=PSIK1Y+SUM1	FREEV 46
IF(KRB.EQ.0) GO TO 51	FREEV 47
CALL PSI(XRB,YRB,GMRB,NDIM,1,KRB,IA,5,SUM,SUM1,TRB)	FREEV 48
PSIK1X=PSIK1X+SUM	FREEV 49
PSIK1Y=PSIK1Y+SUM1	FREEV 50
51 CONTINUE	FREEV 51
RETURN	FREEV 52
3 XX=AK*COS(THETA)	FREEV 53
YY=AK*SIN(THETA)	FREEV 54
C ..... DERIVATIVE OF PSI W.R.T. R ON SURFACE	FREEV 55
IF(KT.LE.1) GO TO 34	FREEV 56
KMINUS1=KT-1	FREEV 57
CALL PSIONE(X,Y,GAMMA,NDIM,1,KMINUS1,IA,1B,SUM,SUM1,TT)	FREEV 58

PSIK1R=PSIK1R+SUM	FREEV 59
IF(KRT.EQ.0) GO TO 34	FREEV 60
CALL PSIONE(XRT,YRT,GMRT,NDIM,1,KRT,IA,IB,SUM,SUM1,TRT)	FREEV 61
PSIK1R=PSIK1R+SUM	FREEV 62
34 IF(KB.LE.1) RETURN	FREEV 63
KMINUS1=KB-1	FREEV 64
CALL PSIONE(XB,YB,GMAB,NDIM,1,KMINUS1,IA,IB,SUM,SUM1,TB)	FREEV 65
PSIK1R=PSIK1R+SUM	FREEV 66
IF(KRB.EQ.0) GO TO 39	FREEV 67
CALL PSIONE(XRB,YRB,GMRB,NDIM,1,KRB,IA,IB,SUM,SUM1,TRB)	FREEV 68
PSIK1R=PSIK1R+SUM	FREEV 69
39 CONTINUE	FREEV 70
RETURN	FREEV 71
END	FREEV 72



SUBROUTINE NONDIM(DMAX,RW,AW,F,S,L,PI)	NONDIM 1
DIMENSION RZ(20)	NONDIM 2
REAL L	NONDIM 3
IEND=20	NONDIM 4
DZSTAR=L/IEND	NONDIM 5
WRITE(6,51)L	NONDIM 6
51 FORMAT(17//30X*BODY GEOMETRY(DIMENSIONAL LENGTH=*F7.3,*)*7/35X,	NONDIM 7
1*ZSTAR*11X*RZERO(ZSTAR)*)	NONDIM 8
ZSTAR=0.0	NONDIM 9
DO 1 I=1,IEND	NONDI 10
RZ(I)=RZERO(ZSTAR)	NONDI 11
WRITE(6,50)ZSTAR,RZ(I)	NONDI 12
50 FORMAT(35XF7.4,13XF7.4)	NONDI 13
1 ZSTAR=ZSTAR+DZSTAR	NONDI 14
C ..... SEARCH FOR MAX DIAMETER	NONDI 15
DMAX=0.0	NONDI 16
DO 2 I=2,IEND	NONDI 17
DMAXN=AMAX1(RZ(I-1),RZ(I))	NONDI 18
IF(DMAXN.LE.DMAX) GO TO 2	NONDI 19
DMAX=DMAXN	NONDI 20
2 CONTINUE	NONDI 21
DMAX=2.0*DMAX	NONDI 22
RW=DMAX/2.0	NONDI 23
F=L/DMAX	NONDI 24
S=PI*DMAX**2/4.0	NONDI 25
IF((RZERO(L)-.001).GT.0.0) GO TO 4	NONDI 26
AW=0.0	NONDI 27
DO 3 I=1,IEND	NONDI 28
TRAP=DZSTAR/2.0*(RZ(I)+RZ(I+1))	NONDI 29
3 AW=AW+TRAP	NONDI 30
AW=(1.0/L)*AW	NONDI 31
GO TO 5	NONDI 32
4 AW=DMAX/2.0	NONDI 33
5 CONTINUE	NONDI 34
RETURN	NONDI 35
END	NONDI 36

FUNCTION PORAG(THETA)	PORAG	1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RMAXSQ,SIGMA,LEVEL	PORAG	2
COMMON/BLOCK7/PHIVT,PHIPT,P1,P2,P3,P4	PORAG	3
DEG=THETA*180.0/PI	PORAG	4
CPK=CPC(THETA)	PORAG	5
PORAG=CPK*COS(THETA)	PORAG	6
WRITE(6,50) DEG,PHIVT,PHIPT,P1,P2,CPK,PORAG,P4	PORAG	7
50 FORMAT(1X,F7.2,7(1X,F12.6))	PORAG	8
RETURN	PORAG	9
ENTRY PLIFT	PORAG	10
CPK=CPC(THETA)	PORAG	11
PLIFT=CPK*SIN(THETA)	PORAG	12
RETURN	PORAG	13
END	PORAG	14

SUBROUTINE POTFLOW(PSIKXP,PSIKYP,PSIKRP,IA)	POTFLO 1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,KC,RCNAXSQ,SIGMA,LEVEL	POTFLO 2
COMMON/BLOCK1/X(100),Y(100),X3(100),YB(100),XRT(100),YRT(100),	POTFLO 3
1 XRB(100),YRB(100)	POTFLO 4
COMMON/BLOCK2/GAMMA(100),GMAB(100),GMRT(100),GMRB(100)	POTFLO 5
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDST	POTFLO 6
COMMON/BLOCK10/THETAS,THETASB,THETA	POTFLO 7
COMMON/BLOCK20/DX,DZ,INTX1,NBIG1	POTFLO 8
INTEGER ALPHA,A	POTFLO 9
REAL L,LB	POTFL 10
GO TO(1,2,3,4,5) IA	POTFL 11
1 L=X(ALPHA)**2+Y(ALPHA)**2	POTFL 12
PSIKXP=2.0*X(ALPHA)*Y(ALPHA)/L**2	POTFL 13
PSIKXP=AKSQD*PSIKXP	POTFL 14
PSIKYP=1.0+AKSQD*(Y(ALPHA)**2-X(ALPHA)**2)/L**2	POTFL 15
RETURN	POTFL 16
2 LB=XB(ALPHA)**2+YB(ALPHA)**2	POTFL 17
PSIKXP=2.0*XB(ALPHA)*YB(ALPHA)/LB**2	POTFL 18
PSIKXP=AKSQD*PSIKXP	POTFL 19
PSIKYP=1.0+AKSQD*(YB(ALPHA)**2-XB(ALPHA)**2)/LB**2	POTFL 20
RETURN	POTFL 21
3 PSIKRP=2.0*SIN(THETA)	POTFL 22
RETURN	POTFL 23
4 L=XRT(ALPHA)**2+YRT(ALPHA)**2	POTFL 24
IF(L.EQ.0.0) RETURN	POTFL 25
PSIKXP=2.0*XRT(ALPHA)*YRT(ALPHA)/L**2	POTFL 26
PSIKXP=AKSQD*PSIKXP	POTFL 27
PSIKYP=1.0+AKSQD*(YRT(ALPHA)**2-XRT(ALPHA)**2)/L**2	POTFL 28
RETURN	POTFL 29
5 LB=XRB(ALPHA)**2+YRB(ALPHA)**2	POTFL 30
IF(LB.EQ.0.0) RETURN	POTFL 31
PSIKXP=2.0*XRB(ALPHA)*YRB(ALPHA)/LB**2	POTFL 32
PSIKXP=AKSQD*PSIKXP	POTFL 33
PSIKYP=1.0+AKSQD*(YRB(ALPHA)**2-XRB(ALPHA)**2)/LB**2	POTFL 34
RETURN	POTFL 35
END	POTFL 36

SUBROUTINE PSI(X,Y,GMA,NDIM,KI,KF,IA,IB,SUM,SUM1,TK)	PSI	1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RCHXSQ,SIGMA,LEVEL	PSI	2
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDST	PSI	3
COMMON/BLOCK30/T,TT,DELT,DELTT,DELTB	PSI	4
COMMON/VTX1/XX,YY	PSI	5
DIMENSION X(NDIM),Y(NDIM),GMA(NDIM),TK(NDIM)	PSI	6
REAL L	PSI	7
INTEGER ALPHA,A	PSI	8
SUM=SUM1=0.0	PSI	9
DO 1 A=KI,KF	PSI	10
IF(ALPHA.EQ.A.AND.IA.EQ.IB) GO TO 1	PSI	11
IFLAG=0	PSI	12
L=X(A)**2+Y(A)**2	PSI	13
R1=(XX-X(A))**2+(YY-Y(A))**2	PSI	14
R2=(XX-X(A)*AKSQD/L)**2+(YY-Y(A)*AKSQD/L)**2	PSI	15
ARE=XX**2+YY**2	PSI	16
IF(R1.GT.RCHXSQ) GO TO 2	PSI	17
RCSQ=5.04*(T-TK(A))/RE	PSI	18
IF(R1.GT.RCSQ) GO TO 2	PSI	19
C ..... POTENTIAL VORTEX APPROX INVALID	PSI	20
IFLAG=1	PSI	21
GMRSET=GMA(A)	PSI	22
GMA(A)=0.0	PSI	23
2 CONTINUE	PSI	24
SUM=SUM+(GMA(A)/PI2)*((XX-X(A))/R1+XX/ARE-(XX-X(A)*AKSQD/L)/R2)	PSI	25
SUM1=SUM1+(GMA(A)/PI2)*((YY-Y(A))/R1+YY/ARE-(YY-Y(A)*AKSQD/L)/R2)	PSI	26
IF(IFLAG.EQ.1) GMA(A)=GMRSET	PSI	27
1 CONTINUE	PSI	28
RETURN	PSI	29
ENTRY PSIONE	PSI	30
SUM=0.0	PSI	31
DO 3 A=KI,KF	PSI	32
IF(X(A).EQ.0.0.AND.Y(A).EQ.0.0) GO TO 3	PSI	33
IFLAG=0	PSI	34
L=X(A)**2+Y(A)**2	PSI	35
R1=(XX-X(A))**2+(YY-Y(A))**2	PSI	36
RCSQ=RC*RC	PSI	37
IF(R1.GE.RCSQ) GO TO 4	PSI	38
C ..... POTENTIAL VORTEX APPROX INVALID	PSI	39
IFLAG=1	PSI	40
GMRSET=GMA(A)	PSI	41
GMA(A)=0.0	PSI	42
4 CONTINUE	PSI	43
SUM=SUM+(GMA(A)/(PI2*AK))*((AKSQD-L)/R1+1.0)	PSI	44
IF(IFLAG.EQ.1) GMA(A)=GMRSET	PSI	45
3 CONTINUE	PSI	46
RETURN	PSI	47
END	PSI	48

SUBROUTINE PV(X,Y,XDT,YDT,GMA,NDIM,KI,KF,SUM,TK)	PV	1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DOR,RTOD,RC,RMAXSQ,SIGMA,LEVEL	PV	2
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	PV	3
COMMON/PRSURE/XX,YY,SINE,COSINE	PV	4
COMMON/BLOCK30/T,TI,DELT,DELTT,DELTB	PV	5
DIMENSION X(NDIM),Y(NDIM),XDT(NDIM),YDT(NDIM),GMA(NDIM)	PV	6
DIMENSION TK(NDIM)	PV	7
REAL L	PV	8
INTEGER A	PV	9
SUM=0.0	PV	10
DO 1 A=KI,KF	PV	11
L=X(A)**2+Y(A)**2	PV	12
IFLAG=0	PV	13
CAPA=(X(A)*COSINE+Y(A)*SINE)	PV	14
R1=AKSQD+L-2.0*AK*CAPA	PV	15
R2=(AKSQD*L+AKSQD**2-2.0*AK**3*CAPA)/L	PV	16
RCSQ=RC*RC	PV	17
IF(R1.GE.RCSQ) GO TO 34	PV	18
SQR1=SQRT(R1)	PV	19
WRITE(6,50)A,SQR1	PV	20
50 FORMAT(* POTENTIAL VORTEX APPROX INVALID ALPHA=*I3,5X,	PV	21
1*CORE RADIUS=*F12.6)	PV	22
C ..... POTENTIAL VORTEX APPROX INVALID	PV	23
IFLAG=1	PV	24
GMRSET=GMA(A)	PV	25
GMA(A)=0.0	PV	26
34 CONTINUE	PV	27
CAPX=(AKSQD*XDT(A)+2.0*AK*X(A)*AKDOT)/L	PV	28
1-(2.0*AKSQD*X(A)/L**2)*(X(A)*XDT(A)+Y(A)*YDT(A))	PV	29
CAPY=(AKSQD*YDT(A)+2.0*AK*Y(A)*AKDOT)/L	PV	30
1-(2.0*AKSQD*Y(A)/L**2)*(X(A)*XDT(A)+Y(A)*YDT(A))	PV	31
SUM=SUM+(GMA(A)/PI2)*((YDT(A)*(XX-X(A))-XDT(A)*(YY-Y(A)))/R1	PV	32
1-(CAPY*(XX-AKSQD*X(A)/L)-CAPX*(YY-AKSQD*Y(A)/L))/R2)	PV	33
IF(IFLAG.EQ.1) GMA(A)=GMRSET	PV	34
1 CONTINUE	PV	35
RETURN	PV	36
END	PV	37

SUBROUTINE RITE(MT, IDIM, JDIM, U, ZN, NX, S, DEG, ZHAT, DELS, K)	RITE	1
DIMENSION U(IDIM, 2, JDIM)	RITE	2
DIMENSION FOR601(4), FOR560(3), FOR561(3), FOR580(2)	RITE	3
DIMENSION NX(53), DEG(53)	RITE	4
DIMENSION S(53), ZN(53)	RITE	5
COMMON/BLOCK20/DX, DZ, INTX1, NBIG1	RITE	6
COMMON/BLOCK30/T, TI, DELT, DELTT, DELTB	RITE	7
COMMON/BLOCK5/AK, AKSQD, AKHALF, AKDOT	RITE	8
COMMON/BLOCK2/TAU, PT4, NBIG	RITE	9
MT=INTX1/12	RITE	10
I=1	RITE	11
M=1	RITE	12
IF(MT.EQ.0) GO TO 35	RITE	13
MM=12	RITE	14
IF(MT.EQ.1) WRITE(6, 549) TI	RITE	15
IF(MT.EQ.2) WRITE(6, 550) K, T, ZHAT, AK, AKDOT	RITE	16
WRITE(6, 600) (NX(I), I=1, 12)	RITE	17
GO TO 32	RITE	18
31 WRITE(6, 601) (NX(I), I=M, MM)	RITE	19
32 WRITE(6, 560) (S(I), I=M, MM)	RITE	20
WRITE(6, 561) (DEG(I), I=M, MM)	RITE	21
WRITE(6, 580) (ZN(J), (U(I, MT, J), I=M, MM), J=1, NBIG)	RITE	22
I=I+1	RITE	23
M=MM+1	RITE	24
MM=M+11	RITE	25
IF(I.LE.MI) GO TO 31	RITE	26
IF(M-1.EQ.INTX1) GO TO 33	RITE	27
35 MM=INTX1	RITE	28
N=(MM-M)+1	RITE	29
NN=N+1	RITE	30
ENCODE(33, 1000, FOR601) N	RITE	31
ENCODE(29, 1004, FOR560) N	RITE	32
ENCODE(30, 1005, FOR561) N	RITE	33
ENCODE(16, 1002, FOR580) NN	RITE	34
IF(MT.EQ.0) WRITE(6, 550) K, T, ZHAT, DELT, DELS, DZ	RITE	35
WRITE(6, FOR601) (NX(I), I=M, MM)	RITE	36
WRITE(6, FOR560) (S(I), I=M, MM)	RITE	37
WRITE(6, FOR561) (DEG(I), I=M, MM)	RITE	38
WRITE(6, FOR580) (ZN(J), (U(I, MT, J), I=M, MM), J=1, NBIG)	RITE	39
33 CONTINUE	RITE	40
RETURN	RITE	41
549 FORMAT(1H1, 40X*BOUNDARY LAYER VELOCITY DISTRIBUTION ( UI ) TI=*	RITE	42
1F5.3, /)	RITE	43
550 FORMAT(1H1, 50X*BOUNDARY LAYER VELOCITY DISTRIBUTION*/30X* K=*I2, 5XRITE	RITE	44
1*T=*F6.3, 5X*ZHAT=*F6.3, 5X*AK=*F6.3, 5X*AKDOT=*F6.3)	RITE	45
560 FORMAT(* R+ (RAD)*, 1X, 12(F9.5, 1X))	RITE	46
561 FORMAT(* (DEG)*, 1X, 12(F9.5, 1X)/)	RITE	47
580 FORMAT(1X, 13(F9.5, 1X))	RITE	48
600 FORMAT(/* NCYCLE *, 12(4X, I2, 4X)/)	RITE	49
601 FORMAT(/// * NCYCLE *, 12(4X, I2, 4X)/)	RITE	50
1000 FORMAT(18H(/// * NCYCLE *, I2, 13H(4X, I2, 4X)/))	RITE	51
1002 FORMAT(4H(1X, I2, 10H(F9.5, 1X)))	RITE	52
1004 FORMAT(17H(* R+ (RAD)*, 1X, I2, 10H(F9.5, 1X)))	RITE	53
1005 FORMAT(17H(* (DEG)*, 1X, I2, 11H(F9.5, 1X)/)	RITE	54
END	RITE	55

SUBROUTINE RSEP(THTASF,THTASR,THTA,UBL,INTX1,INITAL,MODE)	RSEP	1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RMAXSQ,SIGMA,LEVEL	RSEP	2
DIMENSION THTA(53),UBL(53)	RSEP	3
UFMX=0.0	RSEP	4
C ..... SEARCH B.L. FOR MAX VELOCITY	RSEP	5
DO 1 I=2,INTX1	RSEP	6
UFMXN=AMAX1(UBL(I-1),UBL(I))	RSEP	7
IF(UFMXN.LE.UFMX) GO TO 1	RSEP	8
IMAX=I-1	RSEP	9
IF(UFMXN.GT.UBL(I-1)) IMAX=I	RSEP	10
UFMX=UFMXN	RSEP	11
1 CONTINUE	RSEP	12
THTAMXF=THTA(IMAX)	RSEP	13
URMX=0.0	RSEP	14
C ..... SEARCH S.L. FOR MAX BACKFLOW VELOCITY	RSEP	15
ISLS=INTX1+2	RSEP	16
DO 2 I=ISLS,INITAL	RSEP	17
URMXN=AMIN1(UBL(I-1),UBL(I))	RSEP	18
IF(URMXN.GE.URMX) GO TO 2	RSEP	19
JMAX=I-1	RSEP	20
IF(URMXN.LT.UBL(I-1)) JMAX=I	RSEP	21
URMX=URMXN	RSEP	22
2 CONTINUE	RSEP	23
THTAMXR=THTA(JMAX)	RSEP	24
C ..... SEARCH S.L. FOR ZERO VELOCITY	RSEP	25
ISLE=INITAL-1	RSEP	26
DO 4 I=ISLS,ISLE	RSEP	27
UZN=AMIN1(ABS(UBL(I-1)),ABS(UBL(I)))	RSEP	28
IF(I.EQ.ISLS) GO TO 3	RSEP	29
IF(UZN.GE.UZ) GO TO 4	RSEP	30
3 KMAX=I-1	RSEP	31
IF(UZN.LT.ABS(UBL(I-1))) KMAX=I	RSEP	32
UZ=UZN	RSEP	33
4 CONTINUE	RSEP	34
THTAZRO=THTA(KMAX)	RSEP	35
C ..... CALCULATE S.L. SEPARATION POINT	RSEP	36
X=(THTAZRO-THTAMXF)/(THTASF-THTAMXF)	RSEP	37
THTASR=THTAMXR-((THTAMXR-THTAZRO)/X)	RSEP	38
THTAMXF=THTAMXF*RTOD	RSEP	39
THTAMXR=THTAMXR*RTOD	RSEP	40
THTAZRO=THTAZRO*RTOD	RSEP	41
THTASRD=THTASR*RTOD	RSEP	42
WRITE(6,50)UFMX,THTAMXF,URMX,THTAMXR,UZ,THTAZRO,THTASRD	RSEP	43
50 FORMAT(1H1,* MAX VELOCITY=*F6.3,* AT THETA=*F5.1,* DEGREES*/	RSEP	44
1* MAX BACKFLOW VEL=*F6.3,* AT THETA=*F5.1,* DEGREES*/	RSEP	45
2* MIN TANGENTIAL VELOCITY BETWEEN MAX VELOCITY AND MAX BACKFLOW VERSEP	RSEP	46
3LOCITY=*F6.3,* AT THETA=*F5.1,* DEGREES*/	RSEP	47
4F5.3,* DEGREES*)	RSEP	48
RETURN	RSEP	49
END	RSEP	50

SUBROUTINE RVTX(X,Y,GMA,THTASR,THTASM,THTAS,UZZ,UZZSQ,GAMA,	RVTX	1
1MODE,KRN,N,NF,IFLAG,GMATL,NDIM,TK)	RVTX	2
DIMENSION X(NDIM),Y(NDIM),GMA(NDIM),TK(NDIM)	RVTX	3
DIMENSION THTAS(6),UZZ(6),UZZSQ(6),GAMA(6),IFLAG(6)	RVTX	4
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RMAXSQ,SIGMA,LEVEL	RVTX	5
COMMON/KAYS/K,KS,KR,KT,KB,KRT,KRB	RVTX	6
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	RVTX	7
COMMON/BLOCK10/THTAS,THTASB,THETA	RVTX	8
COMMON/BLOCK30/T,TI,DELT,DELTT,DELTB	RVTX	9
IF(K.NE.KR) GO TO 1	RVTX	10
NF=5	RVTX	11
N=N	RVTX	12
GMATL=0.	RVTX	13
1 N=N+1	RVTX	14
THTAS(N)=THTASR	RVTX	15
THETA=THTAS(N)	RVTX	16
CALL FREEVTX(PSIK1X,PSIK1Y,PSIK1R,3)	RVTX	17
CALL POTFLOW(PSIKXP,PSIKYP,PSIKRP,3)	RVTX	18
UZZ(N)=PSIK1R+PSIKRF	RVTX	19
THTAP=THTAS(N)*RTOD	RVTX	20
WRITE(6,600)N,THTAP,UZZ(N)	RVTX	21
600 FORMAT(77* RVTX SUBROUTINE N=*I3,2X*THETAS(N)=*F12.6,	RVTX	22
12X*UZZ(N)=*F12.6)	RVTX	23
UZZ(N)=ABS(UZZ(N))	RVTX	24
UZZSQ(N)=UZZ(N)*UZZ(N)	RVTX	25
GAMA(N)=-DELT*UZZSQ(N)/2.0	RVTX	26
IF(MODE.EQ.2)GAMA(N)=-GAMA(N)	RVTX	27
WRITE(6,601)GAMA(N)	RVTX	28
601 FORMAT(* GAMA(N)=*F12.6)	RVTX	29
IF(N.EQ.NF+1) GO TO 10	RVTX	30
IFLAG(N-1)=0	RVTX	31
IF(THTAS(N)-THTAS(N-1))3,4,2	RVTX	32
2 IF(MODE.EQ.1) IFLAG(N-1)=1	RVTX	33
GO TO 5	RVTX	34
3 IF(MODE.EQ.2) IFLAG(N-1)=1	RVTX	35
GO TO 5	RVTX	36
4 IFLAG(N-1)=1	RVTX	37
5 CONTINUE	RVTX	38
IF(IFLAG(N-1).EQ.1)GMATL=GMATL+GAMA(N-1)	RVTX	39
WRITE(6,602)GMATL,N,IFLAG(N-1)	RVTX	40
602 FORMAT(/* GAMA CHECK SUM=*F12.6,5X*N=*I3,5X*IFLAG(N-1)=*I3)	RVTX	41
AGMATL=ABS(GMATL)	RVTX	42
IF(AGMATL.LE..1) GO TO 6	RVTX	43
IF(GMATL.LE..1) GO TO 6	RVTX	44
NF=N	RVTX	45
GO TO 7	RVTX	46
6 IF(N.LT.5) RETURN	RVTX	47
7 THTASM=THTAS(N)	RVTX	48
GMATL=0.	RVTX	49
RETURN	RVTX	50
10 IF(K.EQ.KR) GO TO 2000	RVTX	51
IFLAG(NF)=0	RVTX	52
IF(THTAS(N)-THTASM)30,40,20	RVTX	53
20 IF(MODE.EQ.1) IFLAG(NF)=1	RVTX	54
GO TO 50	RVTX	55
30 IF(MODE.EQ.2) IFLAG(NF)=1	RVTX	56
GO TO 50	RVTX	57
40 IFLAG(NF)=1	RVTX	58



50	CONTINUE	RVTX	59
	THTAP=THTAS(N)*RTOD	RVTX	60
	THTAPM=THTASM*RTOD	RVTX	61
	WRITE(6,603)N,NF,IFLAG(NF),THTAP,THTAPM	RVTX	62
603	FORMAT(/* OVERLAP CHECK N=*I3,5X*NF=*I3,5X*IFLAG(NF)=*I3,	RVTX	63
	15X*THTAS(N)=*F12.6,5X*THTASM=*F12.6)	RVTX	64
	U00=0.0	RVTX	65
	U00SQ=0.0	RVTX	66
	GAM=0.	RVTX	67
	THTASR=0.	RVTX	68
	RN=0.	RVTX	69
	N=1	RVTX	70
100	IF(IFLAG(N).EQ.0) GO TO 200	RVTX	71
	RN=RN+1.0	RVTX	72
	U00=U00+UZZ(N)	RVTX	73
	U00SQ=U00SQ+UZZSQ(N)	RVTX	74
	GAM=GAM+GAMA(N)	RVTX	75
	THTASR=THTASR+THTAS(N)	RVTX	76
	WRITE(6,604)N,U00,U00SQ,GAM,THTASR	RVTX	77
604	FORMAT(/* LUMP SUMS N=*I3,2X*U00=*F12.6,2X*U00SQ=*F12.6,	RVTX	78
	12X*GAM=*F12.6,2X*THTASR=*F12.6)	RVTX	79
200	IF(N.EQ.NF) GO TO 1000	RVTX	80
	N=N+1	RVTX	81
	GO TO 100	RVTX	82
1000	CONTINUE	RVTX	83
	SMALLM=(RN*DELT/PI2)*(U00SQ/U00)	RVTX	84
	THTASR=THTASR/RN	RVTX	85
	KRN=KRN+1	RVTX	86
	X(KRN)=(AK+SMALLM)*COS(THTASR)	RVTX	87
	Y(KRN)=(AK+SMALLM)*SIN(THTASR)	RVTX	88
	GMA(KRN)=GAM	RVTX	89
	GMA(KRN)=SIGMA*GMA(KRN)	RVTX	90
	THTAP=THTASR*RTOD	RVTX	91
	TK(KRN)=T	RVTX	92
	WRITE(6,605)SMALLM,THTAP,KRN,X(KRN),Y(KRN),GMA(KRN)	RVTX	93
605	FORMAT(//* RVTX BIRTH SMALLM=*F12.6,5X*THTASR(AVERAGE)=*F12.6,/	RVTX	94
	15X*KRN=*I3,2X*X(KRN)=*F12.6,2X*Y(KRN)=*F12.6,2X*GMA(KRN)=*F12.6)	RVTX	95
2000	UZZ(1)=UZZ(NF+1)	RVTX	96
	UZZSQ(1)=UZZSQ(NF+1)	RVTX	97
	GAMA(1)=GAMA(NF+1)	RVTX	98
	THTAS(1)=THTAS(NF+1)	RVTX	99
	N=1	RVTX	100
	NF=5	RVTX	101
	RETURN	RVTX	102
	END	RVTX	103

```

FUNCTION RZRO(ZHAT,L,RW)
REAL L
RZRO=RZERO(ZHAT*L)/RW
RETURN
ENTRY DRZRO
RZRO=(L/RW)*DRZERO(ZHAT*L)
RETURN
END

```

RZRO	1
RZRO	2
RZRO	3
RZRO	4
RZRO	5
RZRO	6
RZRO	7
RZRO	8

FUNCTION UAPRX1(L,N,IDIM,JDIM,U)

DIMENSION U(IDIM,2,JDIM)

\*\*\* \*\*\*\*\*FIRST APPROXIMATION TO U(L+1,2,N)

UAPRX1=U(L+1,1,N)+U(L,2,N)-U(L,1,N)

RETURN

ENTRY US

US=(U(L+1,1,N)+U(L,2,N)+U(L,1,N))/4.0

RETURN

ENTRY UL

UL=U(L+1,1,N)-U(L,2,N)-U(L,1,N)

RETURN

ENTRY UM

UM=U(L,2,N)-U(L+1,1,N)-U(L,1,N)

RETURN

END

UAPRX1 1

UAPRX1 2

UAPRX1 3

UAPRX1 4

UAPRX1 5

UAPRX1 6

UAPRX1 7

UAPRX1 8

UAPRX1 9

UAPRX 10

UAPRX 11

UAPRX 12

UAPRX 13

UAPRX 14

UAPRX 15

SUBROUTINE VEL(X,Y,XDT,YDT,NDIM,KI,KF,IA)	VEL	1
COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RCHXSQ,SIGMA,LEVEL	VEL	2
COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	VEL	3
DIMENSION X(NDIM),Y(NDIM),XDT(NDIM),YDT(NDIM)	VEL	4
INTEGER ALPHA	VEL	5
REAL L	VEL	6
DO 1 ALPHA=KI,KF	VEL	7
L=X(ALPHA)**2+Y(ALPHA)**2	VEL	8
CALL FREEVTX(PSIK1X,PSIK1Y,PSIK1R,IA)	VEL	9
CALL POTFLOW(PSIKXP,PSIKYP,PSIKRP,IA)	VEL	10
PSIKX=PSIKXP+PSIK1X+AK*AKDOT*Y(ALPHA)/L	VEL	11
PSIKY=PSIKYP+PSIK1Y-AK*AKDOT*X(ALPHA)/L	VEL	12
XDT(ALPHA)=-PSIKY	VEL	13
YDT(ALPHA)=PSIKX	VEL	14
1 CONTINUE	VEL	15
RETURN	VEL	16
END	VEL	17

SUBROUTINE	VM(X,Y,XDT,YDT,NDIM,KI,KF,DT)	VM	1
COMMON	ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RCHXSQ,SIGMA,LEVEL	VM	2
COMMON	/BLOCK5/AK,AKSQD,AKHALF,AKDOT	VM	3
DIMENSION	X(NDIM),Y(NDIM),XDT(NDIM),YDT(NDIM)	VM	4
INTEGER	ALPHA	VM	5
DO 1	ALPHA=KI,KF	VM	6
XTEMP	=X(ALPHA)	VM	7
YTEMP	=Y(ALPHA)	VM	8
X(ALPHA)	=X(ALPHA)+DT*XDT(ALPHA)	VM	9
Y(ALPHA)	=Y(ALPHA)+DT*YDT(ALPHA)	VM	10
R	=SQRT(X(ALPHA)**2+Y(ALPHA)**2)	VM	11
IF(R.GT.AK)	GO TO 1	VM	12
WRITE(6,600)	X(ALPHA),Y(ALPHA)	VM	13
CALL	VMFIX(XTEMP,YTEMP,XDT(ALPHA),YDT(ALPHA))	VM	14
X(ALPHA)	=XTEMP+DT*XDT(ALPHA)	VM	15
Y(ALPHA)	=YTEMP+DT*YDT(ALPHA)	VM	16
WRITE(6,601)	X(ALPHA),Y(ALPHA)	VM	17
1	CONTINUE	VM	18
600	FORMAT(// * BEFORE VMFIX(X(ALPHA),Y(ALPHA))=(*F8.5,*,*F8.5,*)*)	VM	19
601	FORMAT(// * AFTER VMFIX(X(ALPHA),Y(ALPHA))=(*F8.5,*,*F8.5,*)*)	VM	20
	RETURN	VM	21
	END	VM	22

	SUBROUTINE VMFIX(X,Y,XDOT,YDOT)	VMFIX	1
	COMMON ALPHA,PI,PI2,RE,SRE,SQRTPI,DTOR,RTOD,RC,RCMAXSO,SIGMA,LEVEL	VMFIX	2
	COMMON/BLOCK5/AK,AKSQD,AKHALF,AKDOT	VMFIX	3
	COMMON/BLOCK10/THETAS,THETASB,THETA	VMFIX	4
	DEF=.001	VMFIX	5
	IF(X.NE.0) GO TO 10	VMFIX	6
	L=1	VMFIX	7
	ANGLE=PI/2.0	VMFIX	8
	IF(Y.LT.0)L=2	VMFIX	9
	IF(Y.LT.0) ANGLE=(3.0/2.0)*PI	VMFIX	10
	GO TO 30	VMFIX	11
10	IF(Y.NE.0) GO TO 20	VMFIX	12
	L=1	VMFIX	13
	ANGLE=0.0	VMFIX	14
	IF(X.LT.0)L=2	VMFIX	15
	IF(X.LT.0) ANGLE=PI	VMFIX	16
	GO TO 30	VMFIX	17
20	IF(X.GT.0.0.AND.Y.GT.0.0)L=1	VMFIX	18
	IF(X.LT.0.0.AND.Y.GT.0.0)L=2	VMFIX	19
	IF(X.LT.0.0.AND.Y.LT.0.0)L=3	VMFIX	20
	IF(X.GT.0.0.AND.Y.LT.0.0)L=4	VMFIX	21
	ANGLE=ATAN(Y/X)	VMFIX	22
30	CONTINUE	VMFIX	23
	SINE=SIN(ANGLE)	VMFIX	24
	COSINE=COS(ANGLE)	VMFIX	25
	GO TO(1,2,3,4),L	VMFIX	26
1	X=(AK+DEF)*COSINE	VMFIX	27
	Y=(AK+DEF)*SINE	VMFIX	28
	XDOT=XDOT+SINE	VMFIX	29
	YDOT=YDOT+COSINE	VMFIX	30
	U=-XDOT+YDOT	VMFIX	31
	XDOT=-U*SINE	VMFIX	32
	YDOT=U*COSINE	VMFIX	33
	GO TO 5	VMFIX	34
2	X=- (AK+DEF)*COSINE	VMFIX	35
	Y=- (AK+DEF)*SINE	VMFIX	36
	XDOT=-XDOT*SINE	VMFIX	37
	YDOT=YDOT+COSINE	VMFIX	38
	U=-XDOT-YDOT	VMFIX	39
	XDOT=U*SINE	VMFIX	40
	YDOT=-U*COSINE	VMFIX	41
	GO TO 5	VMFIX	42
3	X=- (AK+DEF)*COSINE	VMFIX	43
	Y=- (AK+DEF)*SINE	VMFIX	44
	XDOT=XDOT*SINE	VMFIX	45
	YDOT=YDOT+COSINE	VMFIX	46
	U=XDOT-YDOT	VMFIX	47
	XDOT=U*SINE	VMFIX	48
	YDOT=-U*COSINE	VMFIX	49
	GO TO 5	VMFIX	50
4	X=(AK+DEF)*COSINE	VMFIX	51
	Y=(AK+DEF)*SINE	VMFIX	52
	XDOT=-XDOT*SINE	VMFIX	53
	YDOT=YDOT+COSINE	VMFIX	54
	U=XDOT+YDOT	VMFIX	55
	XDOT=-U*SINE	VMFIX	56
	YDOT=U*COSINE	VMFIX	57
	GO TO 5	VMFIX	58

```

5  CONTINUE
   RTOD=180.0/PI
   ADEG=ANGLE*RTOD
WRITE(6,50)ALPHA,ADEG,X,Y,XDOT,YDOT
50  FORMAT(//* VMFIX*2X*ALPHA=*I3,2X*ANGLE=*F12.6,/* X=*F12.6,
12X*Y=*F12.6,2X*XDOT=*F12.6,2X*YDOT=*F12.6)
   RETURN
   END

```

```

VMFIX 59
VMFIX 60
VMFIX 61
VMFIX 62
VMFIX 63
VMFIX 64
VMFIX 65
VMFIX 66

```

SUBROUTINE WRIT(X,Y,XDOT,YDOT,GAMMA,XB,YB,XDOTB,YDOTB,GMAB,	WRIT	1
1KIT,KFT,KIB,KFB,K,NDIM,IW)	WRIT	2
DIMENSION X(NDIM),Y(NDIM),XDOT(NDIM),YDOT(NDIM),GAMMA(NDIM),	WRIT	3
1XB(NDIM),YB(NDIM),XDOTB(NDIM),YDOTB(NDIM),GMAB(NDIM)	WRIT	4
IF(KFT-KFB) 1,2,2	WRIT	5
1 KF=KFB	WRIT	6
GO TO 3	WRIT	7
2 KF=KFT	WRIT	8
3 CONTINUE	WRIT	9
IF(KIT.GT.KIB) GO TO 17	WRIT	10
DO 16 I=KIT,KF	WRIT	11
IF(I.GE.KSB) GO TO 12	WRIT	12
11 WRITE(6,601) I,K,X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I)	WRIT	13
IF(IW.NE.7.AND.IW.NE.9) GO TO 16	WRIT	14
WRITE(IW,701) I,K,X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I)	WRIT	15
GO TO 16	WRIT	16
12 IF(KFT.NE.KFB) GO TO 14	WRIT	17
13 WRITE(6,603) I,K,X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I),	WRIT	18
1XB(I),YB(I),XDOTB(I),YDOTB(I),GMAB(I)	WRIT	19
IF(IW.NE.7.AND.IW.NE.9) GO TO 16	WRIT	20
WRITE(IW,703) I,K,X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I),XB(I),YB(I),	WRIT	21
1XDOTB(I),YDOTB(I),GMAB(I)	WRIT	22
GO TO 16	WRIT	23
14 IF(KFT.LT.KFB) GO TO 15	WRIT	24
IF(I.LE.KFB) GO TO 13	WRIT	25
GO TO 11	WRIT	26
15 IF(I.LE.KFT) GO TO 13	WRIT	27
16 CONTINUE	WRIT	28
GO TO 20	WRIT	29
17 CONTINUE	WRIT	30
DO 19 I=KIB,KF	WRIT	31
IF(I.GE.KS) GO TO 18	WRIT	32
WRITE(6,602) I,K,XB(I),YB(I),XDOTB(I),YDOTB(I),GMAB(I)	WRIT	33
IF(IW.NE.7.AND.IW.NE.9) GO TO 19	WRIT	34
WRITE(IW,702) I,K,XB(I),YB(I),XDOTB(I),YDOTB(I),GMAB(I)	WRIT	35
GO TO 19	WRIT	36
18 WRITE(6,603) I,K,X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I),	WRIT	37
1XB(I),YB(I),XDOTB(I),YDOTB(I),GMAB(I)	WRIT	38
IF(IW.NE.7.AND.IW.NE.9) GO TO 19	WRIT	39
WRITE(IW,703) I,K,X(I),Y(I),XDOT(I),YDOT(I),GAMMA(I),XB(I),YB(I),	WRIT	40
1XDOTB(I),YDOTB(I),GMAB(I)	WRIT	41
19 CONTINUE	WRIT	42
20 CONTINUE	WRIT	43
601 FORMAT(2X I3,2X I3,5(2X,F10.6))	WRIT	44
602 FORMAT(2X I3,2X I3,60X,5(2X,F10.6))	WRIT	45
603 FORMAT(2X I3,2X I3,10(2X,F10.6))	WRIT	46
701 FORMAT(2 I4,5F7.3)	WRIT	47
702 FORMAT(2 I4,35X,4F7.3)	WRIT	48
703 FORMAT(2 I4,10F7.3)	WRIT	49
RETURN	WRIT	50
END	WRIT	51



PROGRAM ADYNF(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)	ADYNF 1
COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE	ADYNF 2
COMMON/OUTPUT/NEPDR(100),FCTI(100),XIL(28),COEFL(27,4),	ADYNF 3
* VORDL(28,2),KNOT,LMAX,INTERV	ADYNF 4
COMMON/OTHER/LXI,LXI1,LXI2,0,CHANGE,ERROR,ACC,XI(28)	ADYNF 5
DIMENSION INFO(16),X(100),Z(100),PORCD(100),CDN(100)	ADYNF 6
DIMENSION Y(100)	ADYNF 7
REAL L	ADYNF 8
REAL LENGTH,LAMBDA	ADYNF 9
EXTERNAL FIT	ADYNF 10
C ..... INFO ..... DATA IDENTIFICATION	ADYNF 11
READ(5,605)(INFO(I),I=1,16)	ADYNF 12
605 FORMAT(16A5)	ADYNF 13
WRITE(6,651)(INFO(I),I=1,16)	ADYNF 14
651 FORMAT(1H1,20X,16A5 //)	ADYNF 15
READ(5,652)AATAACK,LAMBDA,LENGTH,F,AW,RW	ADYNF 16
652 FORMAT(6F12,6)	ADYNF 17
C ..... READ NO. OF KNOTS, NO. OF POINTS, X CO-ORD, Y CO-ORD	ADYNF 18
READ(5,610)NOKNOT,LX,(X(I),PORCD(I),I=1,LX)	ADYNF 19
610 FORMAT(2I4,/(2F12,8))	ADYNF 20
C ..... IF NOKNOT.GT.0 READ IN KNOT POSITIONS	ADYNF 21
LXI2=1ABS(NOKNOT)	ADYNF 22
IF(NOKNOT.GT.0)READ(5,601)(XI(I),J=1,LXI2)	ADYNF 23
601 FORMAT(6F12,6)	ADYNF 24
C ..... ELLIPSOID PARAMETERS	ADYNF 25
PI=4.0*ATAN(1.0)	ADYNF 26
DTOR=PI/180.0	ADYNF 27
RTOD=180.0/PI	ADYNF 28
AATAACK=AATAACK*DTOR	ADYNF 29
FTA=F*TAN(AATAACK)	ADYNF 30
COEFN=4.0*F/PI	ADYNF 31
COEFM=-4.0*F/PI	ADYNF 32
COEF1=AW/RW*SIN(AATAACK)**2	ADYNF 33
C ..... CALCULATE CDN,ZHAT	ADYNF 34
C ..... GET SPLINE X CO ORD XX(I), Y CO ORD U(I)	ADYNF 35
DO 1 I=1,LX	ADYNF 36
Z(I)=X(I)	ADYNF 37
CDN(I)=COEF1*PORCD(I)	ADYNF 38
U(I)=CDN(I)	ADYNF 39
1 XX(I)=Z(I)	ADYNF 40
CALL SPLINEB(NOKNOT)	ADYNF 41
C ..... TEMPORARY DEBUGGING DATA PLOT Y VS. X	ADYNF 42
WRITE(6,62)	ADYNF 43
DO 3 I=1,21	ADYNF 44
X(I)=.05*(I-1)	ADYNF 45
Y(I)=FIT(X(I))	ADYNF 46
3 WRITE(6,61)X(I),Y(I)	ADYNF 47
61 FORMAT(F12,6,4X,F12,6)	ADYNF 48
62 FORMAT(1H1,6X,Z*13X*CDN(Z)*)	ADYNF 49
CNI=CAURE(FIT,0.0,1.0,.01,.01,3,ERR,IFLAG)	ADYNF 50
CN=COEFN*CNI	ADYNF 51
WRITE(6,60)CN,CNI,ERR,IFLAG	ADYNF 52
60 FORMAT(/////* ..... CN=*F12,6,/* ..... CNI=*F12,6,5X*ERROR=*F12,8,ADYNF 53	
15X*IFLAG=*12)	ADYNF 54
DO 2 I=1,LX	ADYNF 55
CDN(I)=(Z(I)*RZRO(Z(I),LENGTH,RW)*DRZRO(Z(I),LENGTH,RW)/	ADYNF 56
1(4.0*F**2))*CDN(I)	ADYNF 57
XX(I)=Z(I)	ADYNF 58

2	U(I)=CDN(I)	ADYNF	59
	CALL SPLINEB(NOKNOT)	ADYNF	60
C	***** TEMP DEBUG DATA SPLINE Y VS X	ADYNF	61
	WRITE(6,63)	ADYNF	62
	DO 4 I=1,21	ADYNF	63
	X(I)=.05*(I-1)	ADYNF	64
	Y(I)=FIT(X(I))	ADYNF	65
4	WRITE(6,61)X(I),Y(I)	ADYNF	66
63	FORMAT(1H1,6X*2*13X*1,5-2)CDN*)	ADYNF	67
	CMI=CADRE(FIT,0.0,1.0,.01,.01,3,ERR,IFLAG)	ADYNF	68
	CM=COEFM*CMI+LAMBDA*CN	ADYNF	69
	WRITE(6,65)CM,CMI,ERR,IFLAG	ADYNF	70
65	FORMAT(///// * ..... CM=*F12.6,/* ..... CMI=*F12.6,5X*ERROR=*F12.8,ADYNF	ADYNF	71
	15X*IFLAG=*I2)	ADYNF	72
	END	ADYNF	73

	FUNCTION FIT(X)	FIT	1
	COMMON/INPUT/LX,XX(100),U(100),JADD,ADDXI(26),MODE	FIT	2
	COMMON/OUTPUT/UERROR(100),ECIL(100),XIL(28),COEFL(27,4),	FIT	3
	VORDL(28,2),KNOT,LMAX,INTERV	FIT	4
	COMMON/OTHER/LXI,LXI1,LXI2,0,CHANGE,ERROR,ACC,XI(28)	FIT	5
	I=LXI2	FIT	6
1	A=X-XI(I)	FIT	7
	IF(A)2,2,4	FIT	8
7	I=I-1	FIT	9
	IF(I)3,3,1	FIT	10
3	I=1	FIT	11
4	FIT=COEFL(I,1)+A*(COEFL(I,2)+A*(COEFL(I,3)+A*COEFL(I,4)))	FIT	12
	RETURN	FIT	13
	END	FIT	14

APPENDIX IV

SAMPLE CASE

SAMPLE  
FUNCTION RZERO  
(INPUT BODY GEOMETRY)

```

FUNCTION RZERO(ZSTAR)
REAL LN
D=4.7
LN=14.1
R=43.475
IF(ZSTAR.GE.LN) GO TO 1
RZERO=SQRT(R**2-(ZSTAR-LN)**2)-(R-D/2.0)
GO TO 2
1 RZERO=D/2.0
2 CONTINUE
RETURN
ENTRY DRZERO
IF(ZSTAR.GE.LN) GO TO 3
RZERO=(LN-ZSTAR)/SQRT(R**2-(ZSTAR-LN)**2)
GO TO 4
3 RZERO=0.0
4 CONTINUE
RETURN
END

```

```

RZERO 1
RZERO 2
RZERO 3
RZERO 4
RZERO 5
RZERO 6
RZERO 7
RZERO 8
RZERO 9
RZERO 10
RZERO 11
RZERO 12
RZERO 13
RZERO 14
RZERO 15
RZERO 16
RZERO 17
RZERO 18
RZERO 19

```

VCF      SAMPLE      INPUT  
CASE ... OGIVE CYLINDER ... ANGLE OF ATTACK (15 DEG)

	*****	VCF	SAMPLE	OUTPUT	*****
15.0		4725600.0	50.478		
125		.05	.6		
39		90.0	1.0		
3 4 5 5					

CARD 1  
CARD 2  
CARD 3  
CARD 4  
CARD 5

\*\*\*\*\* VCF SAMPLE OUTPUT \*\*\*\*\*

140

BODY GEOMETRY(DIMENSIONAL LENGTH= 50.47A)

ZSTAR	RZERO(ZSTAR)
0.0000	0.0000
-2.5239	.7805
5.0478	1.3972
7.5717	1.8571
-10.0956	-2.1652
12.6195	2.3248
15.1434	2.3500
-17.6673	-2.3500
20.1912	2.3500
22.7151	2.3500
-25.2390	-2.3500
27.7629	2.3500
30.2868	2.3500
-32.8107	-2.3500
35.3346	2.3500
37.8585	2.3500
-40.3824	-2.3500
42.9063	2.3500
45.4302	2.3500
-47.9541	-2.3500

-RMAX=-4.7000  
 AW= 2.3500  
 S=10.7400  
 -S=17.3494

ANGLE-OF-ATTACK= 15.0 DEGREES  
 3DS REYNOLDS NO.= 4725600.00  
 2DLS REYNOLDS NO.= 56940.19

2DLS PARAMETERS

DELT= .125  
 RC=.050  
 SIGMA=.600

PROGRAM CONTRL

KFINAL= 39  
 IFINAL= 90.0  
 ZFINAL=1.000  
 LR= 3  
 LW= 4  
 LEVEL= 5  
 KPLN= 5

K=39 T= 5.048 BOUNDARY LAYER VELOCITY DISTRIBUTION  
ZHAT= 2.686 AK= 1.000 AKDOT= 0.000

NO CYCLE	0	3	3	3	3	3	3	4	4	4	4	4
R+ (RAD)	0.00000	.08727	.17453	.26180	.34907	.43633	.52360	.61087	.69813	.78540	.87266	.95993
(DEG)	0.00000	5.00000	10.00000	15.00000	20.00000	25.00000	30.00000	35.00000	40.00000	45.00000	50.00000	55.00000
0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
.14000	0.00000	.03785	.07501	.11081	.14459	.17570	.20353	.22752	.24710	.26176	.27101	.27436
.28000	0.00000	.06936	.13755	.20341	.26581	.32363	.37579	.42128	.45910	.48829	.50792	.51704
.42000	0.00000	.09493	.18847	.27901	.36514	.44543	.51848	.58293	.63745	.68074	.71147	.72627
.56000	0.00000	.11531	.22896	.33929	.44466	.54346	.63407	.71492	.78442	.84101	.88307	.90887
.70000	0.00000	.13105	.26037	.38621	.50684	.62055	.72562	.82033	.90296	.97175	1.02486	1.06030
.84000	0.00000	.14295	.28415	.42185	.55430	.67975	.79644	.90261	.99645	1.07609	1.13957	1.18472
.98000	0.00000	.15171	.30170	.44824	.58962	.72410	.84993	.96533	1.06850	1.15752	1.23037	1.28478
1.12000	0.00000	.15793	.31431	.46729	.61524	.75649	.88931	1.01199	1.12271	1.21960	1.30063	1.36351
1.26000	0.00000	.16237	.32113	.48066	.63333	.77953	.91758	1.04583	1.16251	1.26582	1.35375	1.42408
1.40000	0.00000	.16534	.32913	.48979	.64576	.79548	.93734	1.06974	1.19101	1.29938	1.39236	1.46961
1.54000	0.00000	.16738	.33389	.49585	.65406	.80621	.95078	1.08620	1.21088	1.32315	1.42122	1.50304
1.68000	0.00000	.16855	.33563	.49975	.65944	.81324	.95966	1.09721	1.22438	1.33957	1.44103	1.52732
1.82000	0.00000	.16933	.33720	.50218	.66283	.81770	.96536	1.10438	1.23330	1.35060	1.45469	1.54380
1.96000	0.00000	.16973	.33815	.50366	.66489	.82045	.96892	1.10892	1.23903	1.35782	1.46373	1.55526
2.10000	0.00000	.17006	.33870	.50452	.66611	.82209	.97107	1.11170	1.24261	1.36242	1.46970	1.56289
2.24000	0.00000	.17021	.33902	.50501	.66681	.82304	.97234	1.11336	1.24479	1.36527	1.47345	1.56735
2.38000	0.00000	.17029	.33918	.50528	.66720	.82357	.97305	1.11432	1.24607	1.36649	1.47576	1.57099
2.52000	0.00000	.17034	.33927	.50542	.66740	.82386	.97345	1.11486	1.24680	1.36749	1.47714	1.57292
2.66000	0.00000	.17036	.33932	.50549	.66751	.82401	.97366	1.11515	1.24721	1.36856	1.47795	1.57403
2.80000	0.00000	.17037	.33934	.50553	.66756	.82408	.97376	1.11530	1.24742	1.36888	1.47841	1.57478
2.94000	0.00000	.17037	.33935	.50555	.66759	.82412	.97382	1.11538	1.24754	1.36904	1.47867	1.57515
3.08000	0.00000	.17037	.33936	.50555	.66760	.82414	.97384	1.11542	1.24760	1.36913	1.47880	1.57537
3.22000	0.00000	.17038	.33936	.50556	.66760	.82415	.97386	1.11544	1.24762	1.36918	1.47887	1.57546
3.36000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24764	1.36920	1.47891	1.57554
3.50000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24764	1.36921	1.47892	1.57557
3.64000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36921	1.47893	1.57559
3.78000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36921	1.47894	1.57560
3.92000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.06000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.20000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.34000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.48000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.62000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.76000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
4.90000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.04000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.18000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.32000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.46000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.60000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.74000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
5.88000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.02000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.16000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.30000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.44000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.58000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.72000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
6.86000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560
7.00000	0.00000	.17038	.33936	.50556	.66761	.82415	.97386	1.11545	1.24765	1.36922	1.47894	1.57560



142	RCYCLE	4	5	5	5	5	5	6	6	6	6	6	6
	(RAD)*	1.04720	1.13446	1.22173	1.23918	1.25664	1.27409	1.29154	1.30900	1.32645	1.34390	1.36136	1.37881
	(DEG)*	60.00000	65.00000	70.00000	71.00000	72.00000	73.00000	74.00000	75.00000	76.00000	77.00000	78.00000	79.00000
	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	.14000	.27127	.26105	.24270	.23763	.23241	.22664	.22046	.21372	.20643	.19848	.18983	.18033
	.28000	.51457	.49919	.46890	.46040	.45140	.44152	.43081	.41911	.40637	.39243	.37716	.36036
	.42000	.72960	.71351	.67713	.66662	.65528	.64278	.62911	.61409	.59763	.57953	.55960	.53755
	.56000	.91644	.90330	.86581	.85451	.84211	.82831	.81308	.79621	.77759	.75699	.73416	.70877
	.70000	1.07578	1.06835	1.03376	1.02265	1.01026	.99628	.98067	.96323	.94380	.92213	.89795	.87087
	.84000	1.20849	1.20913	1.18043	1.17028	1.15971	1.14544	1.13042	1.11342	1.09428	1.07274	1.04850	1.02114
	.98000	1.31888	1.32681	1.30597	1.29732	1.28717	1.27527	1.26155	1.24578	1.22779	1.20731	1.18403	1.15752
	1.12000	1.40552	1.42315	1.41128	1.40045	1.39610	1.38600	1.37406	1.36006	1.34384	1.32510	1.30355	1.27874
	1.26000	1.47411	1.50037	1.49779	1.49295	1.48660	1.47853	1.46865	1.45675	1.44266	1.42611	1.40679	1.38428
	1.40000	1.52673	1.56696	1.56741	1.56456	1.56025	1.55428	1.54657	1.53691	1.52514	1.51100	1.49419	1.47432
	1.54000	1.56618	1.60747	1.62227	1.62131	1.61896	1.61504	1.60945	1.60202	1.59259	1.58091	1.56671	1.54961
	1.68000	1.59511	1.64240	1.66450	1.66537	1.66481	1.66278	1.65918	1.65386	1.64665	1.63736	1.62570	1.61134
	1.82000	1.61583	1.66806	1.69658	1.69886	1.69881	1.69953	1.69772	1.69430	1.68914	1.68204	1.67275	1.66098
	1.96000	1.63032	1.68650	1.72025	1.72379	1.72616	1.72726	1.72699	1.72524	1.72187	1.71672	1.70957	1.70014
	2.10000	1.64022	1.69945	1.73738	1.74197	1.74545	1.74774	1.74877	1.74842	1.74559	1.74312	1.73781	1.73043
	2.24000	1.64683	1.70835	1.74954	1.75495	1.75932	1.76258	1.76466	1.76547	1.76490	1.76282	1.75907	1.75344
	2.38000	1.65113	1.71432	1.75797	1.76402	1.76908	1.77310	1.77601	1.77774	1.77819	1.77725	1.77478	1.77058
	2.52000	1.65387	1.71824	1.76371	1.77023	1.77582	1.78041	1.78397	1.78641	1.78766	1.78762	1.78616	1.78312
	2.66000	1.65556	1.72076	1.76752	1.77439	1.78036	1.78539	1.78943	1.79241	1.79427	1.79492	1.79425	1.79212
	2.80000	1.65659	1.72233	1.77080	1.77712	1.78337	1.78872	1.79310	1.79648	1.79879	1.79996	1.79989	1.79846
	2.94000	1.65719	1.72323	1.77158	1.77888	1.78532	1.79089	1.79552	1.79919	1.80183	1.80338	1.80375	1.80284
	3.08000	1.65754	1.72387	1.77256	1.77998	1.78656	1.79227	1.79709	1.80096	1.80383	1.80565	1.80635	1.80582
	3.22000	1.65773	1.72421	1.77317	1.78066	1.78733	1.79315	1.79808	1.80209	1.80512	1.80714	1.80806	1.80780
	3.36000	1.65784	1.72440	1.77352	1.78107	1.78779	1.79368	1.79869	1.80279	1.80594	1.80889	1.80916	1.80910
	3.50000	1.65789	1.72459	1.77373	1.78131	1.78807	1.79400	1.79907	1.80323	1.80645	1.80868	1.80967	1.80993
	3.64000	1.65792	1.72456	1.77385	1.78145	1.78823	1.79419	1.79929	1.80349	1.80676	1.80905	1.81030	1.81046
	3.78000	1.65794	1.72453	1.77392	1.78153	1.78832	1.79430	1.79942	1.80364	1.80694	1.80927	1.81057	1.81078
	3.92000	1.65795	1.72461	1.77396	1.78157	1.78838	1.79436	1.79949	1.80373	1.80705	1.80940	1.81073	1.81098
	4.06000	1.65795	1.72462	1.77398	1.78159	1.78841	1.79440	1.79953	1.80378	1.80711	1.80948	1.81082	1.81110
	4.20000	1.65795	1.72462	1.77399	1.78160	1.78842	1.79442	1.79956	1.80381	1.80715	1.80952	1.81088	1.81117
	4.34000	1.65795	1.72462	1.77399	1.78161	1.78843	1.79443	1.79957	1.80383	1.80717	1.80954	1.81091	1.81121
	4.48000	1.65795	1.72462	1.77399	1.78161	1.78843	1.79443	1.79958	1.80384	1.80718	1.80956	1.81093	1.81123
	4.62000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79443	1.79958	1.80384	1.80718	1.80956	1.81094	1.81124
	4.76000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79443	1.79958	1.80384	1.80719	1.80957	1.81094	1.81125
	4.90000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81094	1.81125
	5.04000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81125
	5.18000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81125
	5.32000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	5.46000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	5.60000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	5.74000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	5.88000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.02000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.16000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.30000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.44000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.58000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.72000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	6.86000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126
	7.00000	1.65795	1.72462	1.77400	1.78162	1.78844	1.79444	1.79958	1.80384	1.80719	1.80957	1.81095	1.81126

NCYCLE	7	7	7	8	8	9	10	12
R+ (RAD)*	1.39626	1.41372	1.43117	1.44862	1.46608	1.48353	1.50098	1.51844
(DEG)*	80.80100	81.00000	82.00000	83.00000	84.00000	85.00000	86.00000	87.00000
0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
.14000	.16987	.15823	.14516	.13024	.11286	.09190	.06510	.02541
.28000	.34176	.32109	.29758	.27073	.23926	.20107	.15174	.07719
.42000	.51704	.48554	.45437	.41846	.37613	.32438	.25681	.15256
.56000	.68076	.64835	.61186	.56958	.51943	.45766	.37613	.24779
.70000	.84819	.80582	.76619	.72000	.66485	.59639	.50507	.35858
.84000	.99017	.95471	.91384	.86590	.80926	.73615	.63897	.48030
.98000	1.12723	1.09237	1.05186	1.00400	.94604	.87295	.77348	.60838
1.12000	1.25013	1.21693	1.17803	1.13173	1.07525	1.00344	.90477	.73850
1.26000	1.35803	1.32728	1.29093	1.24732	1.19370	1.12498	1.02967	.86679
1.40000	1.45095	1.42386	1.38989	1.34976	1.30000	1.23572	1.14576	.99000
1.54000	1.52912	1.50454	1.47491	1.43871	1.39345	1.33451	1.25132	1.10556
1.68000	1.59383	1.57252	1.54653	1.51445	1.47400	1.42090	1.34536	1.21158
1.82000	1.64631	1.62815	1.60572	1.57773	1.54212	1.49501	1.42751	1.30687
1.96000	1.68806	1.67283	1.65372	1.62961	1.59865	1.55741	1.49793	1.39066
2.10000	1.72056	1.70804	1.69194	1.67137	1.64473	1.60900	1.55722	1.46353
2.24000	1.74564	1.73528	1.72181	1.70439	1.68162	1.65090	1.60624	1.52527
2.38000	1.76443	1.75597	1.74475	1.73003	1.71063	1.68434	1.64608	1.57683
2.52000	1.77830	1.77141	1.76204	1.74955	1.73305	1.71058	1.67792	1.61915
2.66000	1.78816	1.78272	1.77485	1.76426	1.75009	1.73082	1.70293	1.65332
2.80000	1.79552	1.79085	1.78418	1.77506	1.76281	1.74617	1.72227	1.68046
2.94000	1.80052	1.79660	1.79085	1.78289	1.77216	1.75762	1.73697	1.70167
3.08000	1.80395	1.80060	1.79554	1.78847	1.77891	1.76603	1.74797	1.71799
3.22000	1.80627	1.80332	1.79877	1.79237	1.78370	1.77210	1.75607	1.73036
3.36000	1.80780	1.80514	1.80097	1.79505	1.78705	1.77641	1.76195	1.73958
3.50000	1.80880	1.80635	1.80244	1.79687	1.78935	1.77942	1.76614	1.74635
3.64000	1.80943	1.80712	1.80340	1.79888	1.79091	1.78150	1.76908	1.75125
3.78000	1.80983	1.80762	1.80402	1.79887	1.79194	1.78290	1.77112	1.75475
3.92000	1.81008	1.80792	1.80441	1.79938	1.79262	1.78384	1.77251	1.75720
4.06000	1.81022	1.80811	1.80465	1.79970	1.79306	1.78445	1.77344	1.75890
4.20000	1.81031	1.80823	1.80480	1.79990	1.79333	1.78485	1.77405	1.76006
4.34000	1.81036	1.80829	1.80489	1.80002	1.79350	1.78510	1.77445	1.76084
4.48000	1.81039	1.80833	1.80494	1.80009	1.79361	1.78526	1.77471	1.76136
4.62000	1.81041	1.80836	1.80498	1.80014	1.79367	1.78536	1.77487	1.76169
4.76000	1.81042	1.80837	1.80499	1.80016	1.79371	1.78541	1.77497	1.76191
4.90000	1.81042	1.80837	1.80500	1.80018	1.79373	1.78545	1.77504	1.76205
5.04000	1.81043	1.80839	1.80501	1.80019	1.79374	1.78547	1.77507	1.76214
5.18000	1.81043	1.80839	1.80501	1.80019	1.79375	1.78548	1.77510	1.76219
5.32000	1.81043	1.80839	1.80501	1.80019	1.79376	1.78549	1.77511	1.76222
5.46000	1.81043	1.80839	1.80501	1.80019	1.79376	1.78549	1.77512	1.76224
5.60000	1.81043	1.80839	1.80501	1.80019	1.79376	1.78550	1.77512	1.76225
5.74000	1.81043	1.80839	1.80501	1.80020	1.79376	1.78550	1.77512	1.76226
5.88000	1.81043	1.80839	1.80501	1.80020	1.79376	1.78550	1.77512	1.76226
6.02000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
6.16000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
6.30000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
6.44000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
6.58000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
6.72000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
6.86000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227
7.00000	1.81043	1.80838	1.80501	1.80020	1.79376	1.78550	1.77513	1.76227

OGAMMA= 1.552795 SMALLM= .035059

## POINT VORTEX LOCATIONS

## TOP BOUNDARY LAYER

## BOTTOM BOUNDARY LAYER

A	K	X(A)	Y(A)	XDOT(A)	YDOT(A)	GAMMA(A)	XB(A)	YB(A)	XDOTB(A)	YDOTB(A)	GMA9(A)
1	39	-1.470798	.337896	-.084505	-.001953	.017547	-1.470798	-.387896	-.084505	.001953	-.017547
2	39	-1.478492	.562271	-.400360	-.037539	.037135	-1.478492	-.562271	-.400360	.037539	-.037135
3	39	-1.374651	.513777	-.274386	-.037525	.061020	-1.374651	-.513777	-.274386	.037525	-.061020
4	39	-1.204024	.592420	-.283578	.054769	.072364	-1.204024	-.592420	-.283578	-.054769	-.072364
5	39	-1.250174	.423280	-.092518	.084677	.084417	-1.250174	-.423280	-.092518	-.084677	-.084417
6	39	-1.049625	.658744	-.317442	.186665	.080703	-1.049625	-.658744	-.317442	-.186665	-.080703
7	39	-.897825	.456571	.231030	.491555	.095220	-.897825	-.456571	.231030	-.491555	-.095220
8	39	-1.173107	.302748	.129747	.263879	.106676	-1.173107	-.302748	.129747	-.263879	-.106676
9	39	-1.011672	.435365	-.028465	.268545	.102046	-1.011672	-.435365	-.028465	-.268545	-.102046
10	39	-.915831	.436608	.237372	.536720	.115301	-.915831	-.436608	.237372	-.536720	-.115301
11	39	-1.007367	.135213	.115211	.471943	.124202	-1.007367	-.135213	.115211	-.471943	-.124202
12	39	-1.673170	.311740	-.007193	-.031816	.131124	-1.673170	-.311740	-.007193	-.031816	-.131124
13	39	-1.094772	.049451	.405832	.028246	.126061	-1.094772	-.049451	.405832	-.028246	-.126061
14	39	-1.439694	.161685	.392592	.037173	.134868	-1.439694	-.161685	.392592	-.037173	-.134868
15	39	-1.319320	.198246	.317274	.082329	.129898	-1.319320	-.198246	.317274	-.082329	-.129898
16	39	-1.607210	.030250	1.050349	-.005364	.127849	-1.607210	-.030250	1.050349	.005364	-.127849
17	39	-2.076149	.255191	-.185664	-.474283	.135813	-2.076149	-.255191	-.135664	.474283	-.135813
18	39	-1.711810	.148758	.450861	-.114611	.131037	-1.711810	-.148758	.450361	.114611	-.131037
19	39	-1.983040	.186633	.276527	-.098828	.129110	-1.983040	-.186633	.276527	.098328	-.129110
20	39	-2.204532	.125398	.014800	-.275954	.127702	-2.204532	-.125398	.014800	.275954	-.127702
21	39	-1.624535	.627607	-.481717	-.1624535	.134314	-1.624535	-.627607	-.481717	.082781	-.134314
22	39	-1.795804	.452980	-.345550	-.150479	.129791	-1.795804	-.452980	-.345550	.150479	-.129791
23	39	-1.940624	.367292	-.170558	-.338341	.128055	-1.940624	-.367292	-.170558	.338341	-.128055
24	39	-1.961811	.431517	-.641739	-.599320	.126807	-1.961811	-.431517	-.641739	.599320	-.126807
25	39	-1.864390	.601270	-.847009	-.472699	.125738	-1.864390	-.601270	-.847009	.472699	-.125738
26	39	-1.666043	.723831	-.902404	-.217859	.124786	-1.666043	-.723831	-.902404	.217958	-.124786
27	39	-1.728547	.794835	-1.210554	-.499095	.123862	-1.728547	-.794835	-1.210554	.499095	-.123862
28	39	-1.294580	.767692	-.569317	-.130324	.124797	-1.294580	-.767692	-.569317	.130324	-.124797
29	39	-1.393426	.819677	-.948762	-.372662	.123000	-1.393426	-.819677	-.948762	.372662	-.123000
30	39	-1.221233	.865369	-.945012	-.188080	.121990	-1.221233	-.865369	-.945012	.188080	-.121990
31	39	-1.127894	.909917	-1.034864	-.050010	.121092	-1.127894	-.909917	-1.034864	.050010	-.121092
32	39	-.970191	.899408	-.728856	-.174231	.122041	-.970191	-.899408	-.728856	.174231	-.122041
33	39	-.880038	.931829	-.855026	-.078367	.120286	-.880038	-.931829	-.855026	.078367	-.120286
34	39	-.769794	.949858	-.836941	-.104686	.119314	-.769794	-.949858	-.836941	.104686	-.119314
35	39	-.654144	.970624	-.894004	-.135379	.118474	-.654144	-.970624	-.894004	.135379	-.118474
36	39	-.523922	.997195	-1.025793	-.180170	.117752	-.523922	-.997195	-1.025793	.180170	-.117752
37	39	-.353272	1.030128	-1.257200	-.240873	.118833	-.353272	-1.030128	-1.257200	.240873	-.118833
38	39	-.159547	1.048199	-1.529307	-.134673	.117236	-.159547	-1.048199	-1.529307	.134673	-.117236
39	39	.054171	1.033641	-1.704354	.115828	.116460	.054171	-1.033641	-1.704354	-.115828	-.116460

## TOP REAR SHEAR LAYER

## BOTTOM REAR SHEAR LAYER

A	K	XRT(A)	YRT(A)	XROOT(A)	YROOT(A)	GMR(A)	XRB(A)	YRB(A)	XROOTB(A)	YROOTB(A)	GMA9(A)
1	39	-1.391255	.428310	-.060685	-.034127	-.001701	-1.391255	-.428310	-.060685	.034127	.001701
2	39	-1.366517	.602144	-.457523	-.084011	-.009489	-1.366517	-.602144	-.457523	.084011	.009489
3	39	-1.445651	.649619	-.541731	-.076439	-.020866	-1.445651	-.649619	-.541731	.076439	.020866
4	39	-.960804	.712634	-.271053	.221530	-.012567	-.960804	-.712634	-.271053	-.221530	.012567
5	39	-.850305	.590171	.030460	.210316	-.064597	-.850305	-.590171	.030460	-.210316	.064597

# PRESSURE DISTRIBUTION

T= 5.0477

7FAT= .8770

AK= 1.0000

AKOOT= 0.0000

THEIAS= 87.00

CEG	PHIPI	PHIPI	Z(PHIT)	PSIKSQD	GPK	PDHAG	UTAN
0.00	.007121	0.000000	.014242	-.000000	.014242	.014242	-.000000
10.00	.007059	0.000000	.014115	-.115164	-.101046	-.099511	.339359
20.00	.006851	0.000000	.013701	-.445701	-.432000	-.405947	.667608
30.00	.006413	0.000000	.012826	-.948413	-.935586	-.810241	.973865
40.00	.005566	0.000000	.011131	-1.556424	-1.545493	-1.183916	1.247647
50.00	.003913	0.000000	.007826	-2.187262	-2.179436	-1.400915	1.476939
60.00	.000524	0.000000	.001048	-2.748803	-2.747755	-1.373878	1.657952
65.00	-.002488	0.000000	-.004975	-2.974729	-2.979304	-1.259108	1.724624
70.00	-.007181	0.000000	-.014366	-3.147067	-3.161433	-1.081274	1.773997
75.00	-.014934	0.000000	-.029868	-3.253856	-3.283724	-.849890	1.803845
80.00	-.028889	0.000000	-.057779	-3.277452	-3.335431	-.579192	1.816429
85.00	-.057824	0.000000	-.115648	-3.188001	-3.303649	-.287932	1.785498
90.00	-.135008	0.000000	-.270016	-2.898292	-3.168308	-.000000	1.702437
95.00	-.457438	0.000000	-.914875	-2.016878	-2.931754	.255519	1.420168
100.00	-.954257	0.000000	-1.988499	-1.043036	-2.951535	.512529	1.021291
105.00	-.595697	0.000000	-1.101379	-1.270289	-2.461668	.637127	1.127071
110.00	-.780847	0.000000	-1.561682	-.704720	-2.266402	.775155	.839476
115.00	-.673573	0.000000	-1.347147	-.574824	-1.921971	.812260	.758172
120.00	-.730796	0.000000	-1.441592	-.302666	-1.764258	.882129	.550151
125.00	-.745331	0.000000	-1.400663	-.164166	-1.654829	.949171	.405174
130.00	-.758687	0.000000	-1.517375	-.077875	-1.595244	1.025406	.279060
135.00	-.766323	0.000000	-1.522646	-.027253	-1.559899	1.103015	.165885
140.00	-.775455	0.000000	-1.550910	-.005173	-1.556083	1.192029	.071922
POTENTIAL VORTEX APPROX	INVALID	INVALID	ALPHA= 5	CORE RADIUS=	.035297		
145.00	-.715488	0.000000	-1.430977	-.037499	-1.468676	1.203069	-.194163
150.00	-.543223	0.000000	-1.086447	-.234987	-1.321433	1.144395	-.484754
POTENTIAL VORTEX APPROX	INVALID	INVALID	ALPHA= 7	CORE RADIUS=	.034997		
POTENTIAL VORTEX APPROX	INVALID	INVALID	ALPHA= 10	CORE RADIUS=	.016923		
155.00	-.752162	0.000000	-1.504324	-.359233	-1.863557	1.688956	-.599360
160.00	-.709884	0.000000	-1.419772	-.424160	-1.843937	1.732734	-.651276
165.00	-.686461	0.000000	-1.372923	-.515227	-1.888150	1.823813	-.717793
POTENTIAL VORTEX APPROX	INVALID	INVALID	ALPHA= 11	CORE RADIUS=	.031208		
170.00	-.756222	0.000000	-1.512445	-.233699	-1.746144	1.719616	-.483425
175.00	-.652105	0.000000	-1.304209	-.253229	-1.557438	1.551512	-.503219
180.00	-.551320	0.000000	-1.102640	-.000000	-1.102640	1.102640	-.000000

K= 39

CDPK= .503871

CDSK= .012166

CEK= .516037

CDN= .034568

MAX VELOCITY= 1.811 AT THETA= 79.0 DEGREES  
MAX BACKFLOW VEL= -.718 AT THETA=165.0 DEGREES  
MIN TANGENTIAL VELOCITY BETWEEN MAX VELOCITY AND MAX BACKFLOW VELOCITY= .072 AT THETA=140.0 DEGREES  
REAR SEPARATION ANGLE=161.7 DEGREES

146 RVIA SUBROUTINE N= 5 THETA5(N)= 161.721311 U00(N)= -.635553  
GAMA(N)= -.025248

GAMA CHECK SUM= -.458117 N= 5 FLAG(N=1)= 1

BEFORE VMFIX(X(ALPHA),Y(ALPHA))=(-.85786, .50642)

VMFIX ALPHA= 10 ANGLE= -75.488734  
X= -.903573 Y= .430764 XDOT= .304025 YDOT= .637725

AFTER VMFIX(X(ALPHA),Y(ALPHA))=(-.86557, .51048)  
ELAPSED TIME= 44.988000

ADYNF      SAMPLE      INPUT  
CASE ... OGIVE CYLINDER ... ANGLE OF ATTACK (5 DEG)

*****		ADYNF	SAMPLE	CASE	*****				
5.0		0.0		50.478	10.74		2.35		2.35
4	15								
0.0		0.0							
	.096516	9.036431		.181378	1				CARD 1
	.163031	8.165342		.306378	2				CARD 2
	.229547	4.086353		.431378	3				CARD 3
	.296063	.047975		.556378	4				CARD 4
	.362578	.041644		.681378	5				CARD 5
	.429094	.043186		.806378	6				CARD 6
	.495610	.055931		.931378	7				CARD 7
	.562125	.069124		1.056378	8				CARD 8
	.628641	.087352		1.181378	9				CARD 9
	.695157	.105378		1.306378	10				CARD 10
	.761672	.132163		1.431378	11				CARD 11
	.828188	.154608		1.556378	12				CARD 12
	.894704	.187945		1.681378	13				CARD 13
	.961215	.222631		1.806378	14				CARD 14
1.0		.249663		1.931378	15				CARD 15
0.0		.125	.3		1.0				CARD 16
									CARD 17
									CARD 18
									CARD 19
									CARD 20

\*\*\*\*\* ADYNF SAMPLE OUTPUT \*\*\*\*\*

GIVEN DATA

148

1	0.00000000	0.00000000
2	.09651600	.06864185
3	.16303100	.06202495
4	.22954700	.03104044
5	.29606300	.00036442
6	.36257800	.00031633
7	.42909400	.00032805
8	.49561000	.00042486
9	.56212500	.00052507
10	.62864100	.00066354
11	.69515700	.00080046
12	.76167200	.00100393
13	.82818800	.00117442
14	.89470400	.00142765
15	.96121900	.00169113
16	1.00000000	.00189647

NO. OF INITIAL

KNOTS = 4

ITER = 8

KNOTS PRIOR TO OPTIMIZATION

0.000000 .125000 .300000 1.000000

\*\*\* FINAL OUTPUT \*\*\*

KNOTS

CUBIC COEFFICIENTS

XI( 1) = -0.000000

C(1) = -2.892801E-14  
C(2) = -4.355484E+00  
C(3) = 1.185283E+02  
C(4) = 6.991980E+02

XI( 2) = .071209

C(1) = 3.840772E-02  
C(2) = 1.888742E+00  
C(3) = -3.083995E+01  
C(4) = 1.349466E+02

XI( 3) = .149811

C(1) = 6.186244E-02  
C(2) = -4.582100E-01  
C(3) = 9.812087E-01  
C(4) = -6.308512E-01

XI( 4) = 1.000000

LEAST SQUARE ERROR =

4.933780E-03

AVERAGE ERROR =

3.812333E-03

MAXIMUM ERROR =

1.349815E-02 AT -.296063

# APPROXIMATION AND SCALED ERROR CURVE

	DATA POINT	APPROXIMATION	DEVIATION X 10E+3
1	0.00000000	-0.00000000	0.000000
2	.09551500	.06864185	.000000
3	.16303100	.05597500	-6.049947
4	.22954700	.03124520	-.204763
5	.29506300	.01386257	-13.498148
6	.36257800	.00271330	-2.396967
7	.42909400	-.00331686	3.644905
8	.49561000	-.00534162	5.766478
9	.56212500	-.00447494	5.000012
10	.62864100	-.00183070	2.494236
11	.69515700	.00147717	-.676710
12	.76167200	.00437472	3.330796
13	.82818800	.00562812	-4.453697
14	.89470400	.00424339	-2.815733
15	.96121900	-.00093329	2.624420
16	1.00000000	-.00614404	8.040511

Z	CON(Z)
0.000000	-.000000
.050000	-.008853
.100000	.070443
.150000	.061776
.200000	.041257
.250000	.025170
.300000	.013040
.350000	.004395
.400000	-.001278
.450000	-.004332
.500000	-.005361
.550000	-.004798
.600000	-.003116
.650000	-.000787
.700000	.0001714
.750000	.003915
.800000	.005342
.850000	.005523
.900000	.003985
.950000	.000253
1.000000	-.006144

BFG,STEP 0. 1.00000000E+00 1  
 BEG,STEP 5.00000000E-01 5.00000000E-01 1  
 H2 CONVERGENCE AT ROW 3  
 INTEGRAL IS 3.46173213E-04, ERROR 2.01407345E-04 FROM T(3,2)  
 BEG,STEP 0. 5.00000000E-01 1  
 BEG,STEP 2.50000000E-01 2.50000000E-01 1  
 H2 CONVERGENCE AT ROW 3  
 INTEGRAL IS 1.03065782E-03, ERROR 9.03363896E-05 FROM T(3,2)  
 BEG,STEP 0. 2.50000000E-01 1  
 H2 CONVERGENCE AT ROW 5  
 INTEGRAL IS 8.09074826E-03, ERROR 8.07258925E-05 FROM T(5,2)

647

..... CN= .129465  
 ..... CNI= .709468 ERROR= .00037247 IFLAG= 1



# GIVEN DATA

150

1	0.00000000	0.00000000
2	.09651600	.00707654
3	.16303100	.01047393
4	.22954700	.00770532
5	.29676300	.00910789
6	.36257800	.00011470
7	.42909400	.00014076
8	.49561000	.00021056
9	.56212500	.00029516
10	.62864100	.00041713
11	.69515700	.00055645
12	.76167200	.00076466
13	.82818800	.00097264
14	.89470400	.00127733
15	.96121900	.00162555
16	1.00000000	.00189647

NO. OF INITIAL KNOTS = 4  
ITER = 0

## KNOTS PRIOR TO OPTIMIZATION

0.000000 .071209 .149811 1.000000

\*\*\* FINAL OUTPUT \*\*\*

## KNOTS

## CUBIC COEFFICIENTS

XI( 1) = 0.000000

C(1) = -1.284775E-14  
C(2) = -9.314970E+00  
C(3) = 2.089747E+02  
C(4) = -1.183289E+03

XI( 2) = .071209

C(1) = -3.091969E+02  
C(2) = 2.446370E+00  
C(3) = -4.380895E+01  
C(4) = 2.525566E+02

XI( 3) = .129259

C(1) = 1.286898E-02  
C(2) = -8.665235E-02  
C(3) = 1.733354E-01  
C(4) = -1.033547E-01

XI( 4) = 1.000000

LEAST SQUARE ERROR = 9.302876E-04  
AVERAGE ERROR = 6.924194E-04  
MAXIMUM ERROR = 2.650252E-03 AT .296063

APPROXIMATION AND SCALED ERROR CURVE

DATA POINT	APPROXIMATION	DEVIATION X 10E+4
1	0.00000000	-0.00000000
2	.09651600	-.00702654
3	.16303100	.01013625
4	.22954700	.00581788
5	.29606300	.00275814
6	.36257800	.00077458
7	.42909400	-.00031538
8	.49561000	-.00069418
9	.56212500	-.00054434
10	.62864100	-.00004834
11	.69515700	.00061131
12	.76167200	.00125211
13	.82818800	.00169159
14	.89470400	.00174722
15	.96121900	.00123654
16	1.00000000	.00060493

(0.5=2) CON	
0.000000	-.000000
.050000	-.091223
.100000	.009227
.150000	.011145
.200000	.007570
.250000	.004752
.300000	.002613
.350000	.001076
.400000	.000063
.450000	-.000502
.500000	-.000699
.550000	-.000603
.600000	-.000293
.650000	.000154
.700000	.000661
.750000	.001149
.800000	.001542
.850000	.001761
.900000	.001730
.950000	.001370
1.000000	.000605

BEG,STEP 0. 1.00000000E+00 1  
 BEG,STEP 5.00000000E-01 5.00000000E-01 1  
 H2 CONVERGENCE AT ROW 3  
 INTEGRAL IS 3.75214479E-04, ERROR 2.49143177E-05 FROM T(3,2)  
 BEG,STEP 0. 5.00000000E-01 1  
 BEG,STEP 2.50000000E-01 2.50000000E-01 1  
 H2 CONVERGENCE AT ROW 3  
 INTEGRAL IS 2.53646229E-04, ERROR 1.58105198E-05 FROM T(3,2)  
 BEG,STEP 0. 2.50000000E-01 1  
 H2 CONVERGENCE AT ROW 5  
 INTEGRAL IS -4.86222290E-03, ERROR 1.84561813E-04 FROM T(5,2)

..... CM= .057890  
 ..... CMI= -.004233 ERROR= .00022529 IFLAG= 1

## LIST OF REFERENCES

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2. Wundt, H., "Wachstum der laminaren Grenzschicht an schräg angeströmten Zylinder bei Anfahrt aus der Ruhe," Ingen-Arch 23 212 (1955).
3. Carl de Boor and John R. Rice, "Least Squares Cubic Spline Approximation I - Fixed Knots," Purdue University Computer Sciences Department Report CSD TR20, (1968).
4. Carl de Boor and John R. Rice, "Least Squares Cubic Spline Approximation II - Variable Knots," Purdue University Computer Sciences Department Report CSD TR21, (1968).

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